



Driving dynamics and hybrid combined in the torque vectoring

Concepts of axle differentials with hybrid functionality and active torque distribution

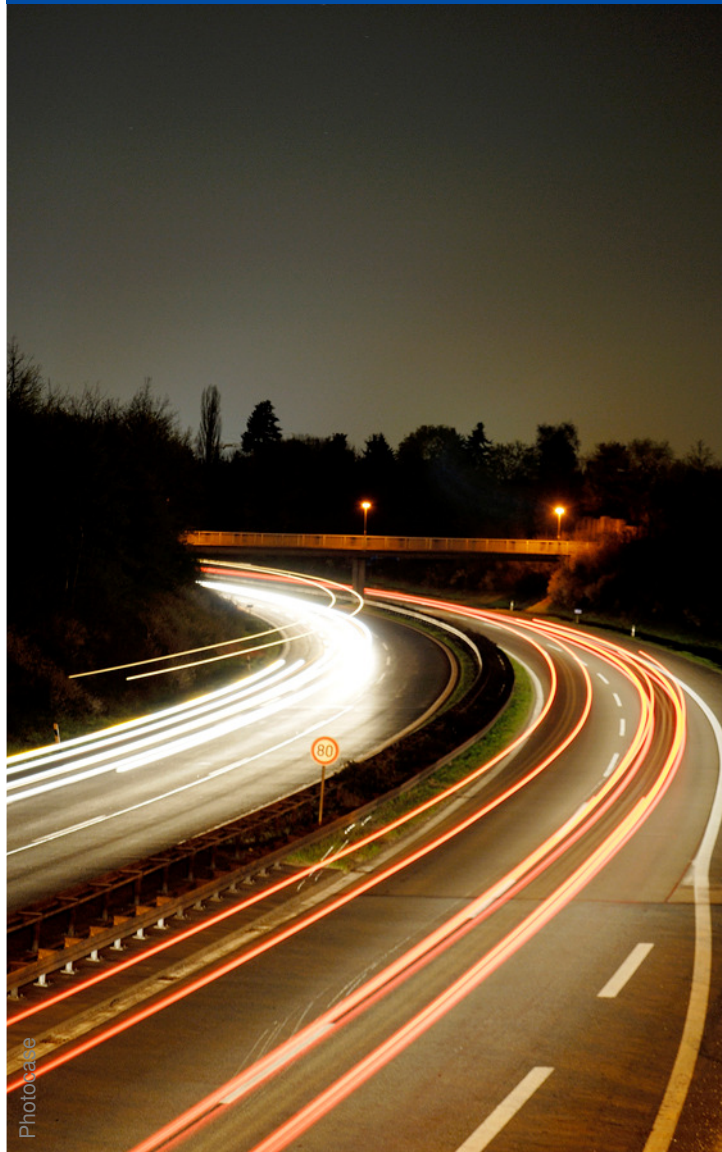
Vehicle Dynamics Expo 2009 'Open Technology Forum'

Dr. Rüdiger Freimann
Dr. Thieß-Magnus Wolter
Erik Schneider

Stuttgart, June 17th, 2009

Overview

Driving dynamics and hybrid combined in the torque vectoring



Initiation

- Motivation
- Torque Vectoring and driving dynamics
- Simulation approach

2 Examples of “Hybridization with active torque distribution”

- Design
- Functionality

Evaluation results for longitudinal and lateral dynamics

- Layout and optimization of longitudinal dynamics
- Layout and optimization of lateral dynamics

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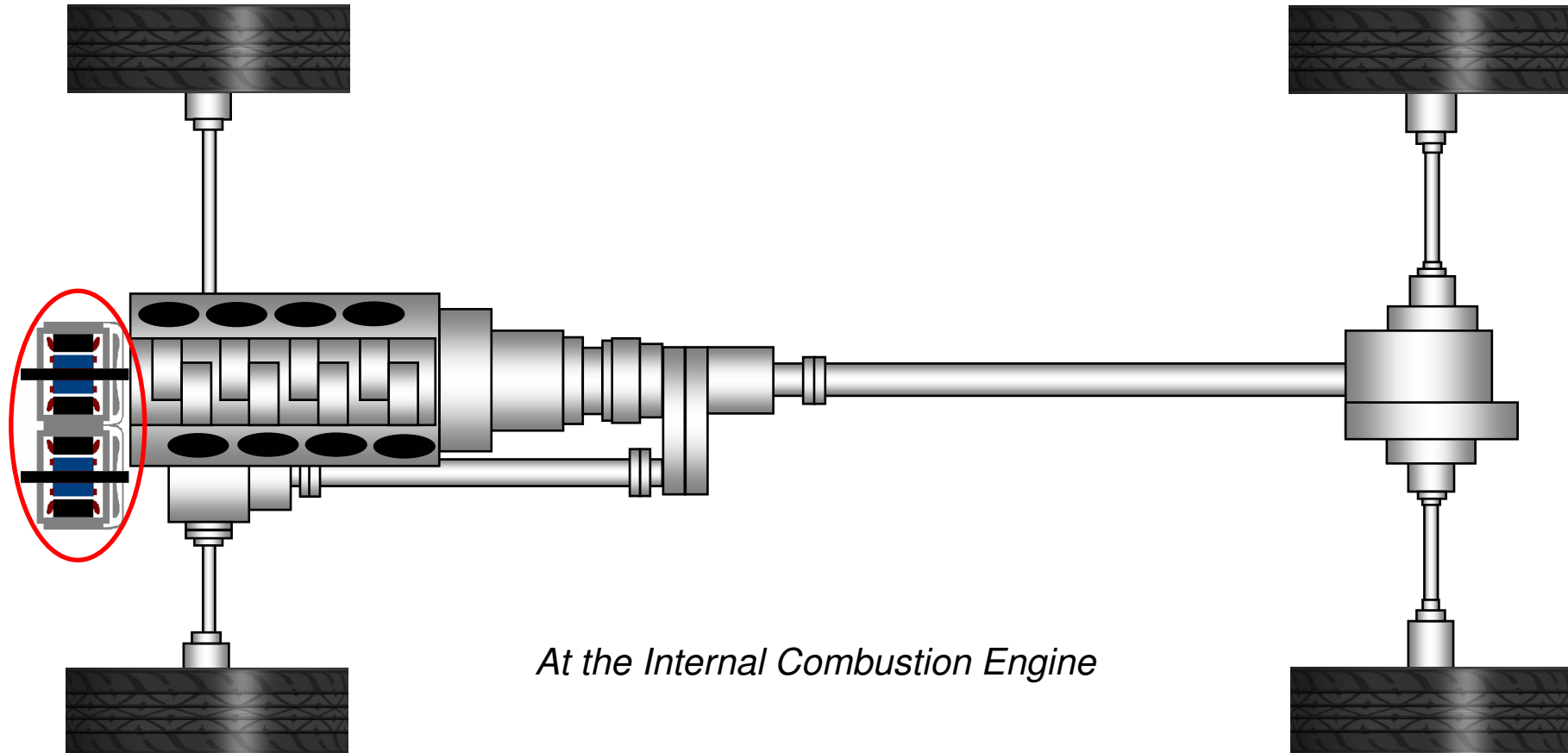
Driving dynamics and hybrid combined in the torque vectoring



- **Active manipulation of lateral dynamics**
 - Torque Vectoring System
- **Active manipulation of longitudinal dynamics**
 - Traction advancement
 - Advancement of acceleration behavior
- **Hybrid function**
 - Energy recovery and boost function
- **Ease integration**
 - Moderate changes in driveline design and package
 - Preservation of engine and driveline configurations
 - Modularity and ability to retrofit

Positioning possibilities

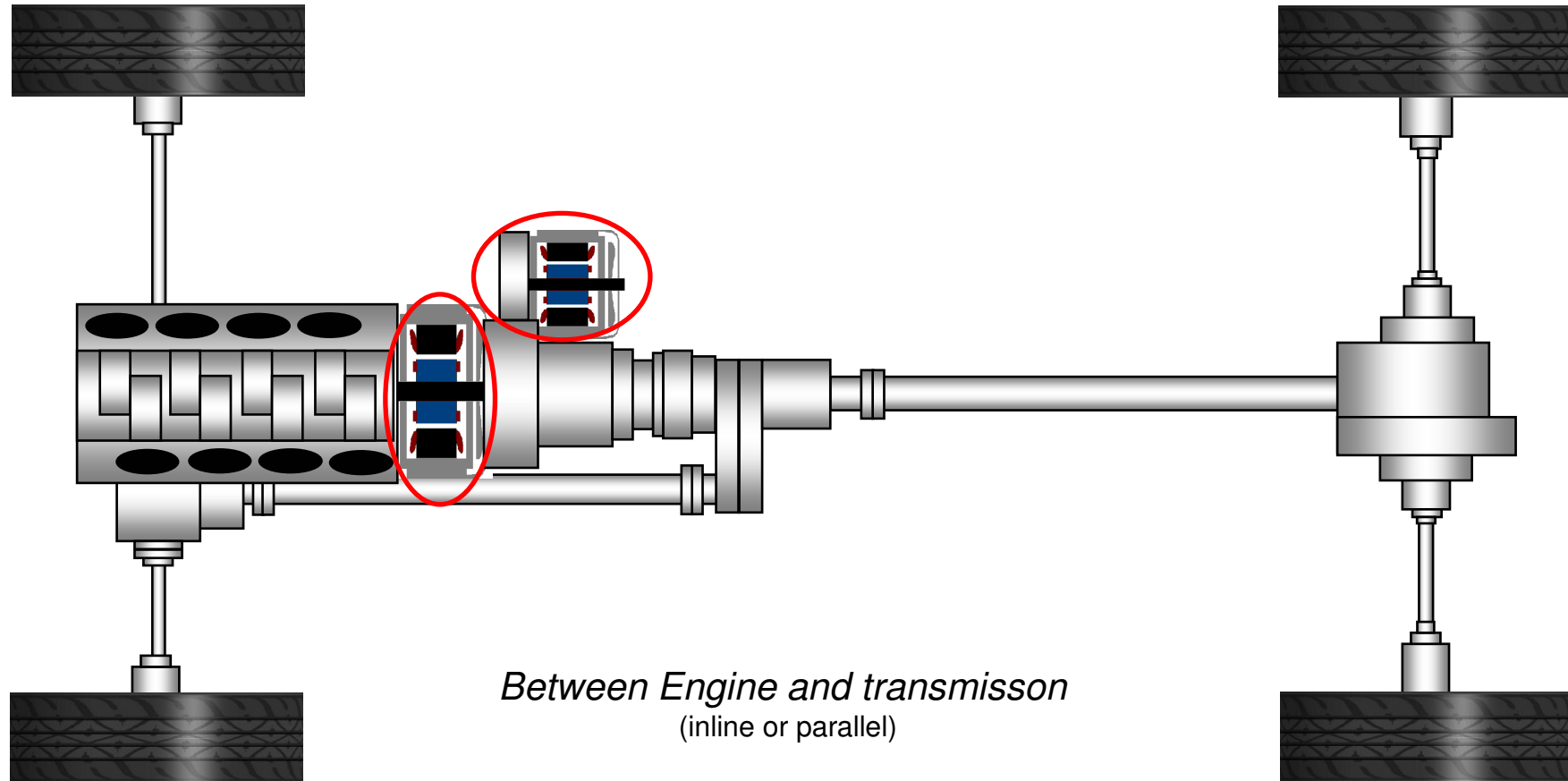
Integration of electrical machines in the powertrain



Quelle: vgl. VDI-Berichte Nr. 1943, 2006

Positioning possibilities

Integration of electrical machines in the powertrain

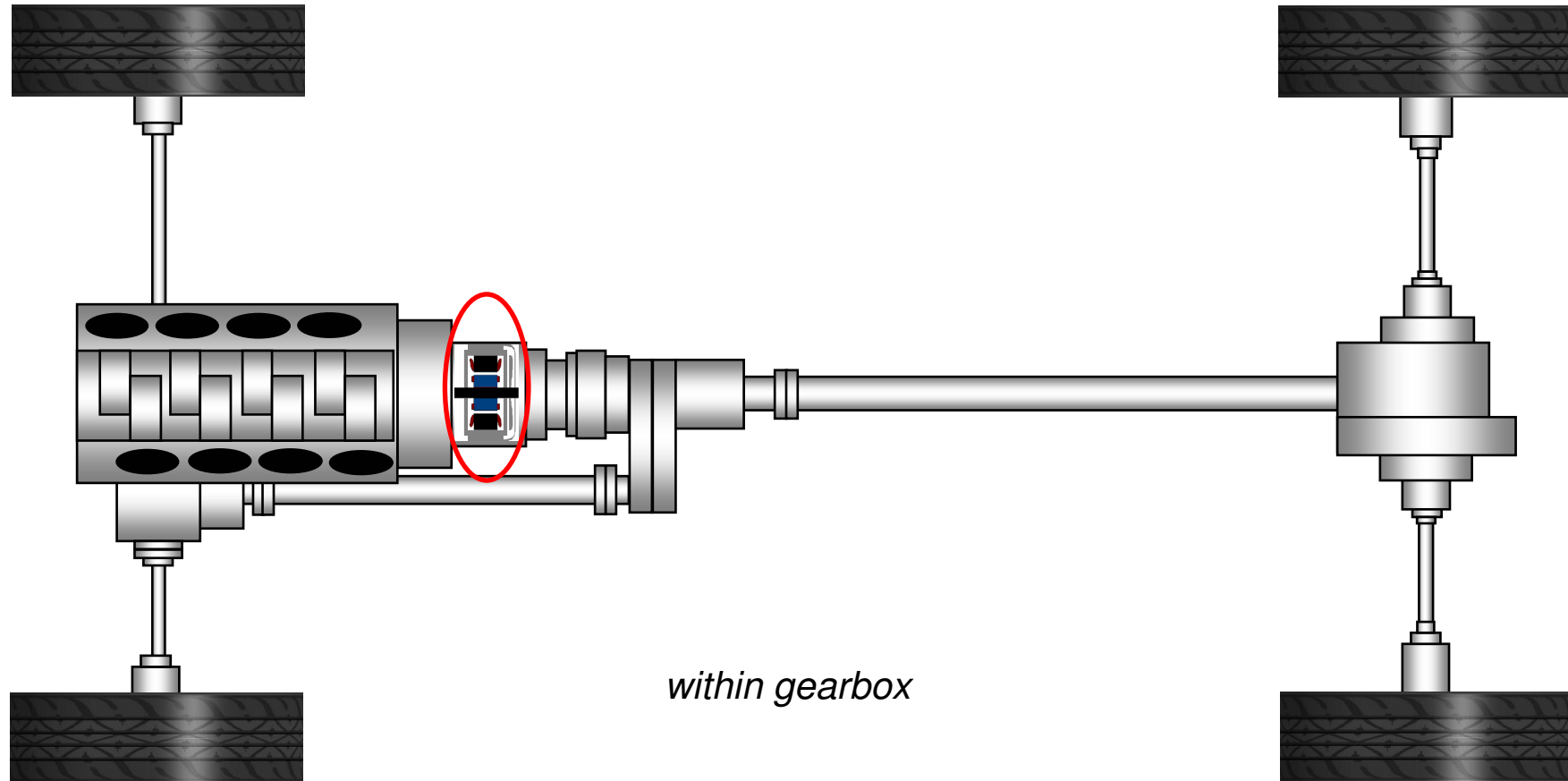


Between Engine and transmission
(inline or parallel)

Quelle: vgl. VDI-Berichte Nr. 1943, 2006

Positioning possibilities

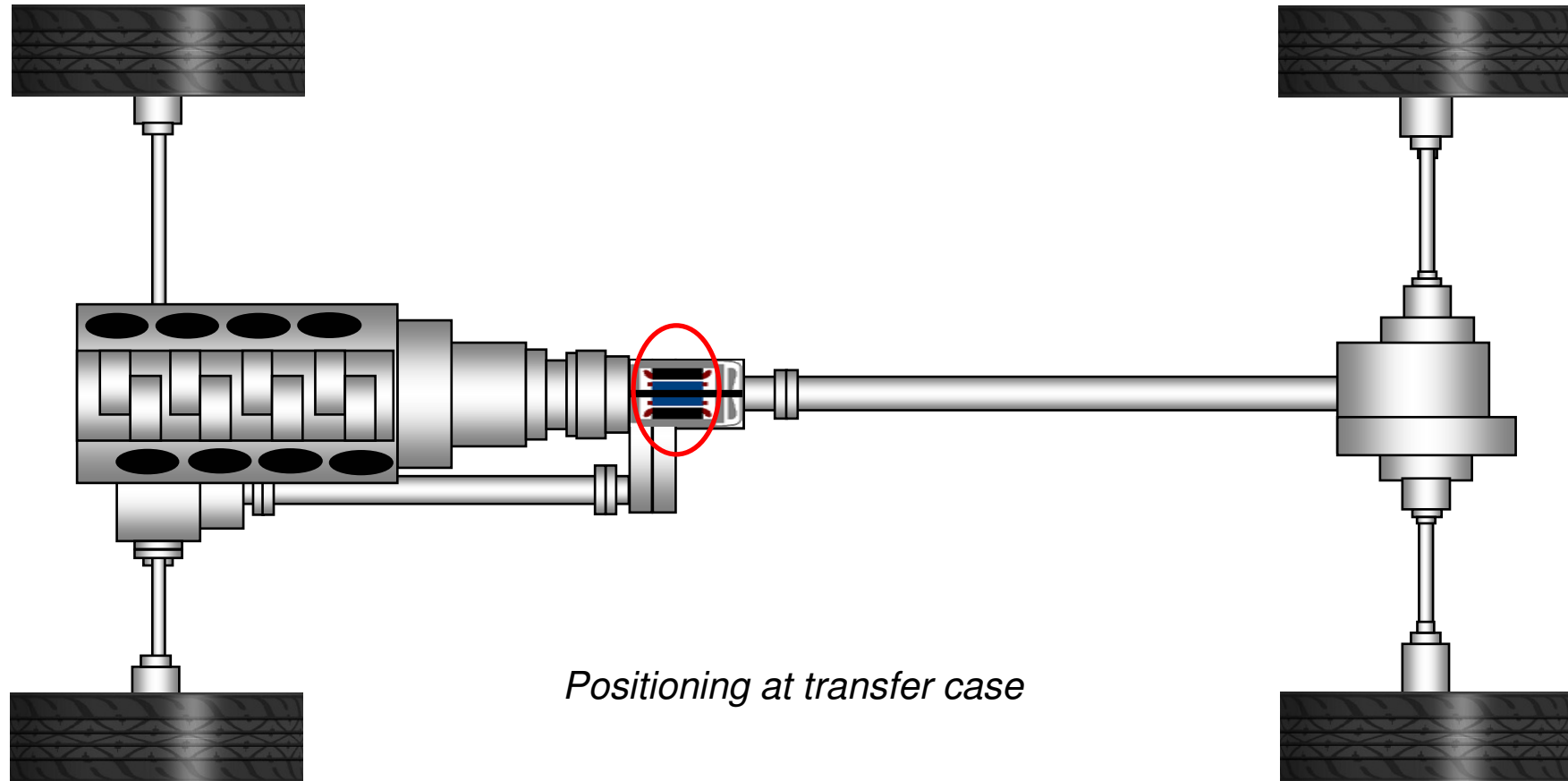
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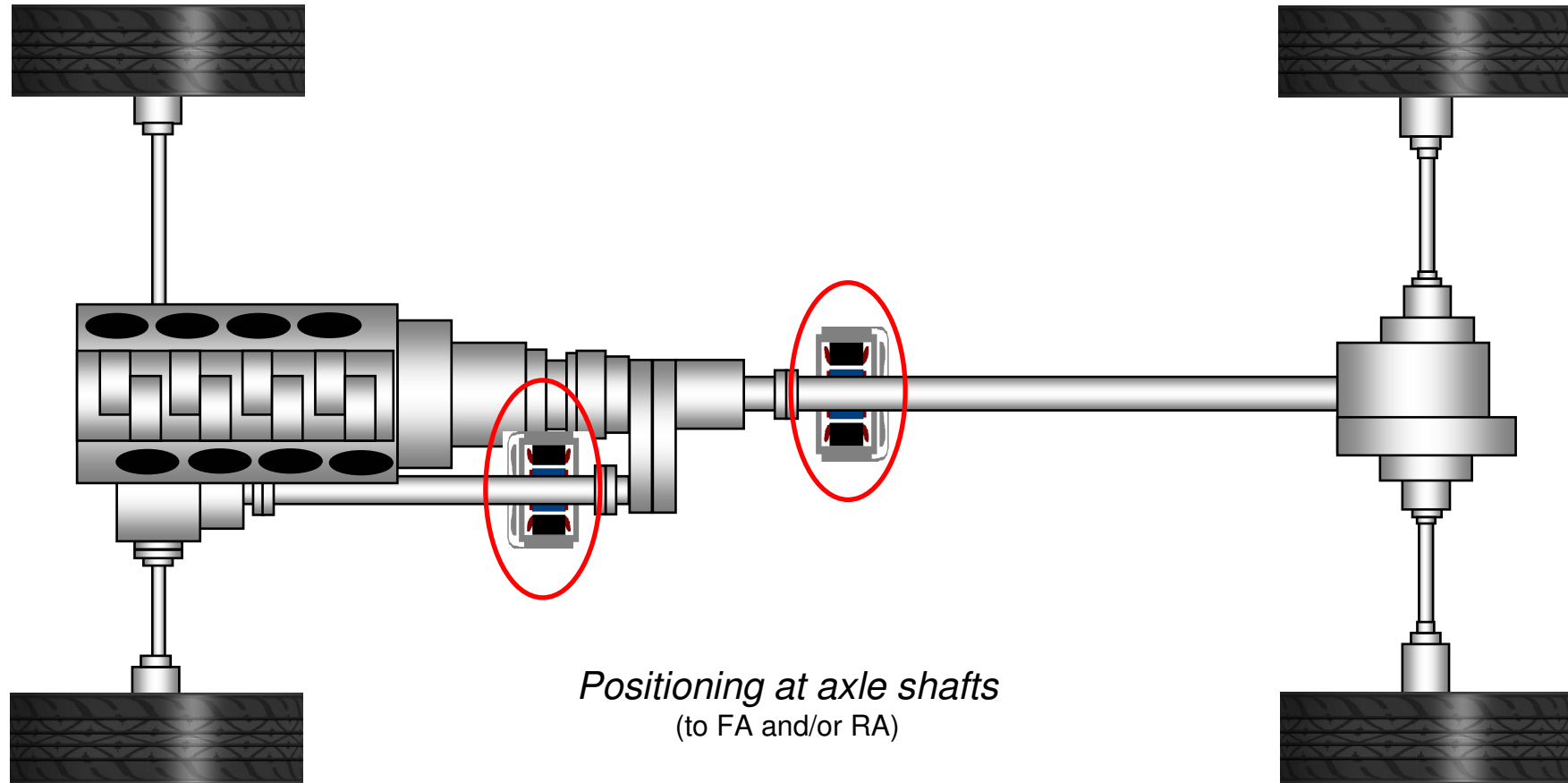


Positioning at transfer case

Quelle: vgl. VDI-Berichte Nr. 1943, 2006

Positioning possibilities

Integration of electrical machines in the powertrain

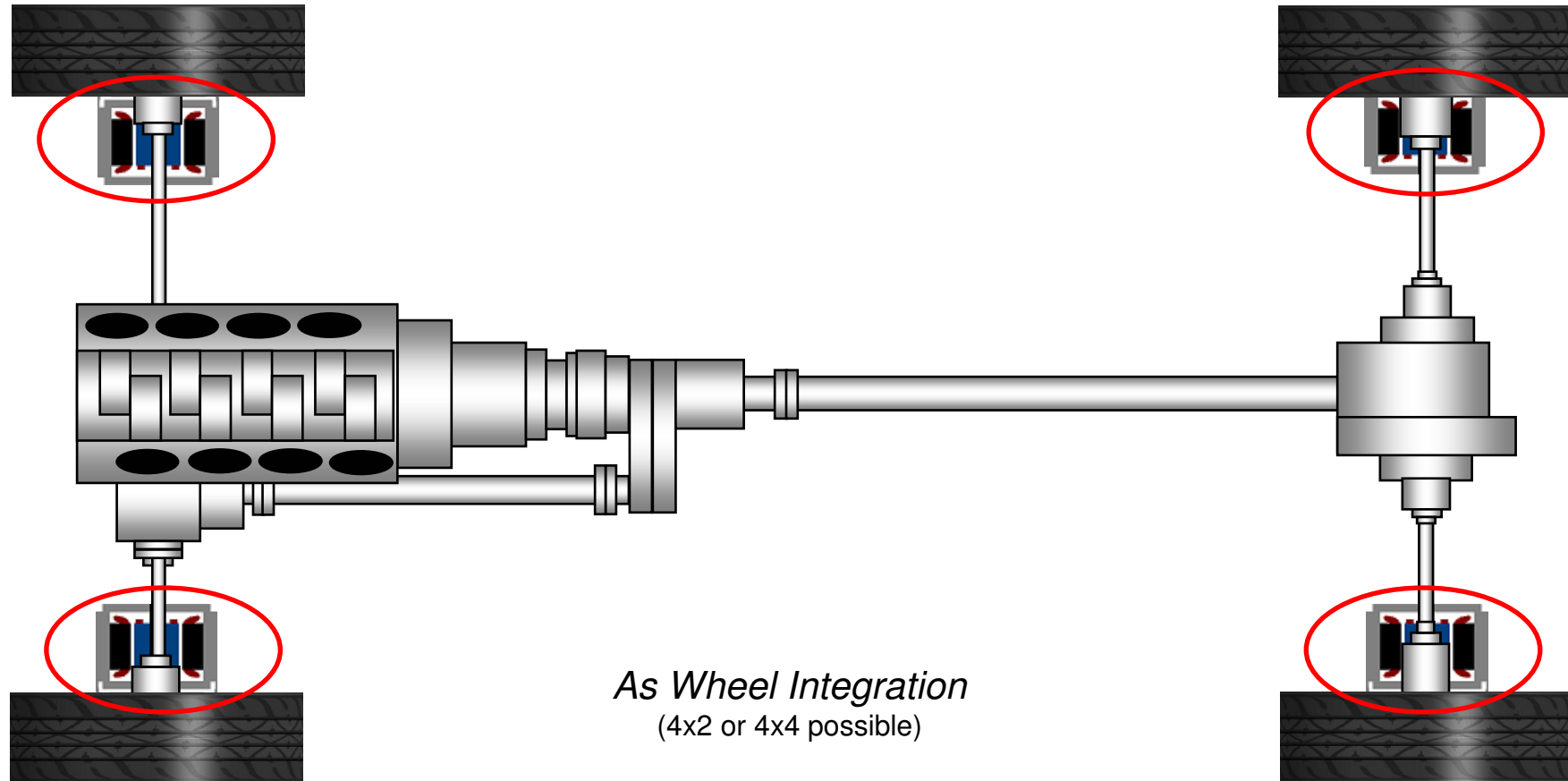


Positioning at axle shafts
(to FA and/or RA)

Quelle: vgl. VDI-Berichte Nr. 1943, 2006

Positioning possibilities

Integration of electrical machines in the powertrain

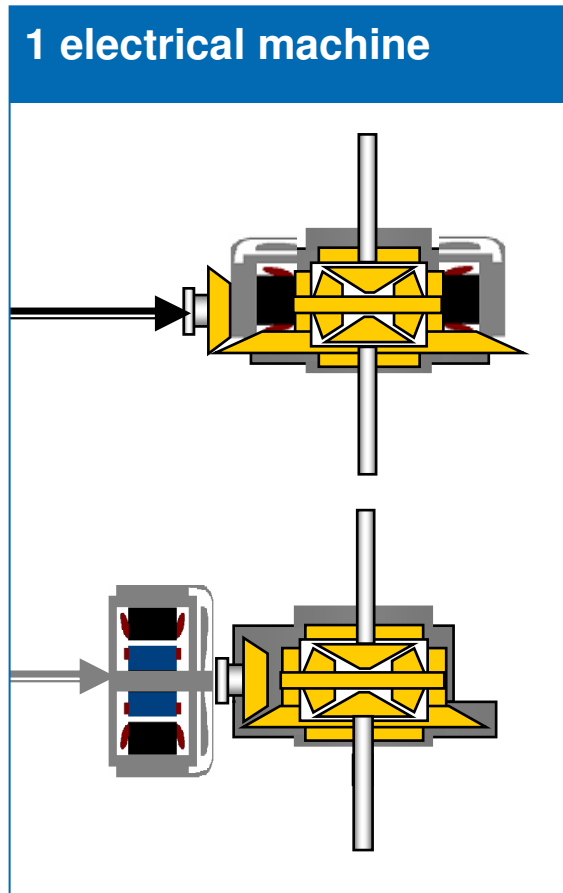


As Wheel Integration
(4x2 or 4x4 possible)

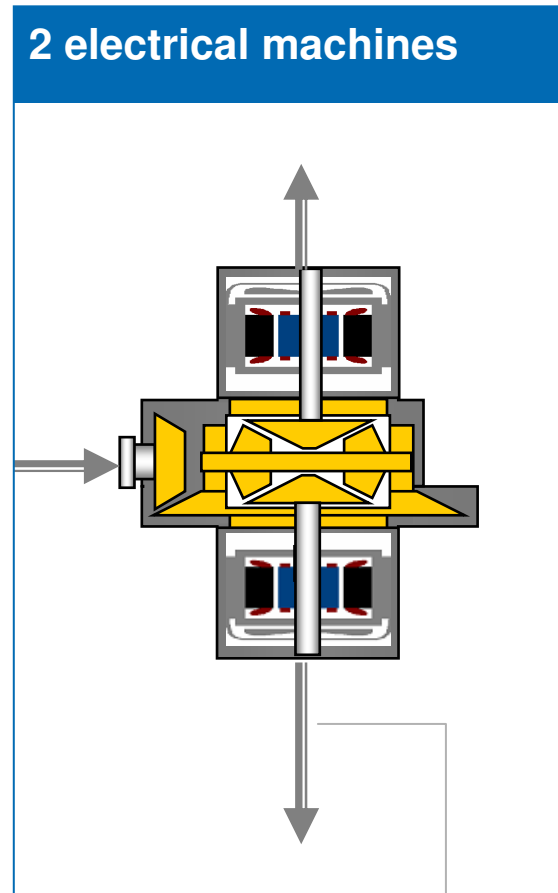
Quelle:vgl. VDI-Berichte Nr. 1943, 2006

Possible positions at the differential

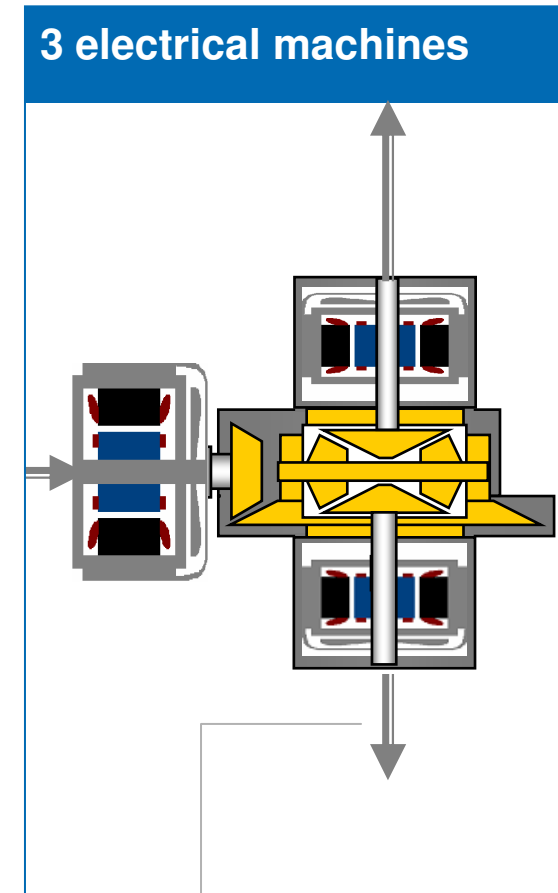
Integration of electrical machines in the powertrain



Axle Torque Support

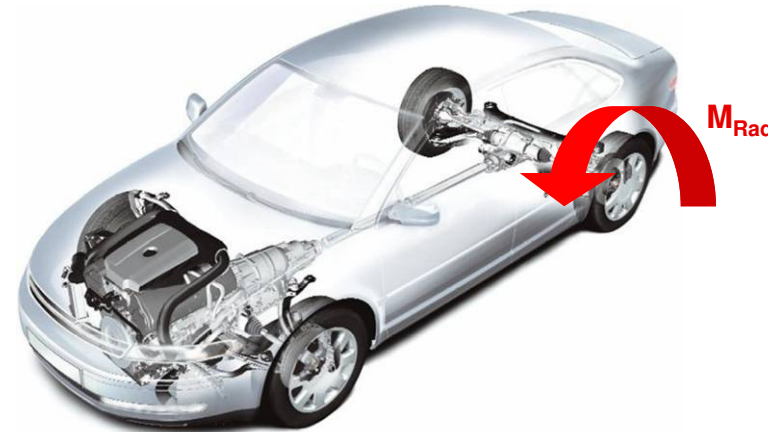
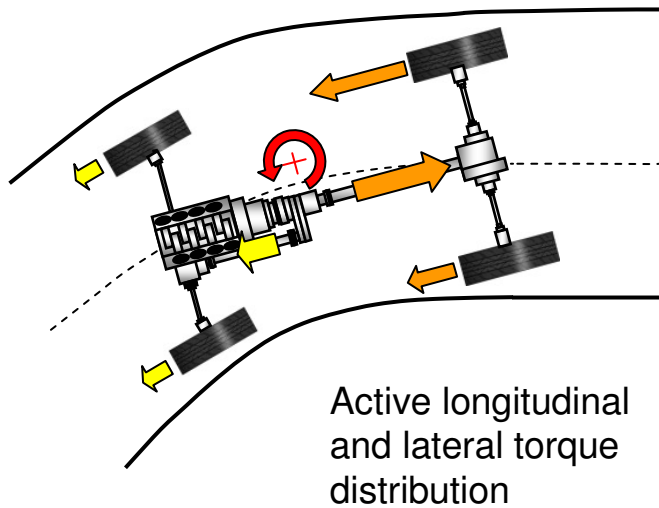
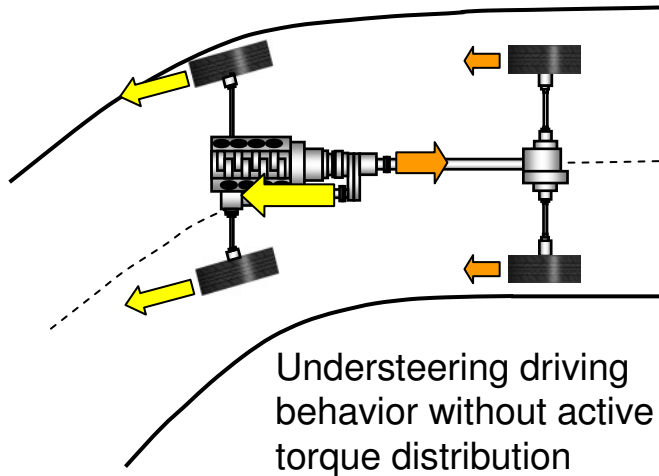


Wheel Individual Torque distribution possible



Axle differential with active torque distribution

Torque-Vectoring



Positive effect on

- Traction
- Critical cornering speed
- Self-steering response
- Handling and cornering characteristics
- Agility
- Yaw damping / yaw boosting
- Reducing brake intervention

Basic Optimization Targets

System Definition



- **Longitudinal Dynamics**
 - Optimal E-Machine Concept related to driving Cycle and performance targets
 - Optimal Battery Capacity related to driving Cycle
 - Optimal Hybrid Strategy related to driving Cycle
- **Lateral Dynamics and Driving safety**
 - Optimal E-Machine Concept and set-up for dynamic Torque Vectoring
 - Targets for mass distribution and self steer characteristics
 - Limitations to hybrid strategy under lateral dynamics
 - Necessary sub-controls for ASR/MSR and ESC Intervention

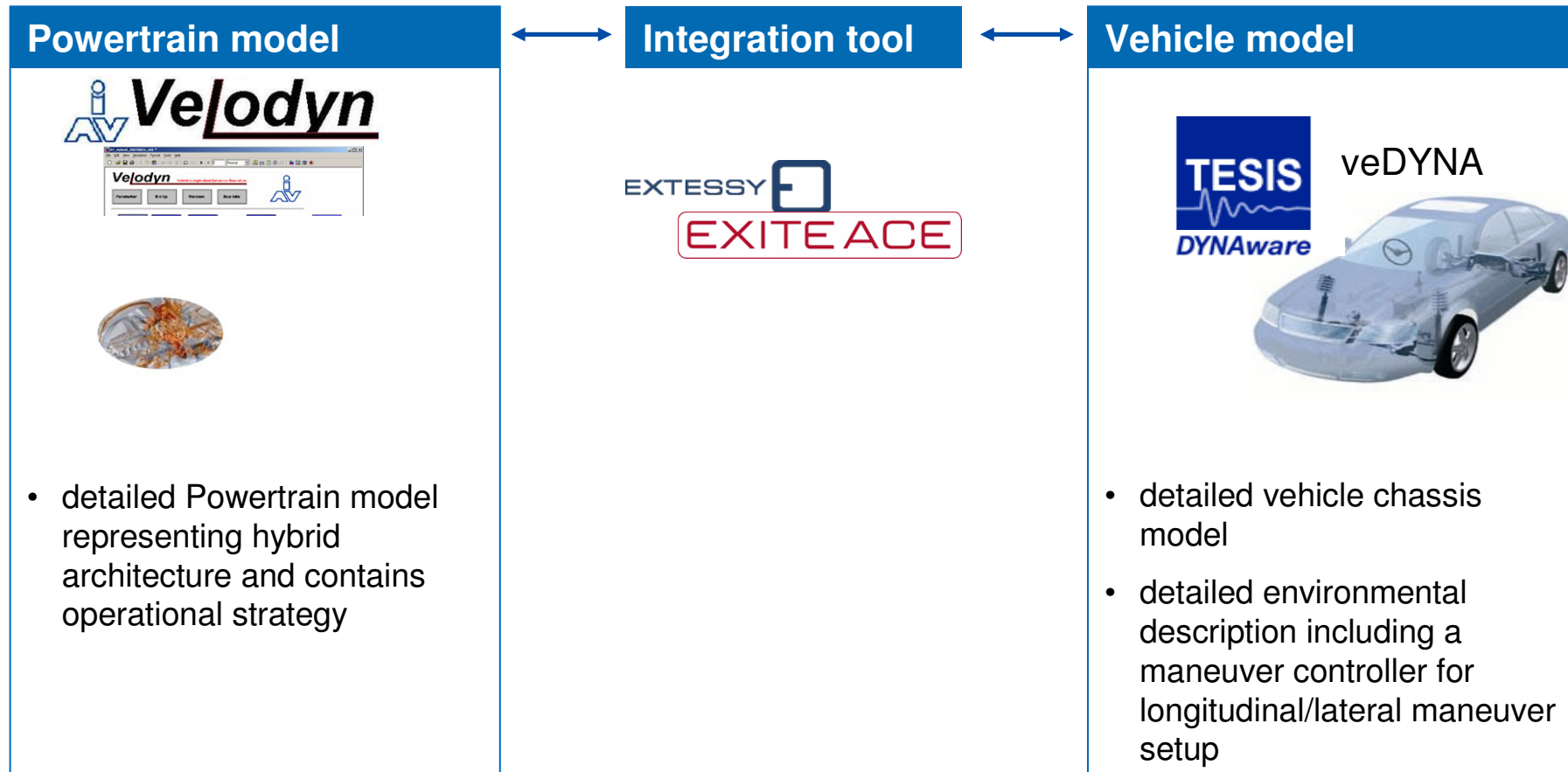
→ **Networked Simulation approach for Optimization and pre evaluation through virtual test runs**

Simulation environment

Networked simulation



Use of EXITE-ACE as co-simulation tool to connect IAV-powertrain model VeLoDyn and common handling simulation tool veDyna



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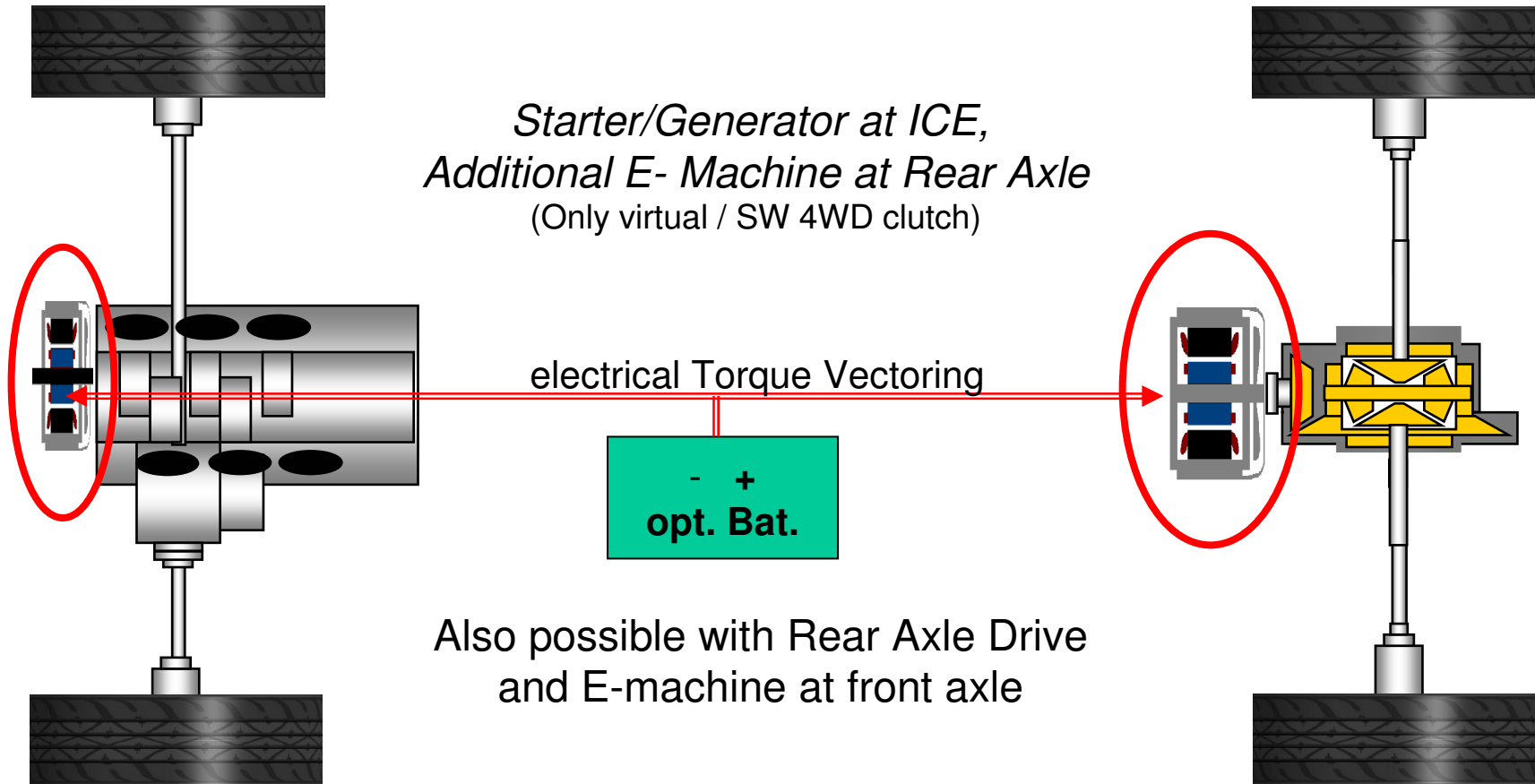
Evaluation results for longitudinal and lateral dynamics

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Summary

#1 Example, roughly equiv. to Lexus RX400h

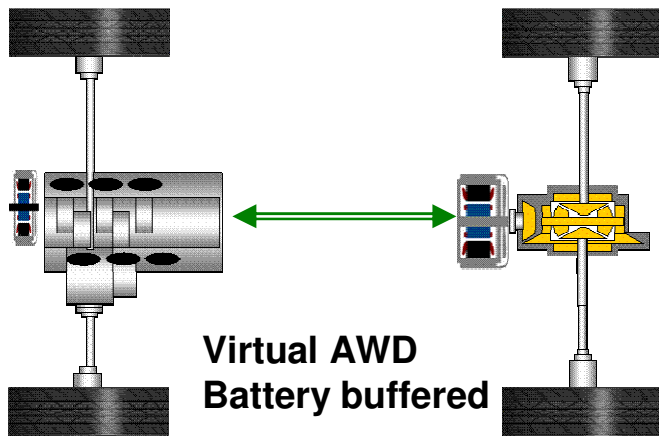
Integration of electrical machines in the powertrain



Quelle:vgl. VDI-Berichte Nr. 1943, 2006

Potential Hybrid strategy (w/ Rear Axle E-Machine)

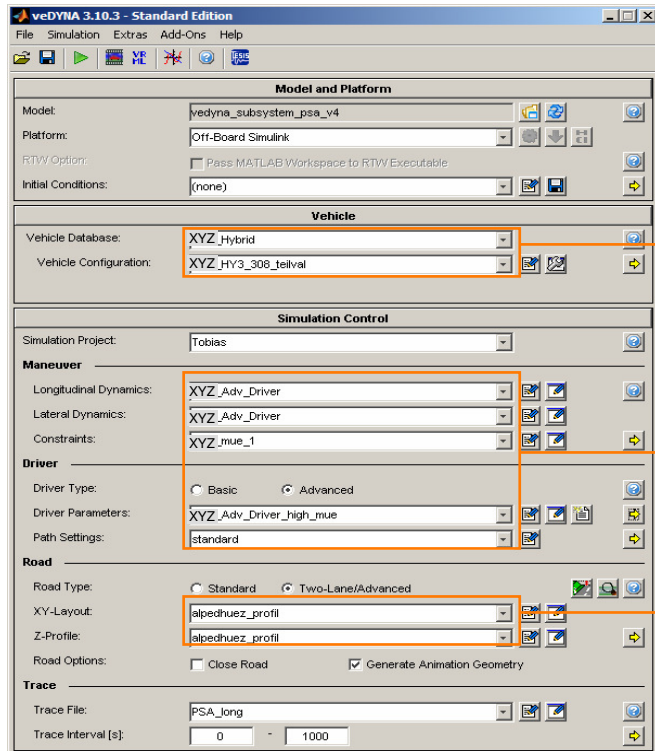
Integration of electrical machines in the powertrain



- Battery charging during normal driving
- Basic Recuperation (engine drag torque superposition)
- Brake recuperation (system blending).
- AMT shift support (boost)
- Driving with E-machine only
- 4WD-strategy and rear axle boost
- Safety strategy for:
 - Driving with E- machine in "Active Short"
 - Erroneous Torque set-point / sign
 - Slip intervention (ASR/MSR)
 - ESC and ABS intervention (e. g. under coupled inertia)

Simulation settings

3d-Alpe d'Huez simulation



Vehicle parameterization

Advanced driver settings and road conditions

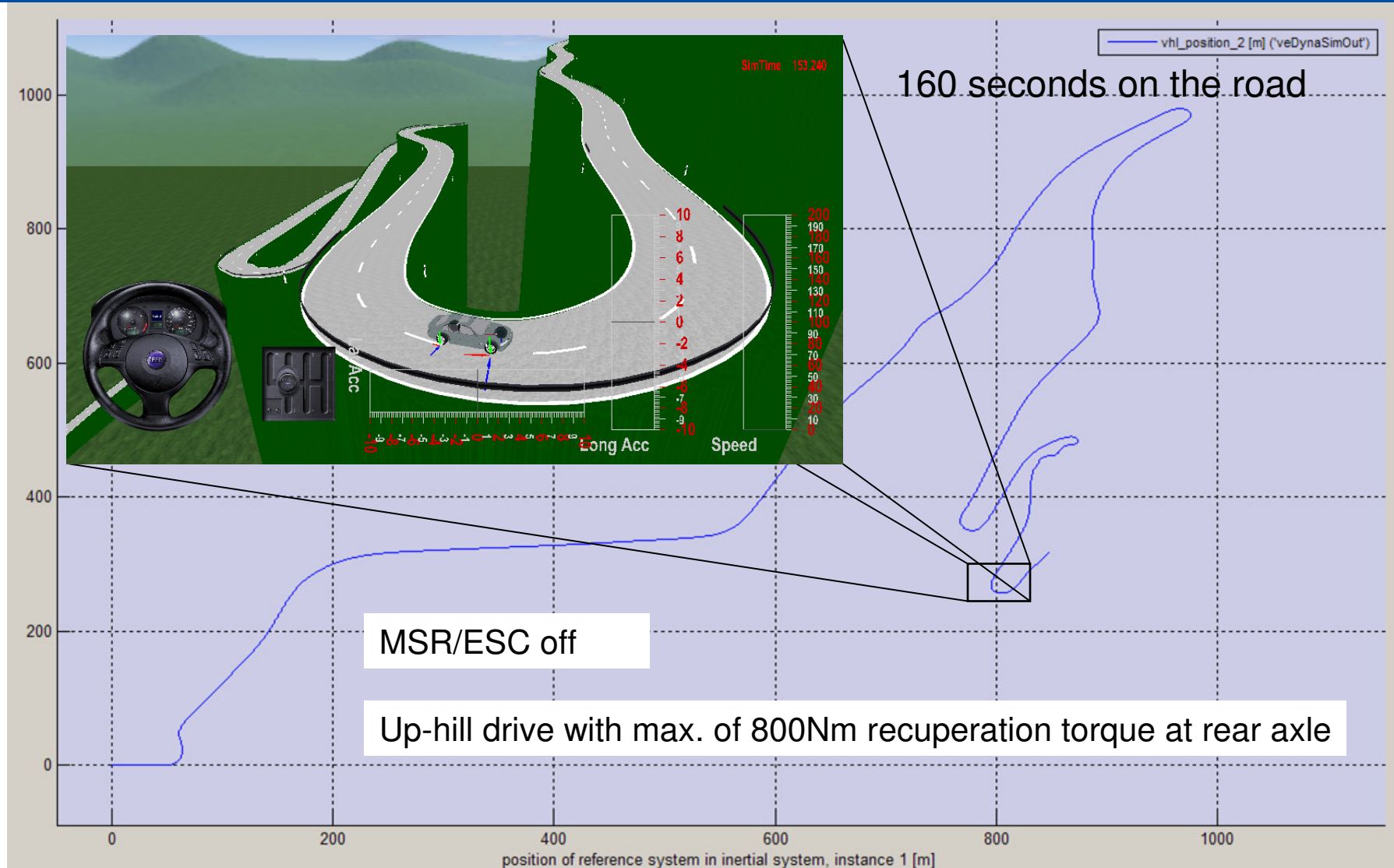
3D-Two-Lane Alpe d'Huez road profile

→ Implementation of a ASR/MSR controller by IAV

- Front and rear E-Machine scaled from longitudinal optimization
- Driver used form veDyna expect gear shifting
- All hybrid functions enabled
- SOC at start: 70 %
- 4WD torque split strategy:
 1. As much as possible with front axle, then add rear axle
 2. Permanent 4WD suport SOC dependent
- ASR on
- MSR on/off

Vehicle behaviour while regen. braking on Alpe d'Huez

3d-Alpe d'Huez simulation

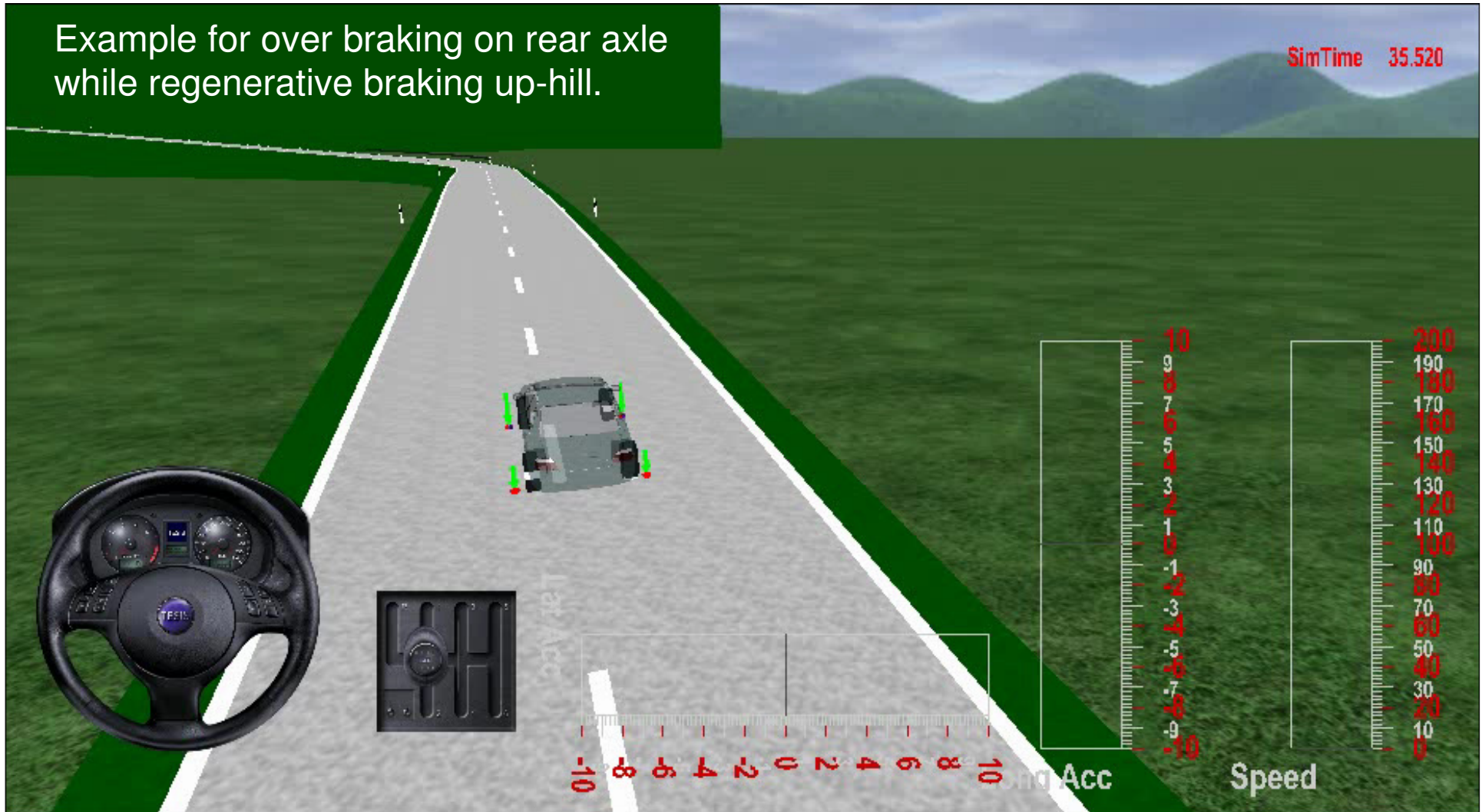


Vehicle behavior while regen. braking on Alpe d'Huez



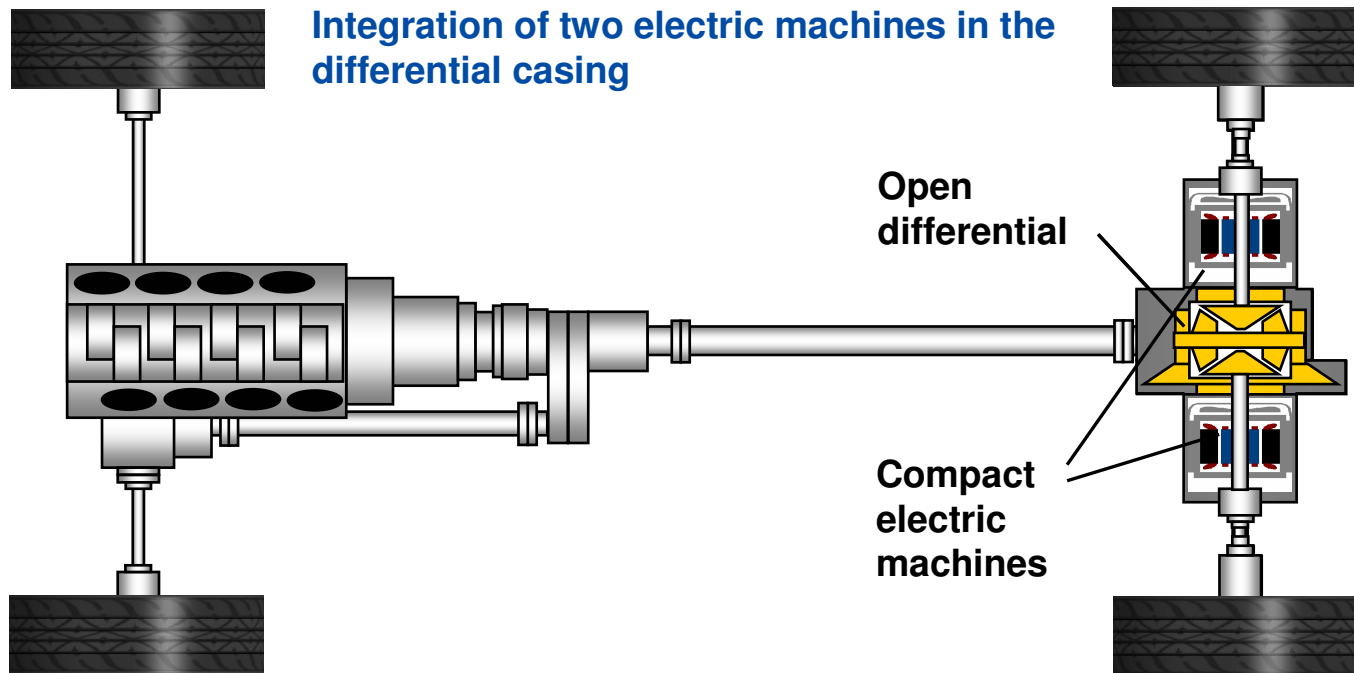
Example for over braking on rear axle while regenerative braking up-hill.

SimTime 35.520



Integration of electric machines in the powertrain

#2 Rear Axle differential with active torque distribution



Wheel-specific torque vectoring

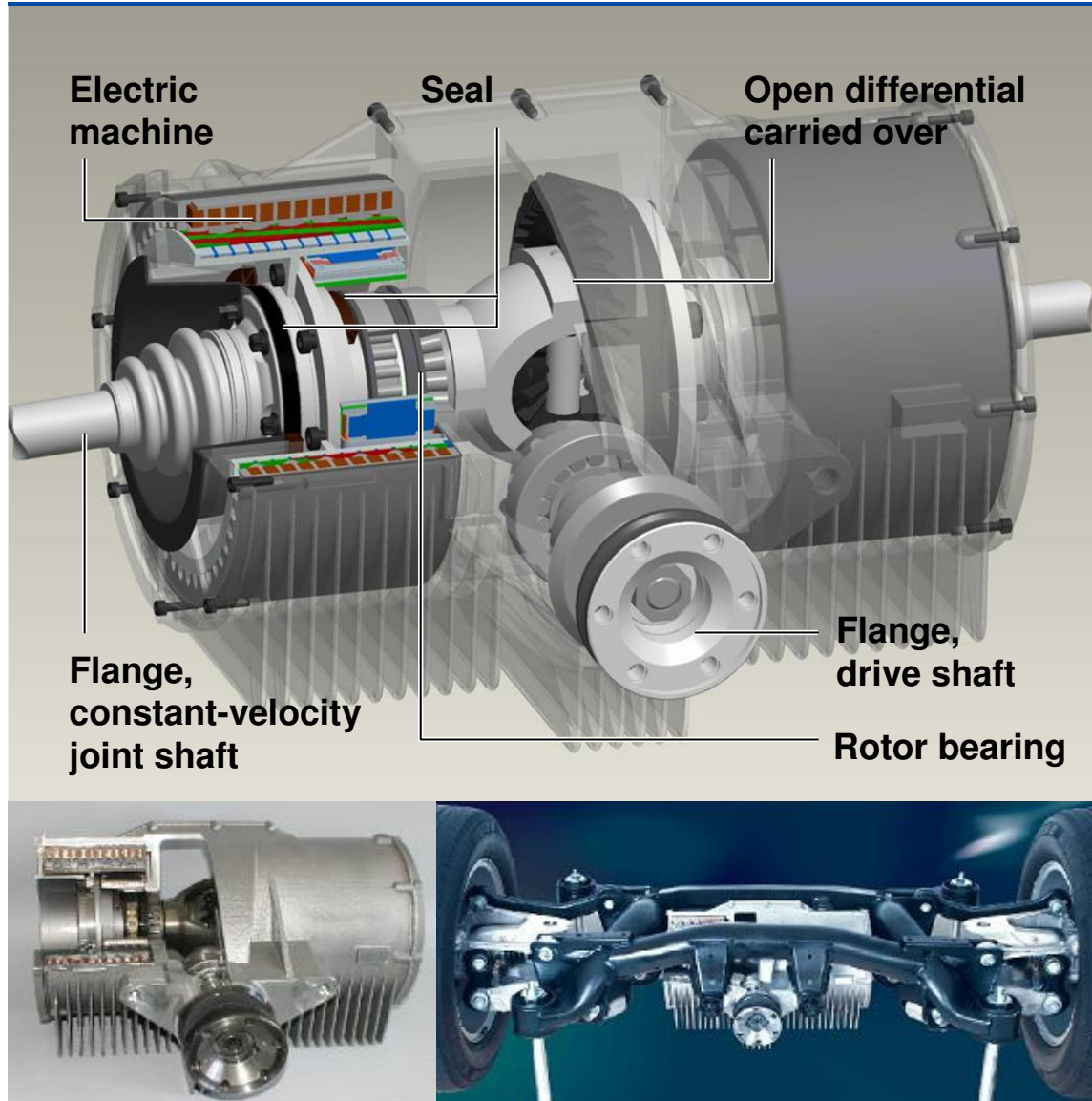
- Existing engine/transmission configurations (MT, AMT, DCT, CVT, AT) can be carried over
- Rear-axle module: supplier add-on
- Utilization of wheel-specific coefficient of friction

Using a suitable storage system

- Parallel hybrid
- Improved longitudinal dynamics
- Avoidance of traction interruption

Design of active differential

Axle differential with active torque distribution

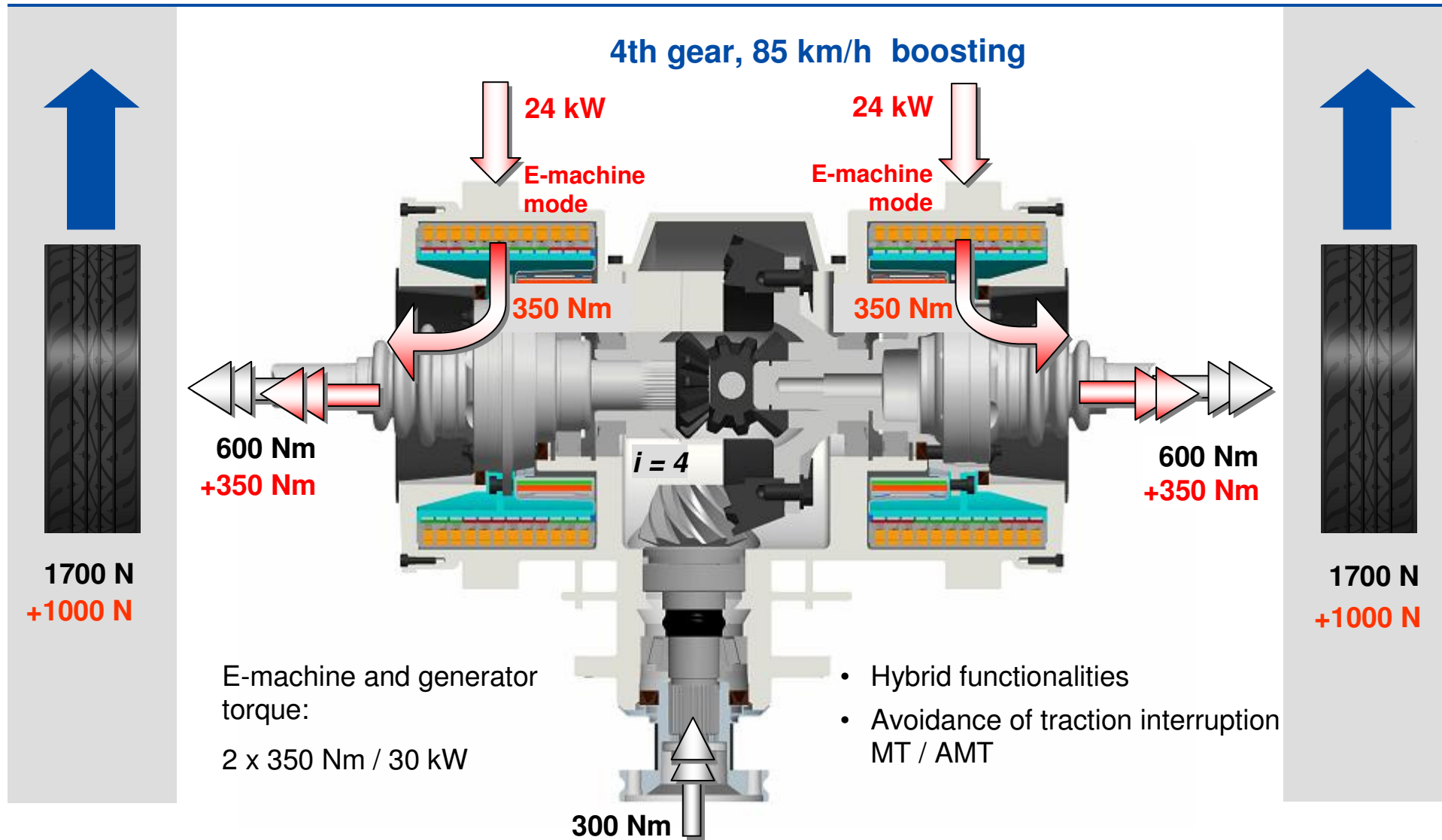


Flexibility and modularity

- Open differential
- Active differential
- ... with hybrid function
- Basis for electric axle
- Capability of integrating gear ratio
- High degree of integration for electric machine without gear ratio
- Existing mechanical structures and technologies carried over
- Low additional moments of inertia, utilization of existing package

Hybrid functionalities

Axle differential with active torque distribution

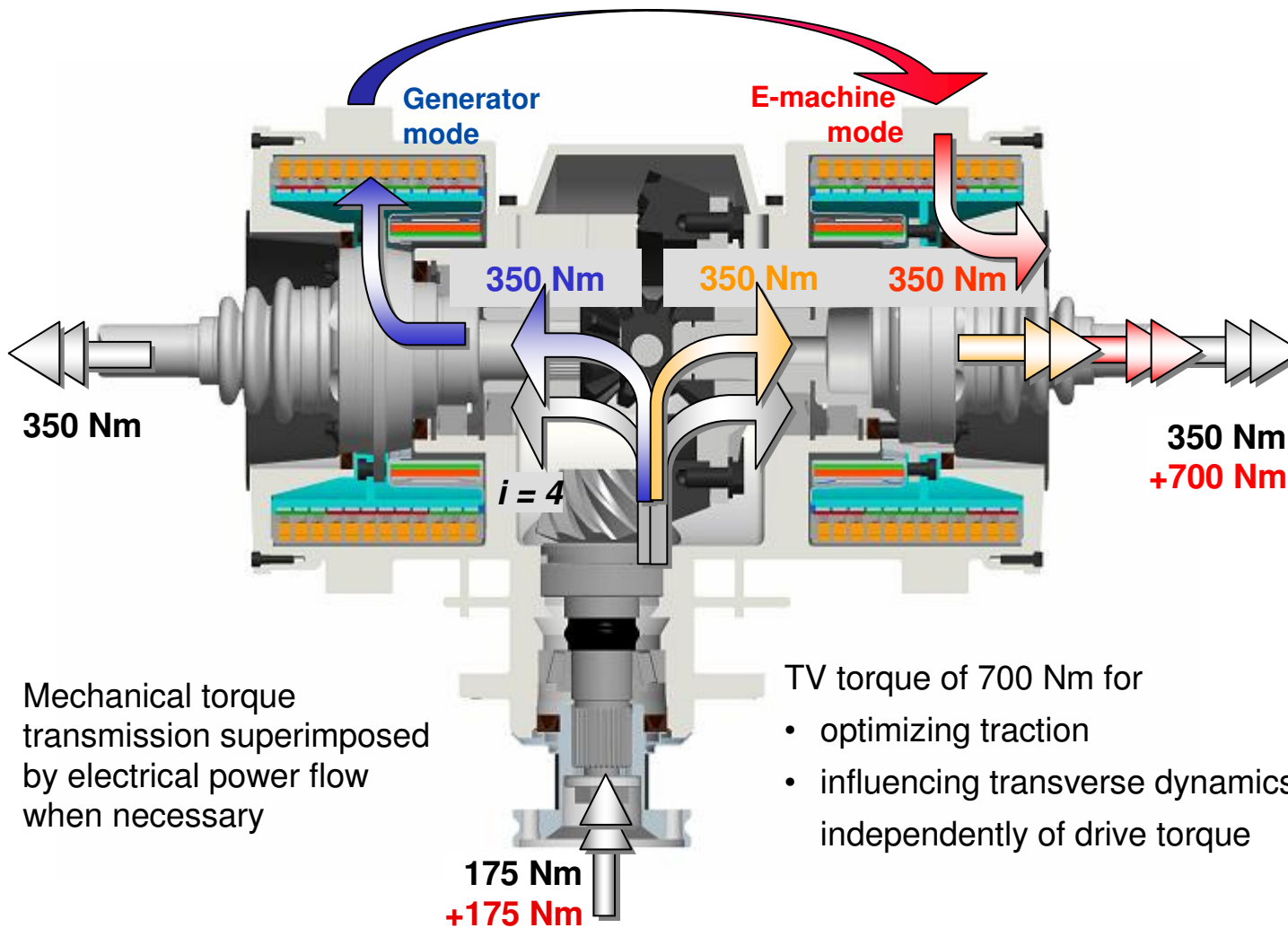


Torque vectoring functionality

Axle differential with active torque distribution



Moving off with μ -split



Mechanical torque transmission superimposed by electrical power flow when necessary

TV torque of 700 Nm for

- optimizing traction
- influencing transverse dynamics independently of drive torque

1000 N

μ low

1000 N
+2000 N

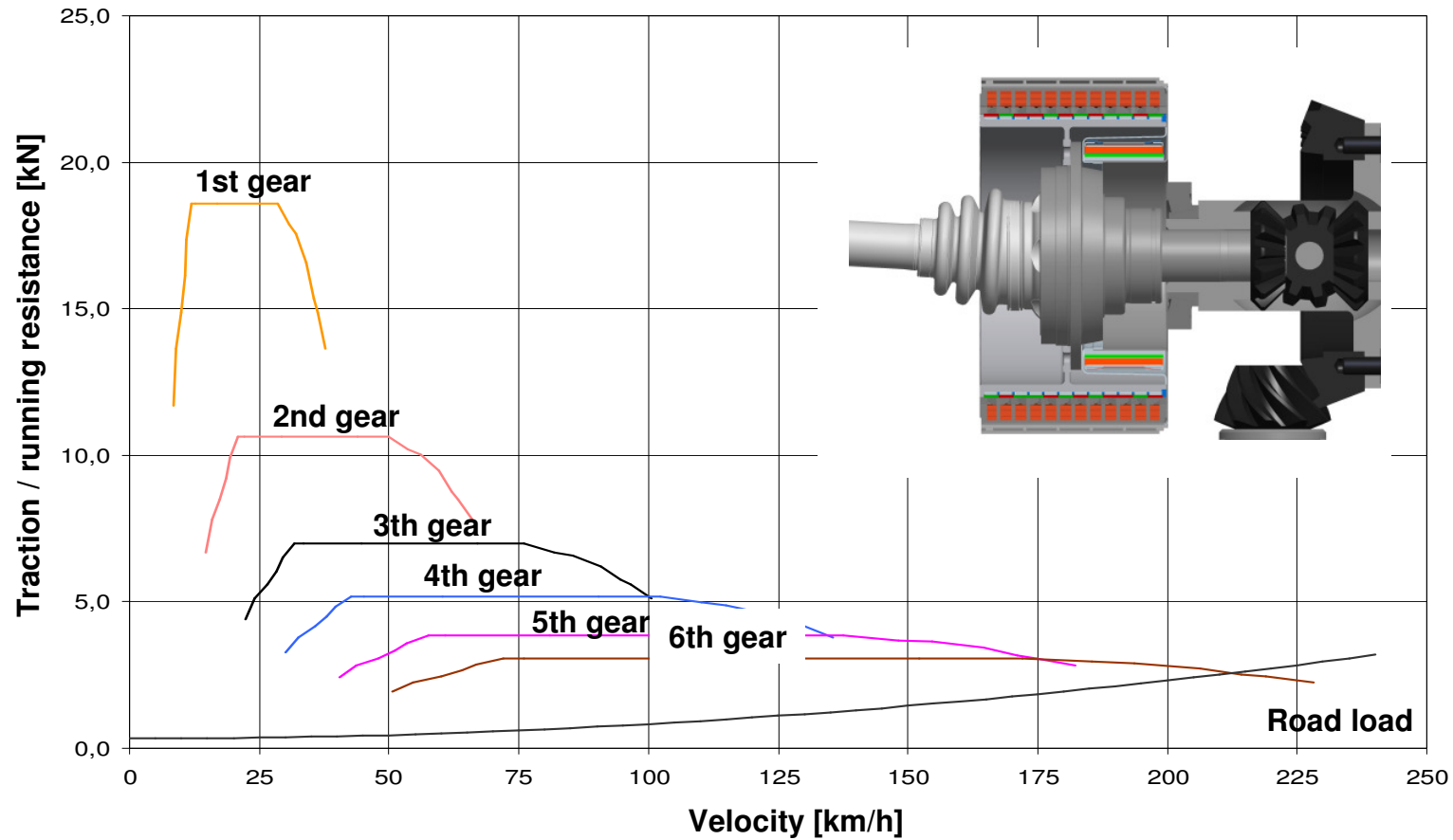
μ high

Traction potential in boosted mode

Tractive -power chart



Constant-speed driving without e-machines

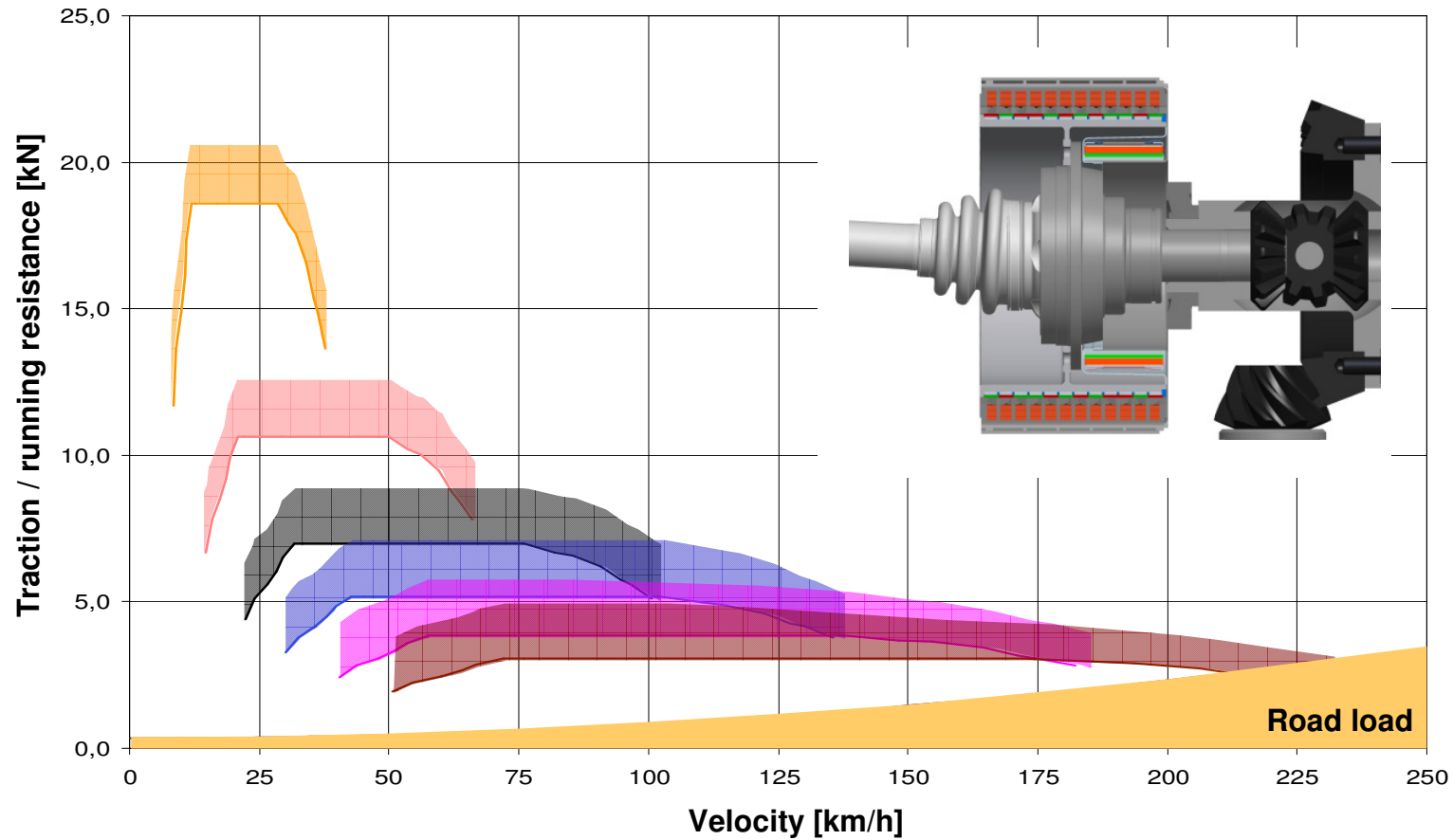


Traction potential in boosted mode

Tractive -power chart



Constant-speed driving boosted by e-machines (2 x 350 Nm)

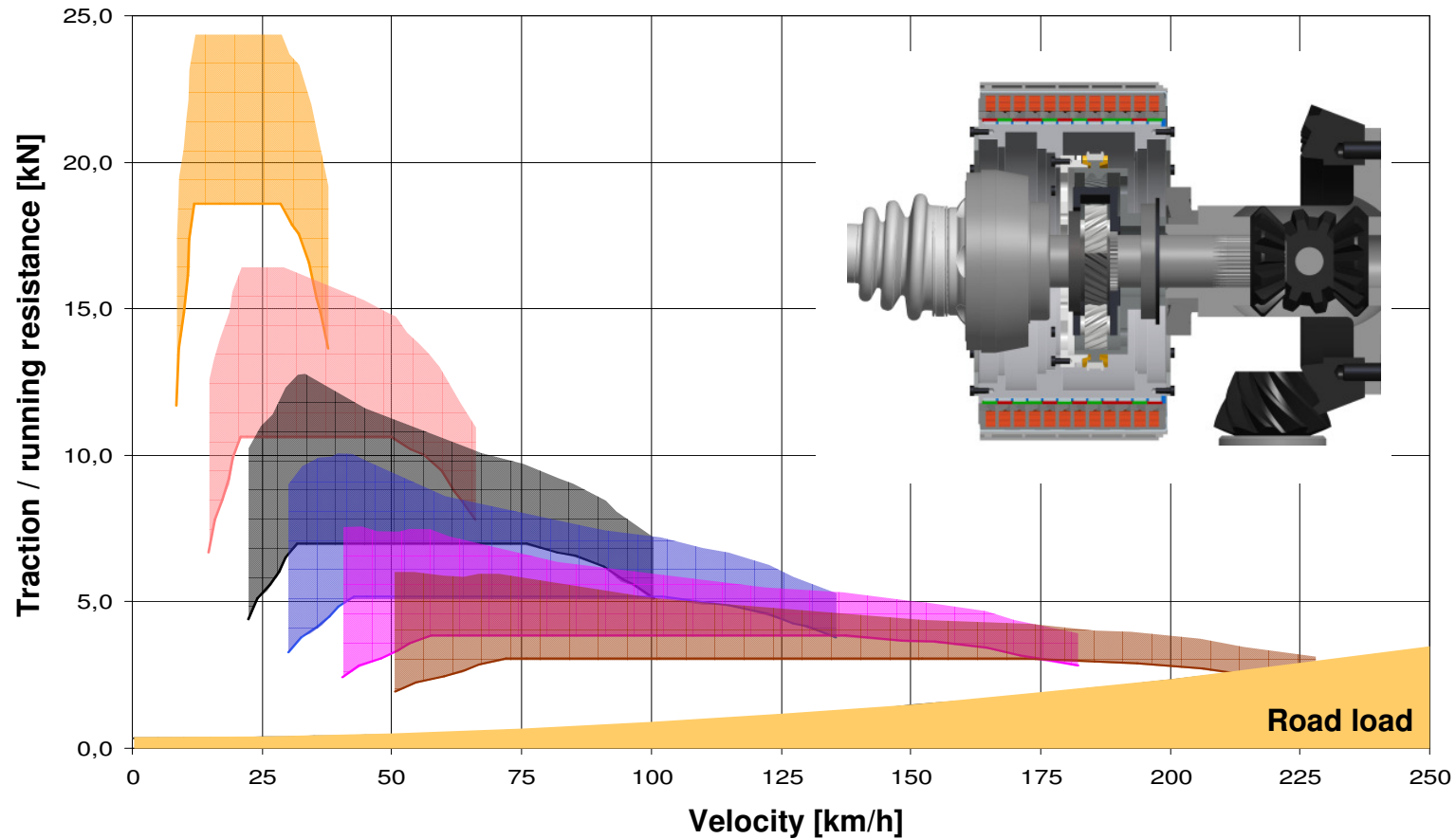


Traction potential in boosted mode

Tractive -power chart



Constant-speed driving boosted by e-machines (2 x 350 Nm) and transmission

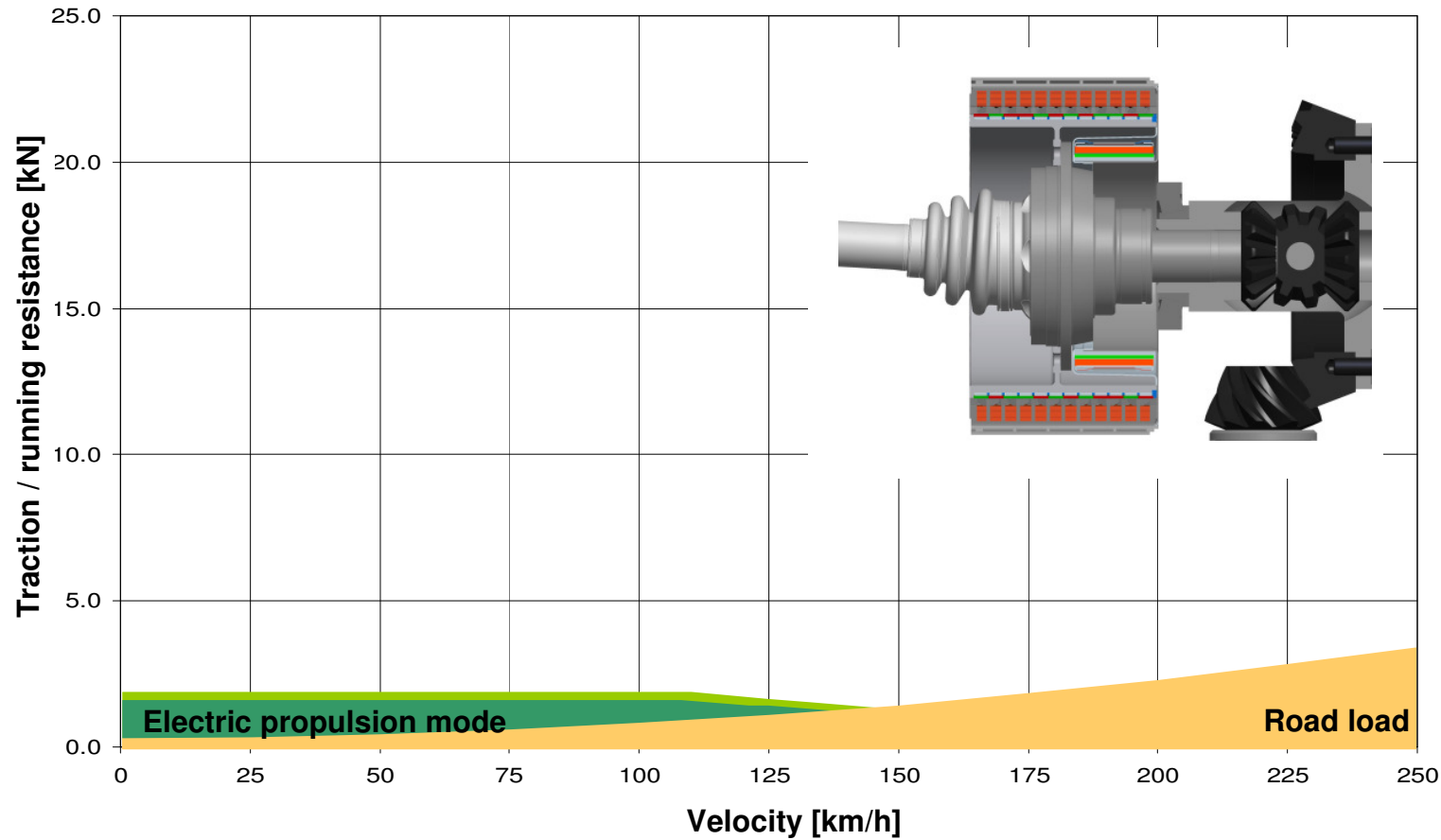


Traction potential in boosted mode

Tractive -power chart



Constant-speed driving only with e-machines (2 x 350 Nm)

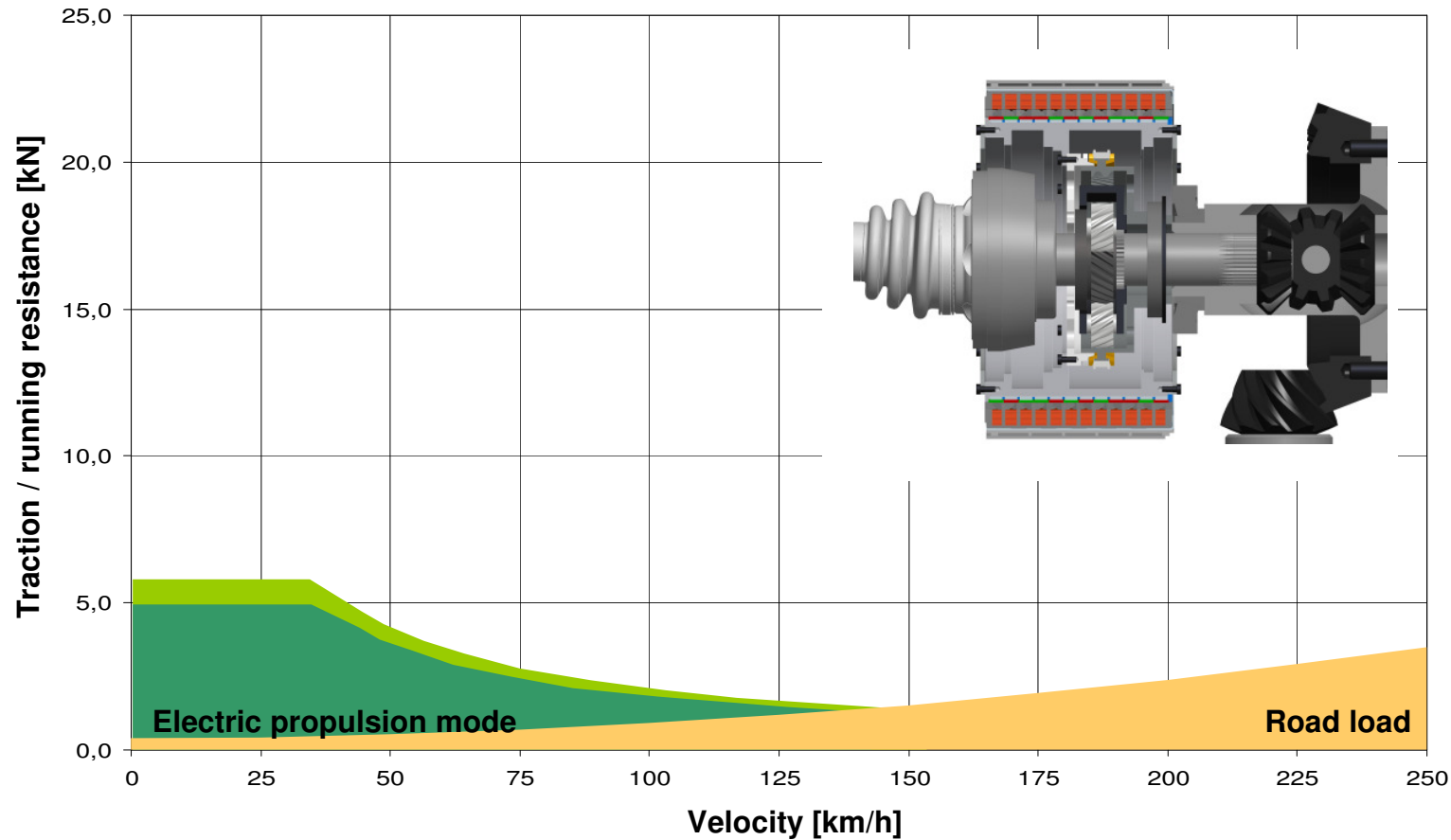


Traction potential in boosted mode

Tractive -power chart



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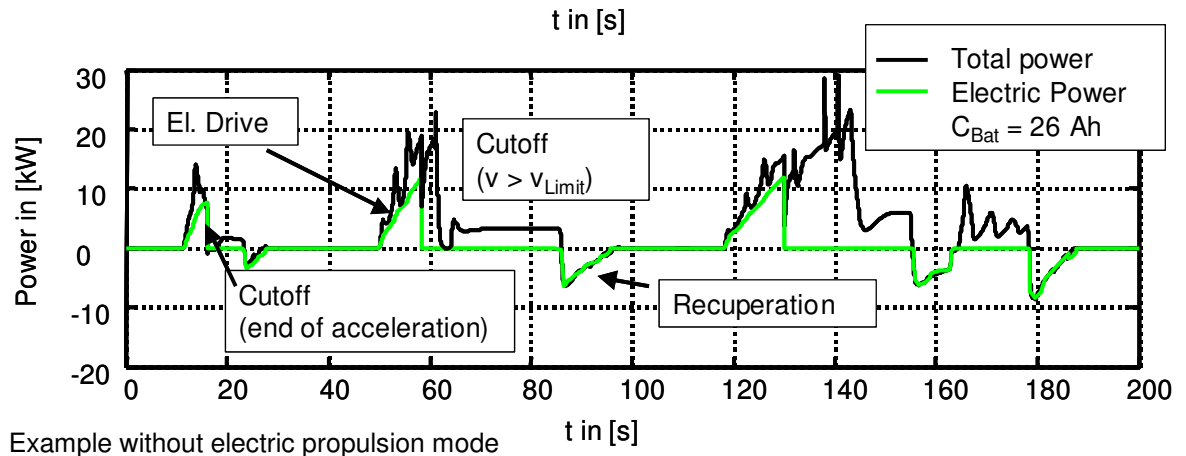
Summary

Consumption potential in the NEDC

Simulations results of longitudinal dynamics



Power component from electric machines in NEDC



Full-load acceleration

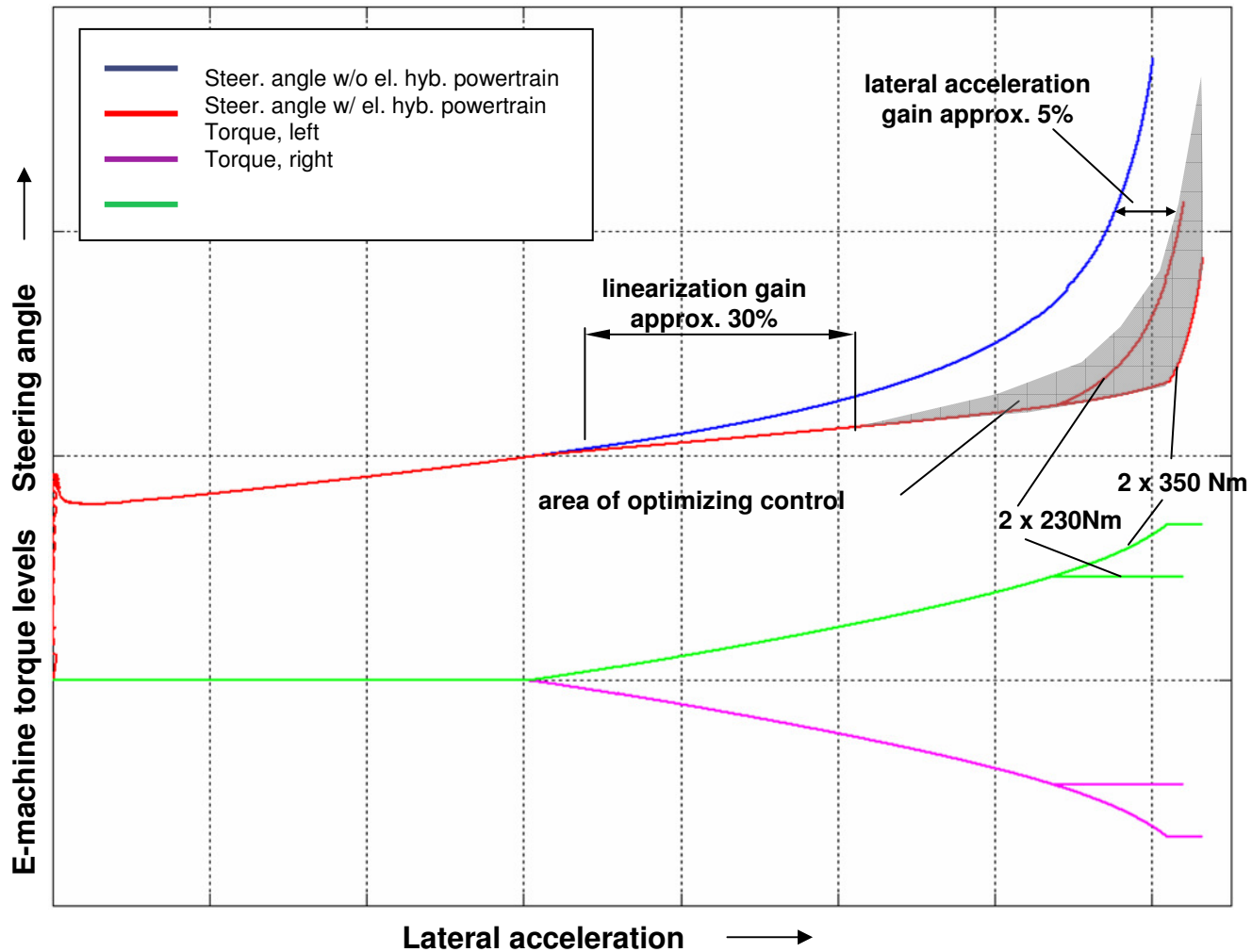
	Boosted versus conventional
Acceleration from 0 – 100 km/h	-18.9 %
Acceleration from 80 – 120 km/h	-27.7 %
Acceleration from 80 – 160 km/h	-31.6 %

Consumption in NEDC

	Start-stop	Dependent on operating strategy
Potential	- 4.1%	-9.5% to -15.5%

Wheel-specific Torque-Vectoring

Simulations results of lateral dynamics ISO 4138



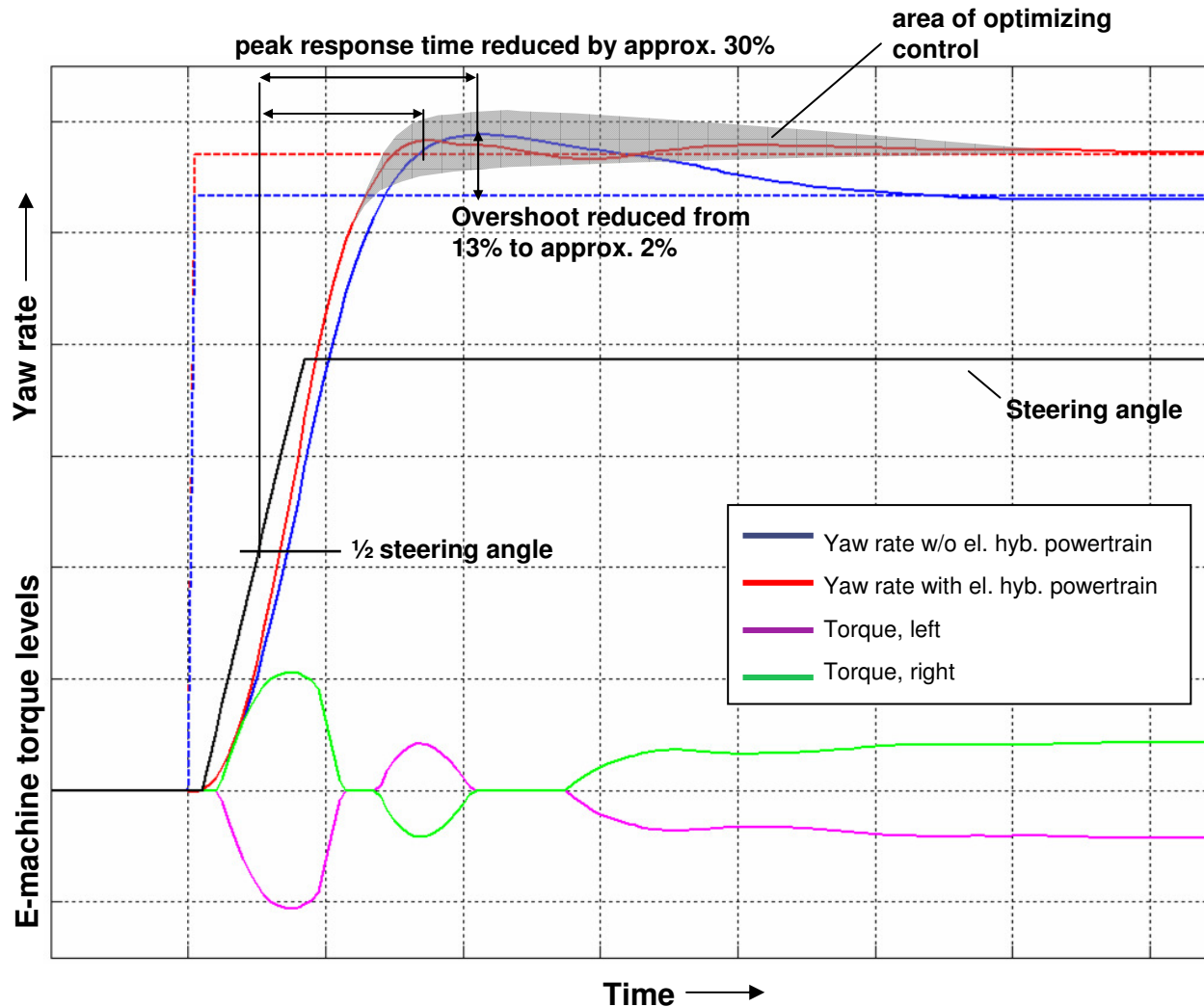
Steady-state skid-pad driving R = 100 m (test to ISO 4138)

Self-steering response impact

- predictable driving behavior also on upper lateral acceleration
- increase the speed of cornering
- possibility to recuperate transversal dynamics energy
- possibility to realize a lane keeping system

Wheel-specific Torque-Vectoring

Simulations results of lateral dynamics ISO 7401



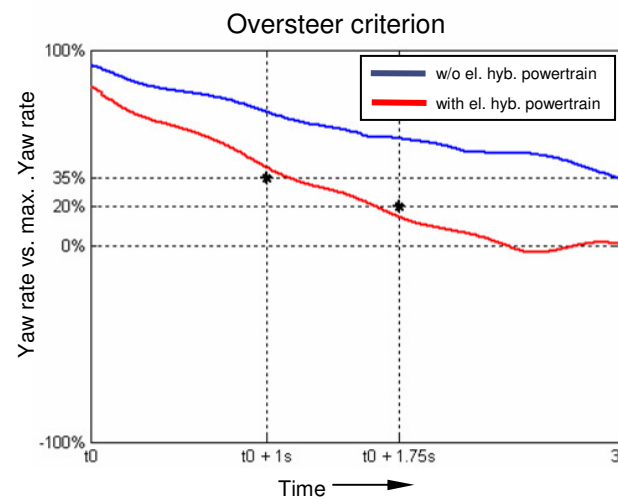
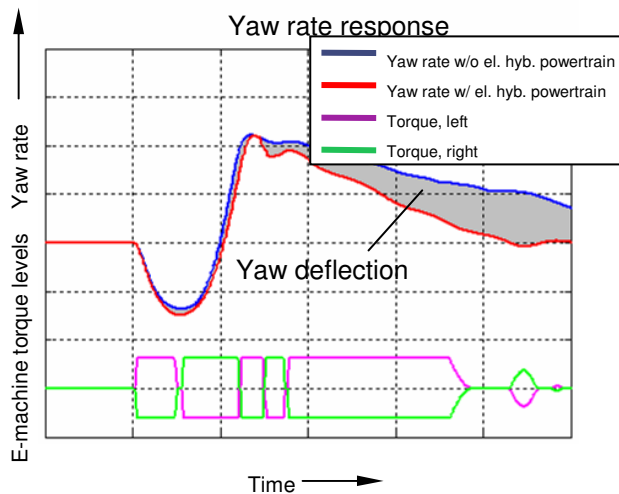
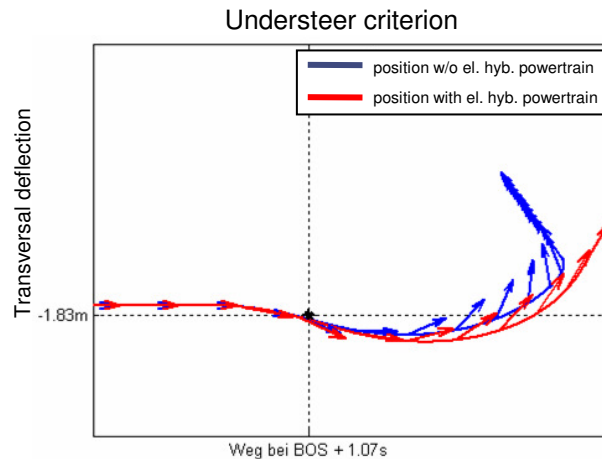
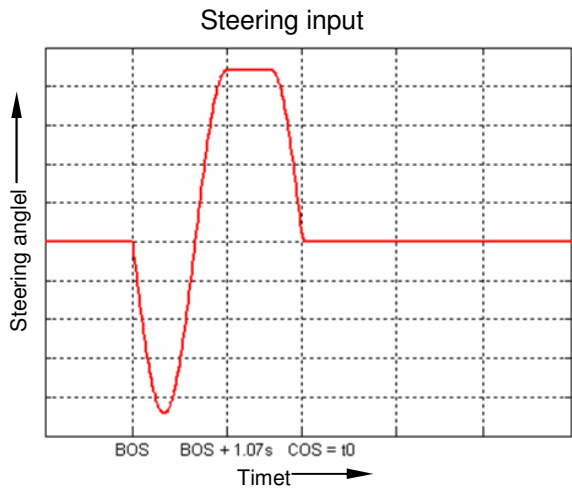
Step steering-angle change from 0 to 50° (300°/s at 80 km/h, test to ISO 7401)

Driving dynamics impact

- low response time by fast actuator speed (~10 ms)
- enhancement of steering response (yaw rate gain)
- reduction of undesired yaw rate response (yaw rate amortization)
- reduction of body motion

Wheel-specific Torque-Vectoring

Simulations results of lateral dynamics FMVSS 126



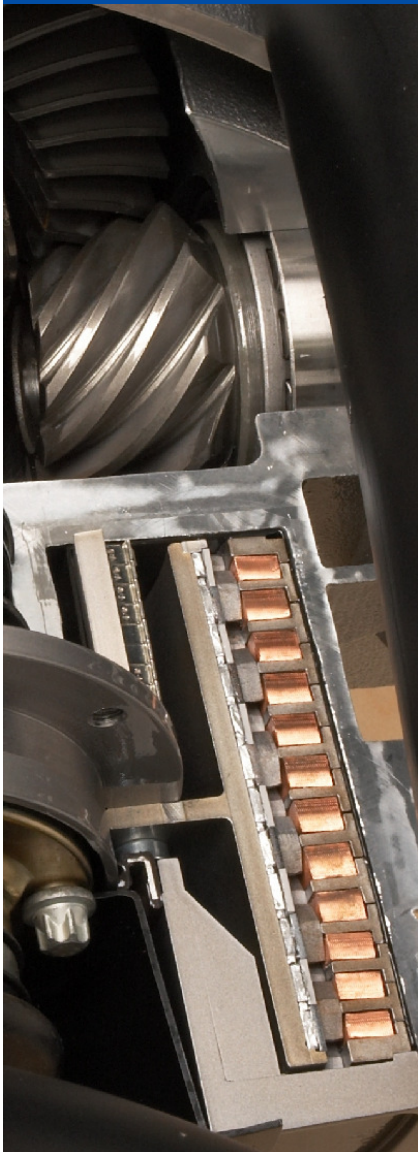
Sine with dwell for 6.5xA
(test to FMVSS 126)

Driving stability impact

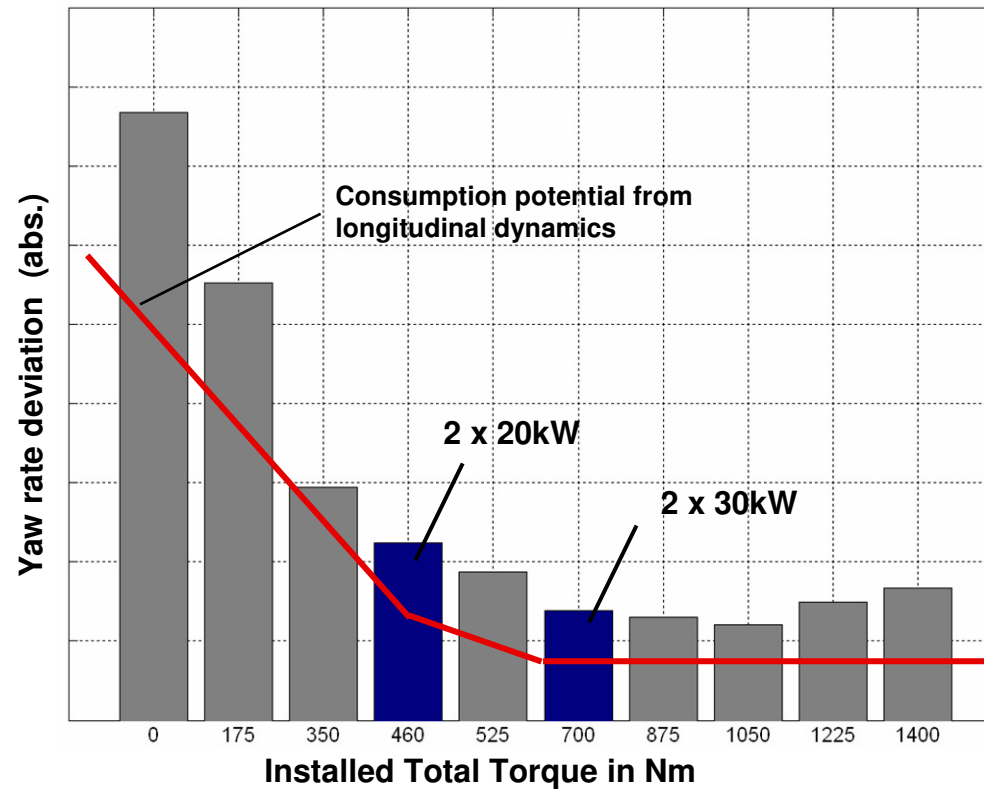
- impact of tracking stability
- vehicle stabilization without braking
- increase of driving dynamics by pre controlled intervention



Torque-Vectoring and Hybrid Combined system layout optimisation



Influence of additional torques for stabilizing potential Based on: FMVSS 126 at max. steering angle amplification



Simulated Vehicle category: SUV, (not fully verified)

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Hybrid control with active torque distribution



Positive effect on longitudinal and lateral dynamics

- Assist cornering behavior and vehicle stabilization
- Offer traction optimization, boost function and shift support at MT and AMT

Parallel hybrid

- Electric machines provide the basis for hybridized powertrain

Benefits of electric machines direct at the differential

- Use of existing engine/transmission configurations
- Integrative, flexible and modular solution
- Very short control response time to provide the demanded driving dynamics intervention

Drawbacks

- Additional costs and weight related to standard TV
- Advanced control necessary

Thank you

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