

Simulation based Power Steering Hose Design and Optimization

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COMPETENCE IN FLUID POWER SYSTEMS SIMULATION
KOMPETENZ IN DER SIMULATION FLUIDTECHNISCHER SYSTEME

Table of contents

- 1 Introduction**
- 2 Current situation of hydraulic pipe and hose simulation
- 3 Development of a library for flexible hose elements
- 4 A development methodology for automotive lines
- 5 Presentation of example lines
- 6 Summary

FLUIDON a spin-off of the RWTH Aachen



IFAS, Expansion Building and Conference Room



Areal View of IFAS

Historical Highlights of IFAS - Institute for Fluid Power Drives and Controls

As nationally and internationally recognized research institution, the IFAS is and has been pioneering many developments in Fluid Power technology.

60's: Beginnings of servo hydraulics, fluidics

70's: Basis of cavitation research, servo pneumatics, pump controlled systems

80's: Digital control, development of DSHplus (simulation tool), proportional / directional control cartridge valves, secondary control

90's: Pre-compression chamber in piston pumps, fuzzy control, bio fluids, piezo technology, sealing engineering (blow-by effect)

present: Coating technology, condition monitoring

The Institute's Development

1968: IFAS is founded as "Institut für hydraulische und pneumatische Antriebe und Steuerungen" - IHP in short. Under Professor Backé's direction, two academic and six non-academic staff members are employed in the very beginning.

1977: The Institute now moves into its own large experimental hall with attached office building in the RWTH Expansion Area Seffent-Melaten. Now, there is room for about 50 test-stands, workshops, laboratories, computer rooms and a library.

1994: Concurring with the succession to the direction of the Institute and to the professorship by Professor Murrenhoff is the change of the Institute's name. Today, about 25 academic staff members, 20 non-academic employees and approx. 40 student assistants are working under the grammalogue IFAS. **Founding of FLUIDON as Spin-Off**

1998: Opening of the expansion building which offers additional space for offices as well as computer, seminar and conference rooms thus giving more capacity for R&D tasks.

Laboratory and test rig recourses at IFAS

IFAS disposes two experimental laboratory buildings which are equipped with workshops and laboratories and give excellent opportunities to deal effectively with R&D tasks. The newest measuring technology for all fluid power values is available.

- floor space about 1250 m² room for approx. 60 test rigs
- 2 clamping beds (5 x 3m), 70 ton foundation, 2 clamping beds (3 x 2.5m)
- 5 sound proof closets, 35 ton foundations
- anechoic room for sound measurements, (6.5 x 8m), drives 200 kW
- passable climatic test room (4.75 x 3.3 x 3m),
-70 °C to +70 °C, 20% to 95% relative humidity
- valve test stand max. 315 bar
- max. 500 l/min. ageing test rigs
for hydraulic fluids tribo tester

Laboratory Building 2



Laboratory Buildings 1

1

Introduction

2

Current situation of hydraulic pipe and hose simulation

3

Development of a library for flexible hose elements

4

A development methodology for automotive lines

5

Presentation of example lines

6

Summary

Thematic introduction

- The inside noise level of a vehicle represents an essential decision feature for the purchase decision of the customer. To satisfy this consumer expectation, it is nowadays extremely important that a potential source of noise, vibration or harshness (NVH) is identified and eliminated as early as possible in the development process.
- A known source for noise which can lead to NVH problems within the vehicle is the fluid-borne noise, issued by the pump of the hydraulic power steering. Currently the design and optimization of power steering hoses is mainly done by costly hardware tests.
- The adaptation of the automotive hose lines requires a high effort since hardware prototypes are optimized up to the desired maturity degree by means of test rig or vehicle tests. Without the amplified use of CAE tools a cost optimal development on schedule of new automotive hose lines in future can be only handled with difficulty.
- What was missing till now, for a time-domain-based simulation, were suitable models for the flexible hose parts. As a result of the cooperation of FLUIDON GmbH and a manufacturer of automotive hoses these models are available now and a simulation-based development methodology for automotive lines can be presented.

Simplified consideration of hose wall compliance

Vereinfachte Berücksichtigung der Schlauchwandnachgiebigkeit

1. The combination of rubber material and cord netting of the hose is responsible for a viscous-elastic behavior that determinates its damping characteristics (Figure 1).
2. The reinforcement material has either a more linear (steel braiding) or viscous-elastic (polyamid yarn) behavior. Due to the relative movement between the reinforcement layers there is moreover a static friction (coulomb friction) in the hose sleeve, which affects the damping characteristics as well. Some literature sources propose linear/viscoelastic damper models that are in a series connection to represent the reinforcement layers (Figure 2).
3. Up to now there is no physical model available that describes such behavior. However there are some approaches available that use measured material properties for simplified replacement models (Figure 3).

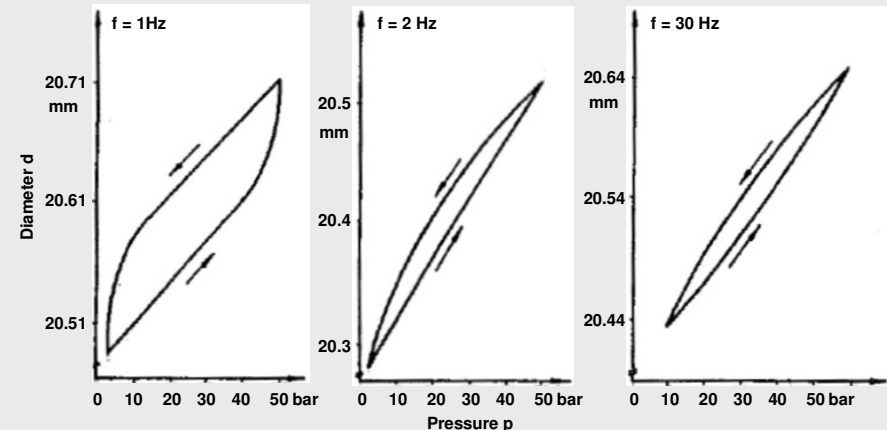


Figure 1

Hose Wall Dynamic at 1Hz, 2Hz, and 30 Hz
(Diss Sanger, IHP, Aachen, 1985)

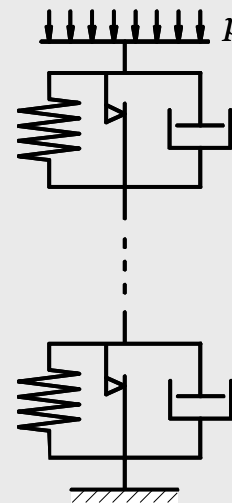


Figure 2

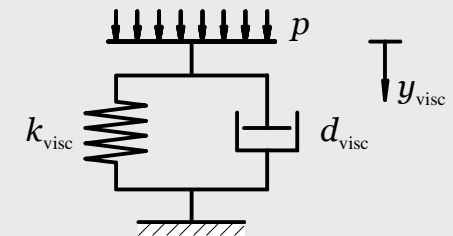
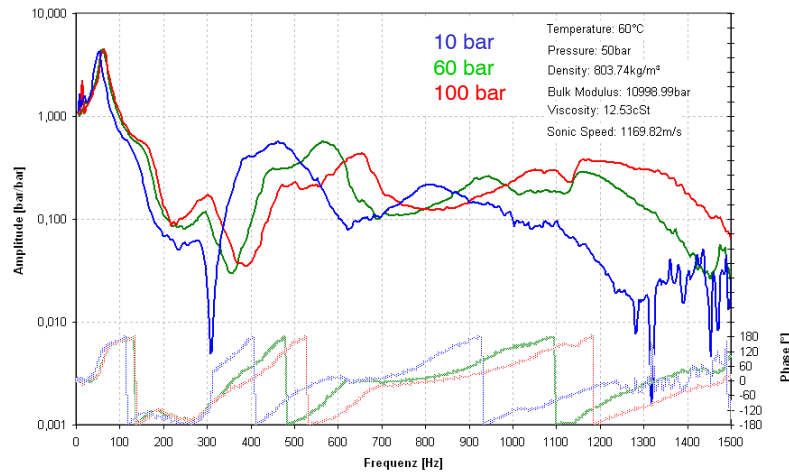


Figure 3

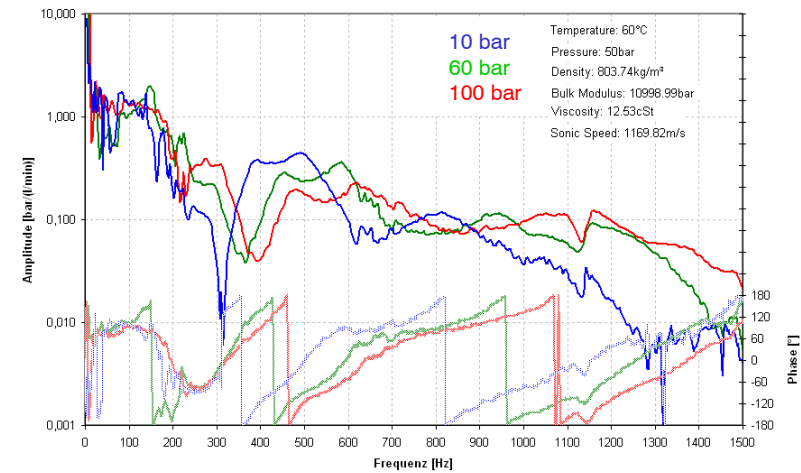
Pressure variation of an one-chamber hose line at 60 °C

Druckvariation einer Ein-Kammer-Schlauchleitung bei 60 °C

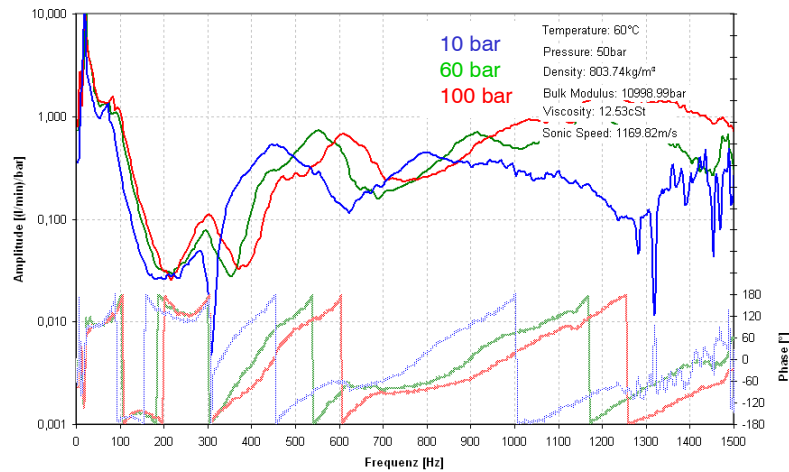
T11



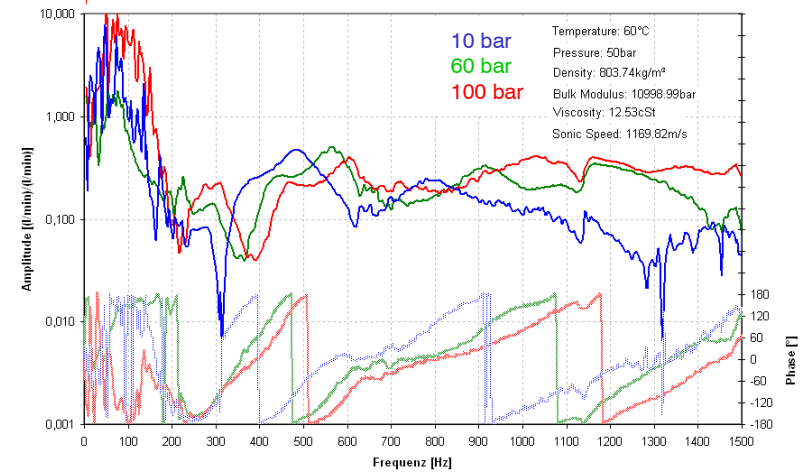
T12



T21



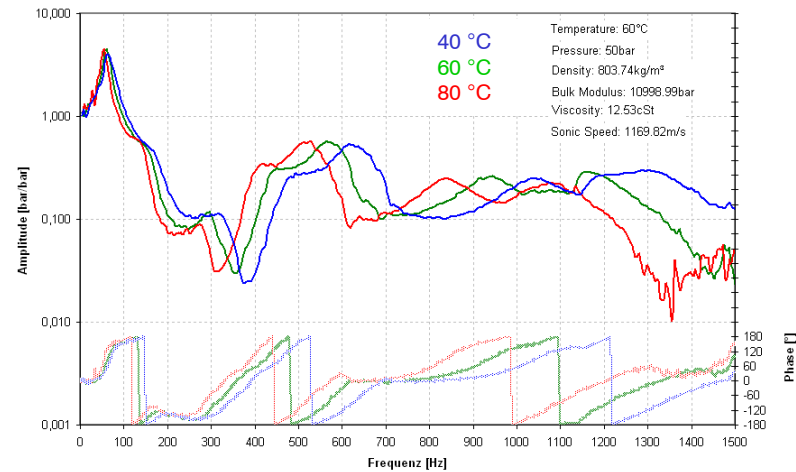
T22



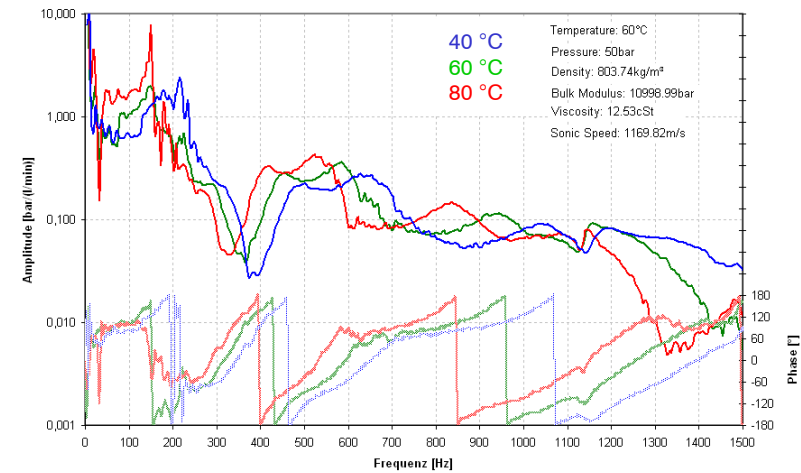
Temperature variation of an one-chamber hose line at 50 bar

Temperaturvariation einer Ein-Kammer-Schlauchleitung bei 50 bar

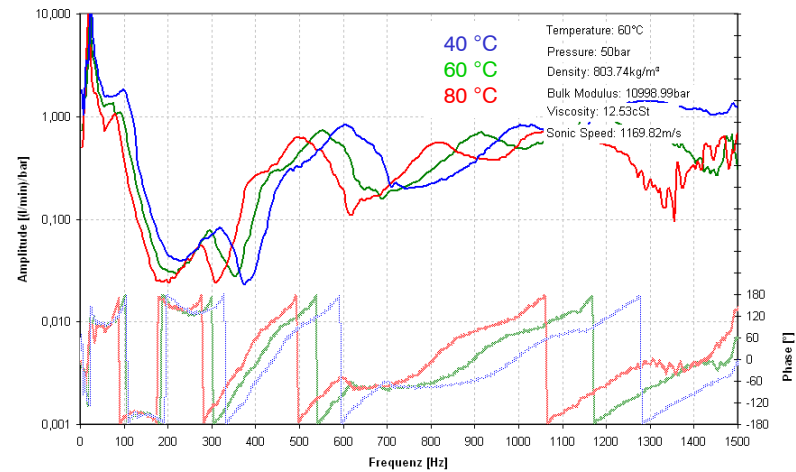
T11



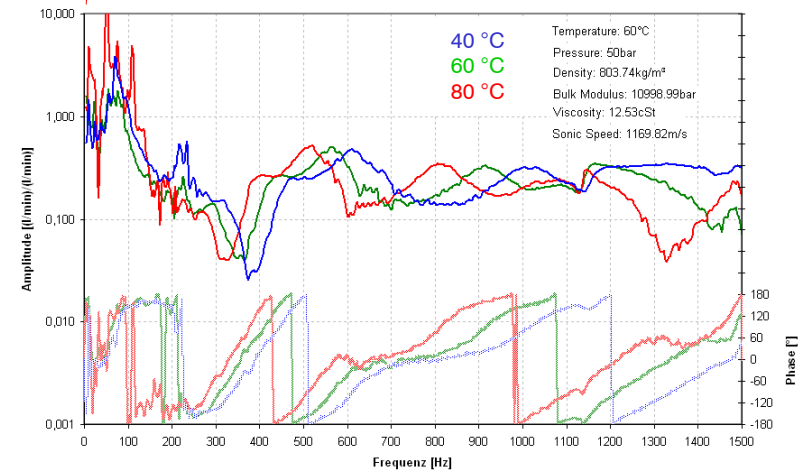
T12



T21



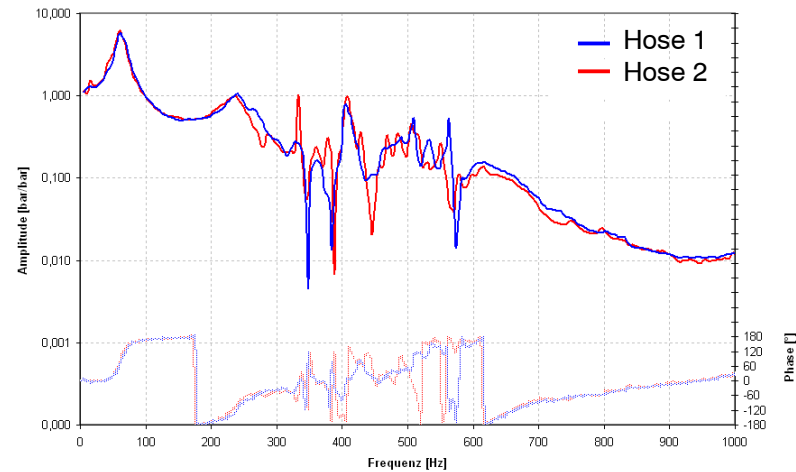
T22



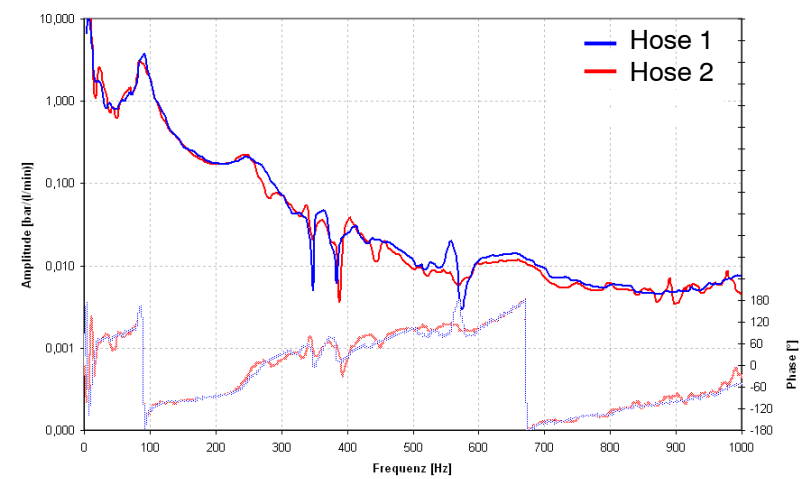
Fingerprint of an one-chamber line at 50 bar – 60 °C

Vergleich zweier Ein-Kammer-Leitungen bei 50 bar – 60 °C

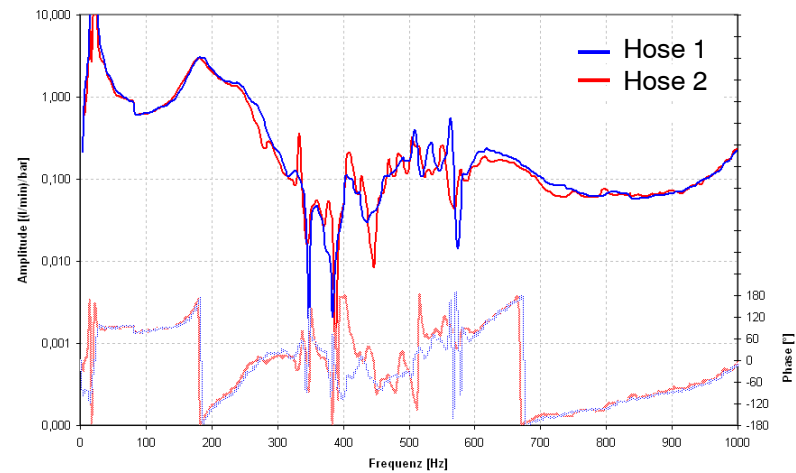
T11



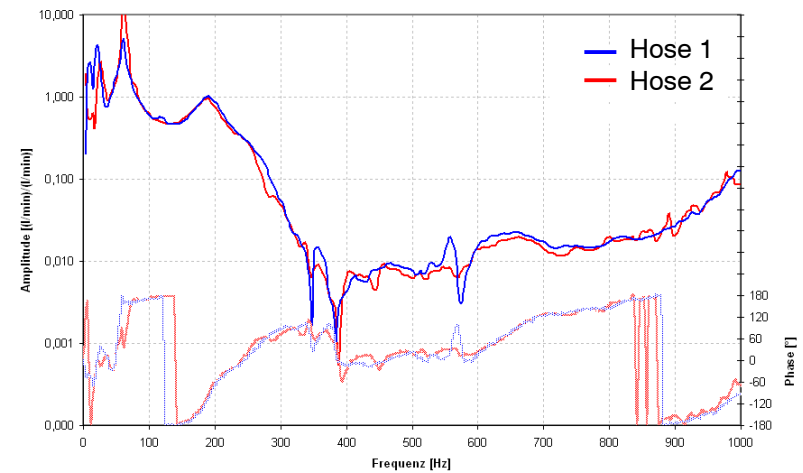
T12



T21

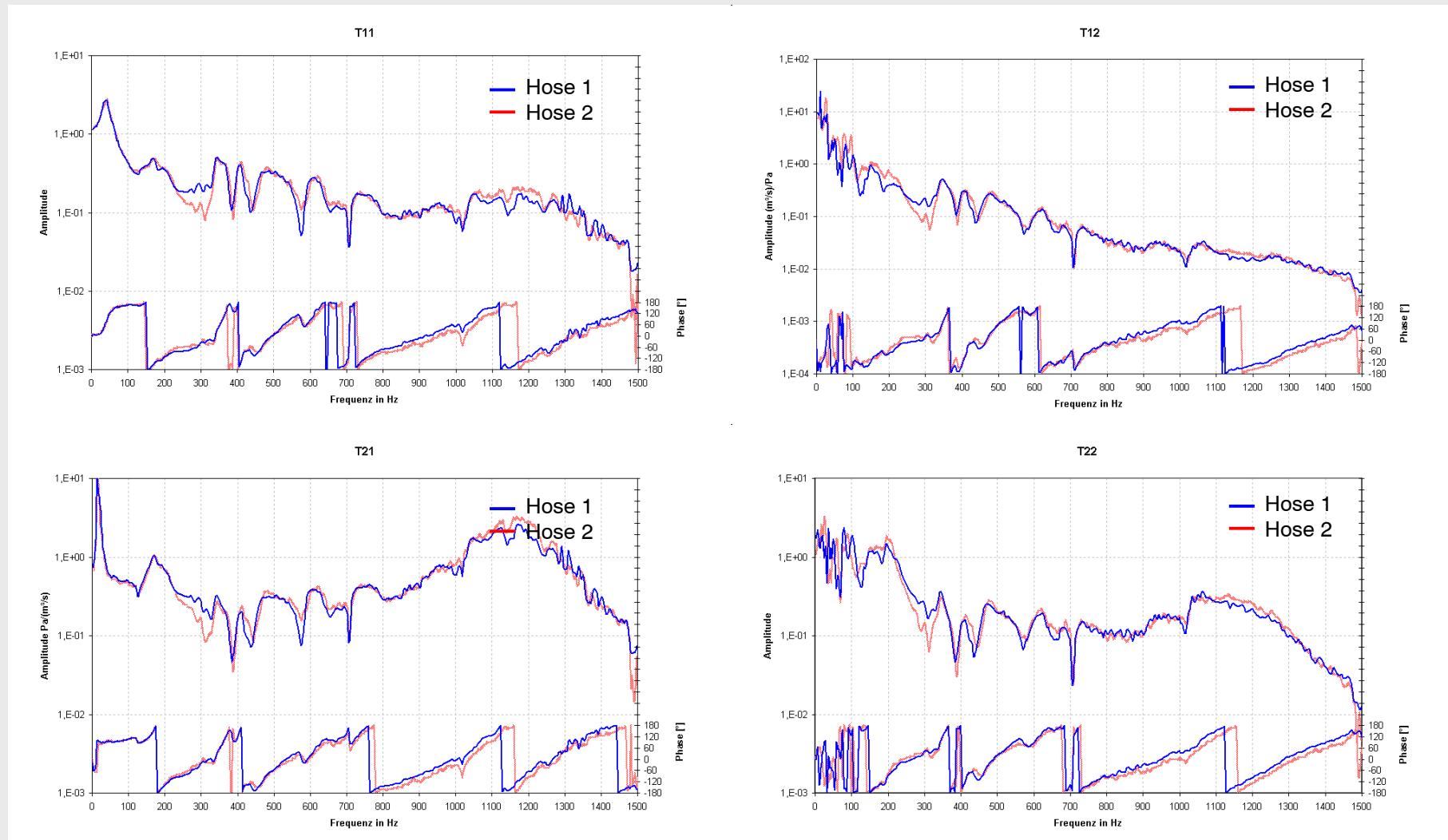


T22



Fingerprint of a two-chamber line at 10 bar - 40 °C

Vergleich zweier Zwei-Kammer-Leitungen bei 10 bar und 40 °C



1

Introduction

2

Current situation of hydraulic pipe and hose simulation

3

Development of a library for flexible hose elements

4

A development methodology for automotive lines

5

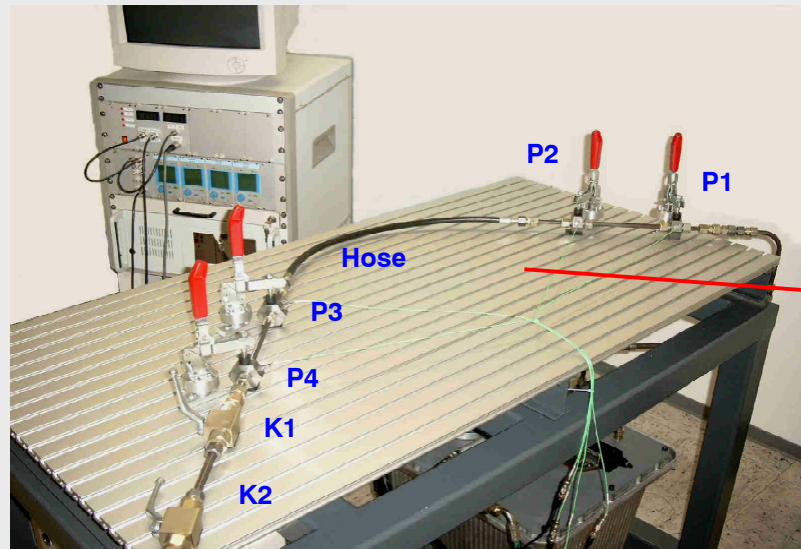
Presentation of example lines

6

Summary

Identification of hose material characteristic

Identifikation der Schlauchleitungscharakteristik



1. Test rig measurements:

Variation of hose length from 100 mm to 500 mm.

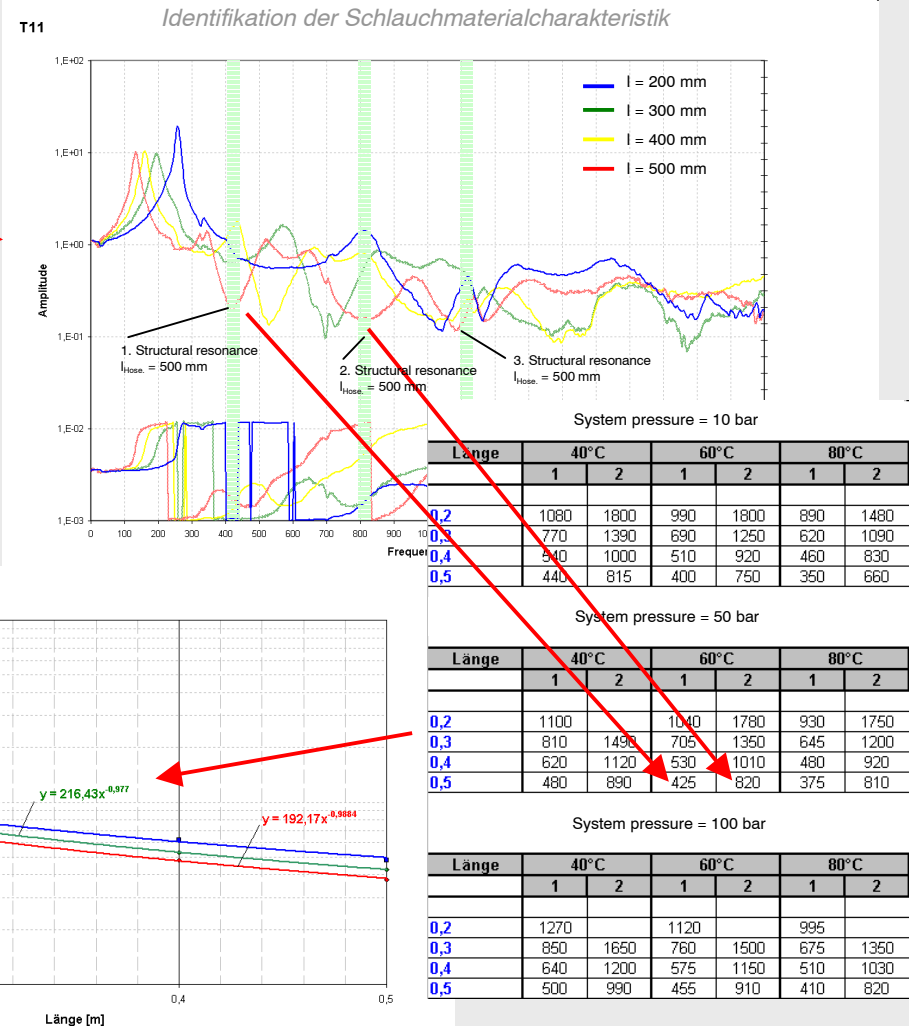
Each hose at 40, 60, 80 °C and at 10, 50, 100 bar

Prüfstandsmessungen: Variation der Schlauchlänge von 100 mm bis 500 mm. Jeder Schlauch bei 40, 60, 80 °C und bei 10, 50, 100 bar

3. Calculation of material characteristics

Berechnung der Materialcharakteristik

2. Identification of Hose Material Characteristic

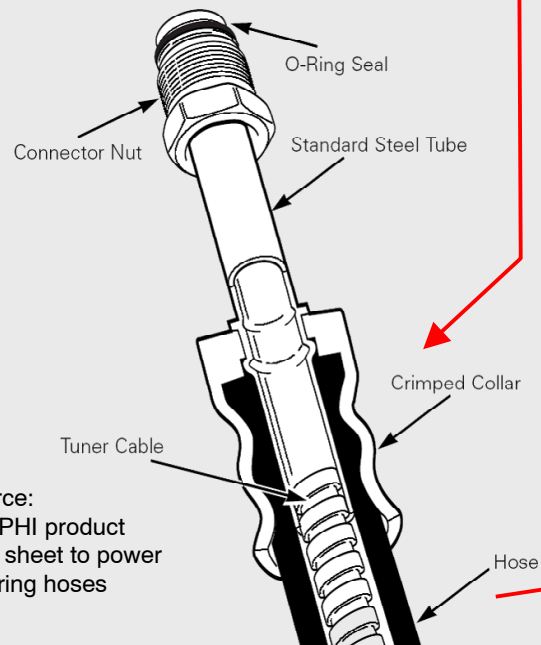
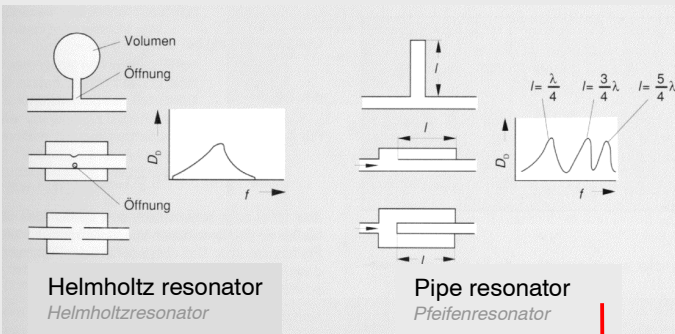


Example of a steering system model with complex feed line

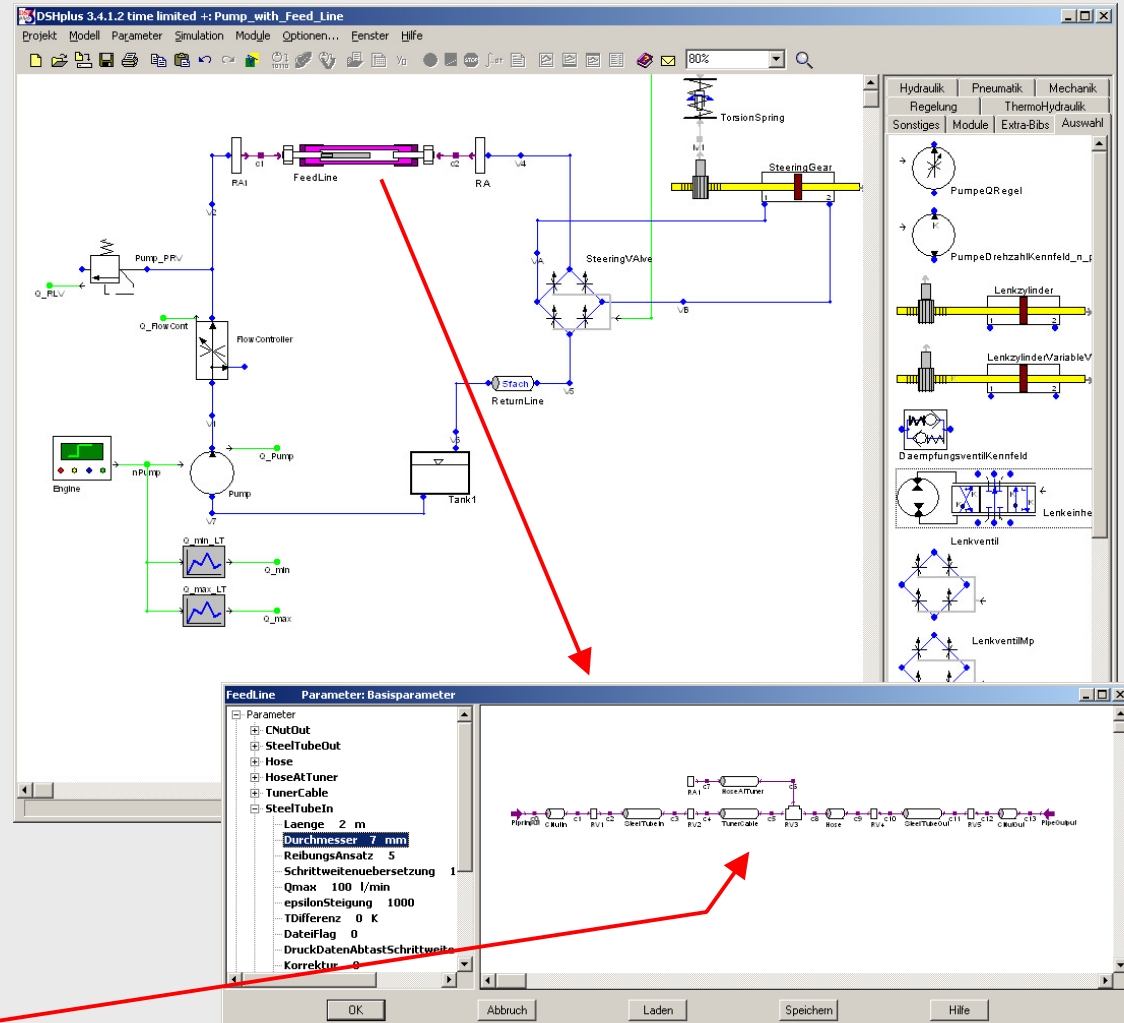
Beispiel eines Lenksystemmodells mit komplexer Versorgungsleitung

Basic resonator types

Basistypen für Resonatoren

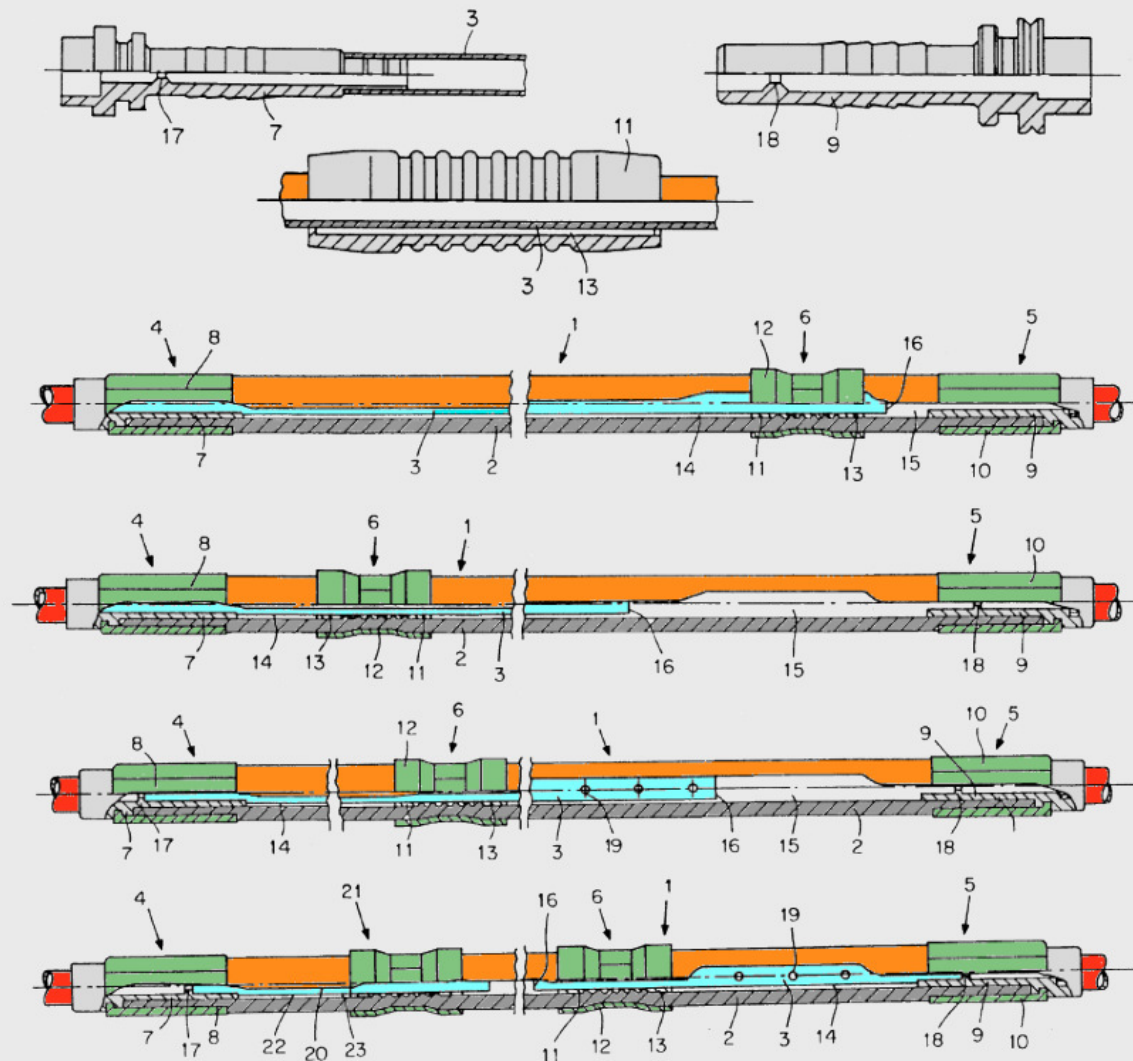


Source:
DELPHI product
data sheet to power
steering hoses



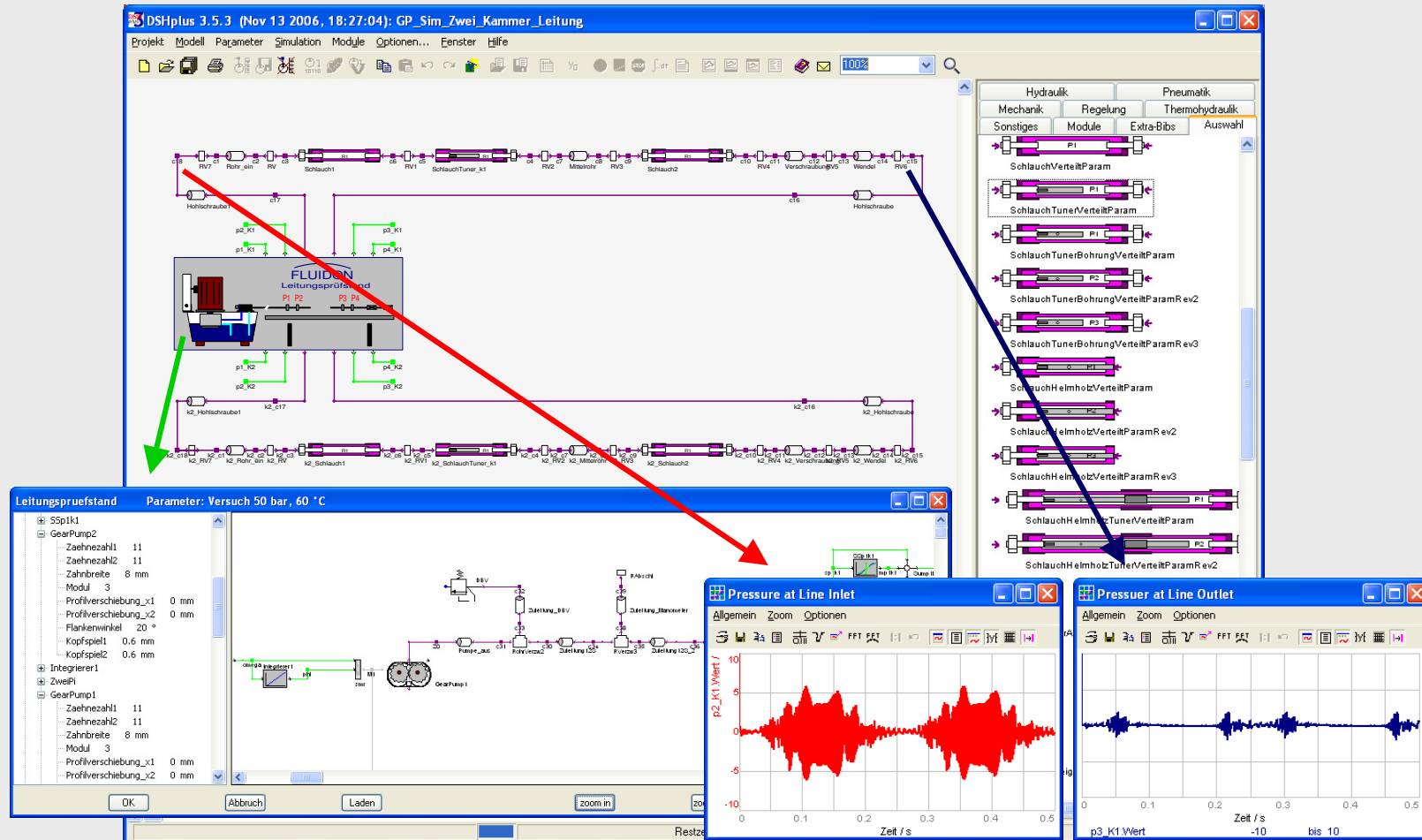
Examples for fittings and flexible hose elements

Beispiele für Installationen und flexible Schlauchelemente



Flexible hose library and simulation model of a two-chamber line

Dehnschlauchbibliothek und Simulationsmodell einer Zwei-Kammerdehnschlauchleitung

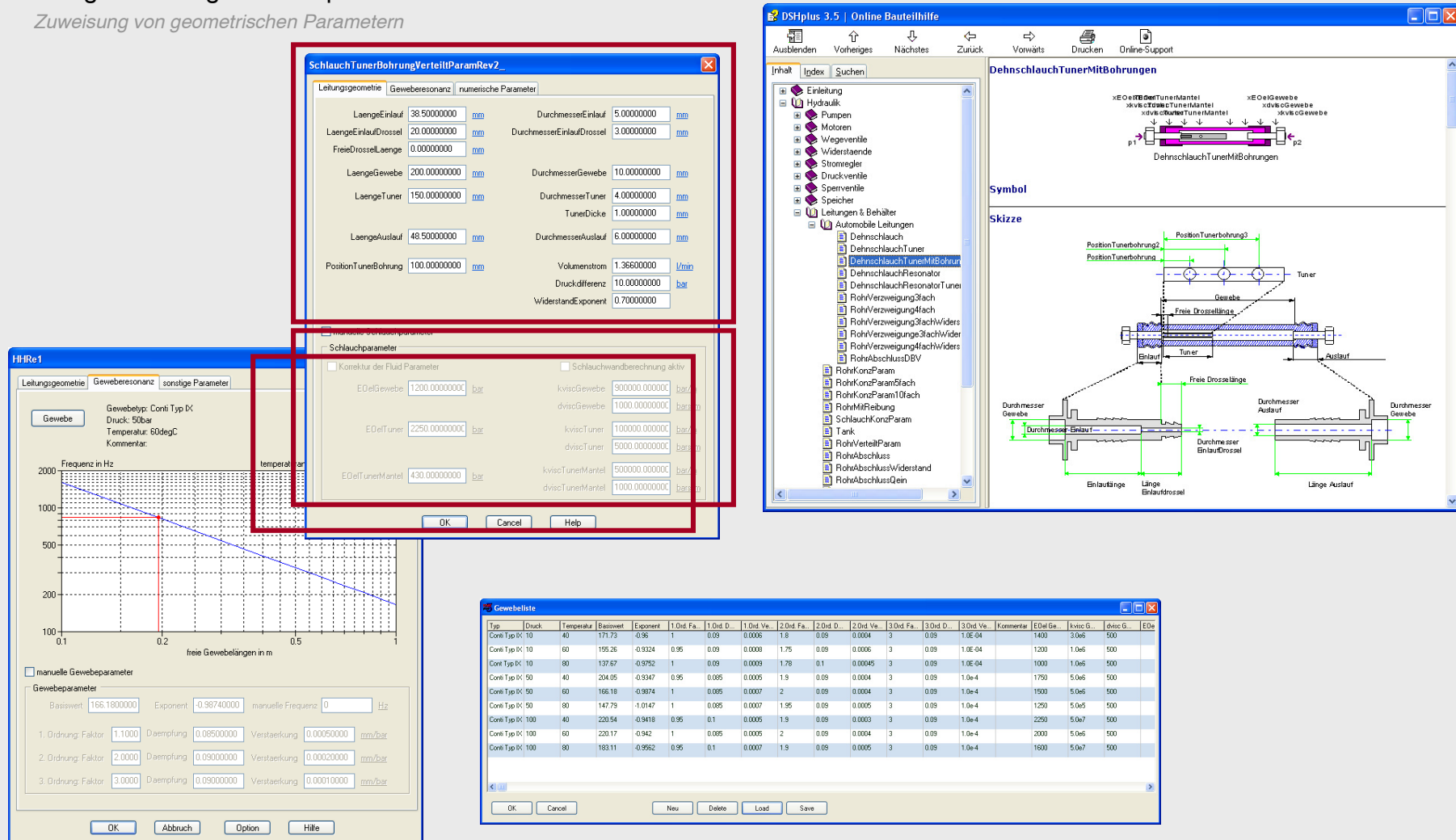


Usage of hose material characteristic

Anwendung der Schlauchleitungseigenschaft

1. Assignment of geometric parameters

Zuweisung von geometrischen Parametern



SchlauchTunerBohrungVerteilParamRev2

Leitungsgeometrie | Gegebenheiten | numerische Parameter

LaengeEinlauf: 38.50000000 mm | DurchmesserEinlauf: 5.00000000 mm
 LaengeEinlaufDrossel: 20.00000000 mm | DurchmesserEinlaufDrossel: 3.00000000 mm
 FreieDrosselLaenge: 0.00000000 mm
 LaengeGewebe: 200.00000000 mm | DurchmesserGewebe: 10.00000000 mm
 LaengeTuner: 150.00000000 mm | DurchmesserTuner: 4.00000000 mm
 TunerDicke: 1.00000000 mm
 LaengeAuslauf: 48.50000000 mm | DurchmesserAuslauf: 6.00000000 mm
 PositionTunerBohrung: 100.00000000 mm | Volumenstrom: 1.36600000 l/min
 Druckdifferenz: 10.00000000 bar
 WiderstandExponent: 0.70000000

HIRE1

Leitungsgeometrie | Gegebenheiten | sonstige Parameter

Gewebe: Gewebetyp: Coni Typ IK
 Druck: 50 bar
 Temperatur: 60 degC
 Kommentar:

Frequenz in Hz

freie Gewebelänge in m

Gewebe

Gewebeparameter

Basistwert: 165.1800000 | Exponent: 0.98740000 | manuelle Frequenz: 0 Hz

1. Ordnung: Faktor: 1.1000 | Dämpfung: 0.08500000 | Verstärkung: 0.00050000 mm/bar
 2. Ordnung: Faktor: 2.0000 | Dämpfung: 0.09000000 | Verstärkung: 0.00020000 mm/bar
 3. Ordnung: Faktor: 3.0000 | Dämpfung: 0.09000000 | Verstärkung: 0.00010000 mm/bar

GewebeListe

Typ	Druck	Temperatur	Basistwert	Exponent	1. Ord. Fa.	1. Ord. D.	1. Ord. Ve.	2. Ord. Fa.	2. Ord. D.	2. Ord. Ve.	3. Ord. Fa.	3. Ord. D.	3. Ord. Ve.	Kommentar	EOel Ge...	kvac Ge...	dvac Ge...	EOel
Coni Typ IK	10	40	171.73	-0.98	1	0.09	0.0006	1.8	0.09	0.0004	3	0.09	1.0e-04		1400	2.0e5	500	
Coni Typ IK	10	60	155.26	-0.9324	0.95	0.09	0.0009	1.75	0.09	0.0006	3	0.09	1.0e-04		1200	1.0e5	500	
Coni Typ IK	10	80	137.67	-0.9752	1	0.09	0.0009	1.78	0.1	0.00045	3	0.09	1.0e-04		1000	1.0e5	500	
Coni Typ IK	50	40	204.05	-0.9347	0.95	0.095	0.0005	1.9	0.09	0.0004	3	0.09	1.0e-4		1750	5.0e5	500	
Coni Typ IK	50	60	166.18	-0.9874	1	0.095	0.0007	2	0.09	0.0004	3	0.09	1.0e-4		1500	5.0e5	500	
Coni Typ IK	50	80	147.79	-1.0147	1	0.095	0.0007	1.95	0.09	0.0005	3	0.09	1.0e-4		1250	5.0e5	500	
Coni Typ IK	100	40	220.54	-0.9418	0.95	0.1	0.0005	1.9	0.09	0.0003	3	0.09	1.0e-4		2250	5.0e7	500	
Coni Typ IK	100	60	220.17	-0.942	1	0.095	0.0005	2	0.09	0.0004	3	0.09	1.0e-4		2000	5.0e5	500	
Coni Typ IK	100	80	183.11	-0.9562	0.95	0.1	0.0007	1.9	0.09	0.0005	3	0.09	1.0e-4		1800	5.0e7	500	

1

Introduction

2

Current situation of hydraulic pipe and hose simulation

3

Development of a library for flexible hose elements

4

A development methodology for automotive lines

5

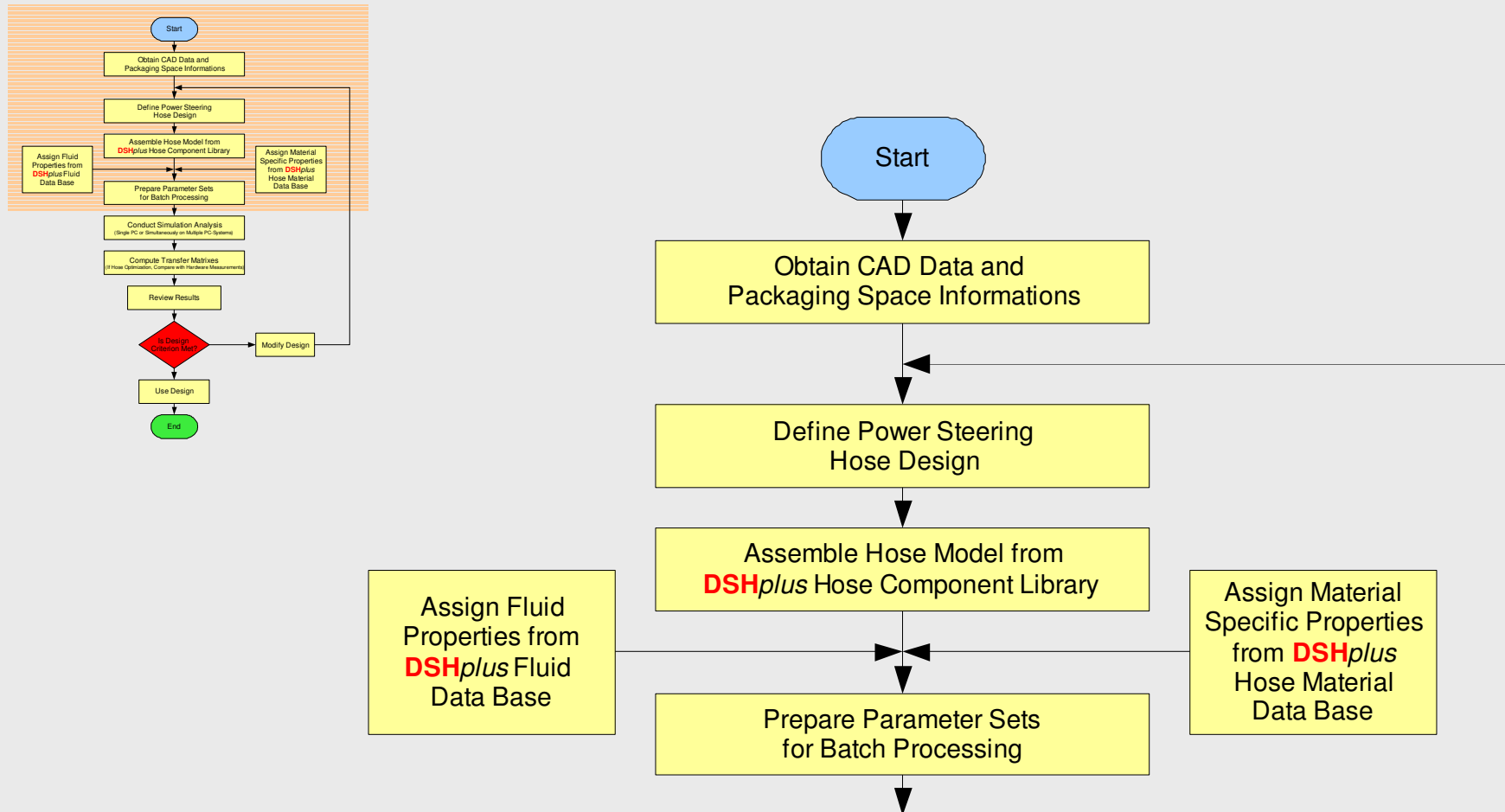
Presentation of example lines

6

Summary

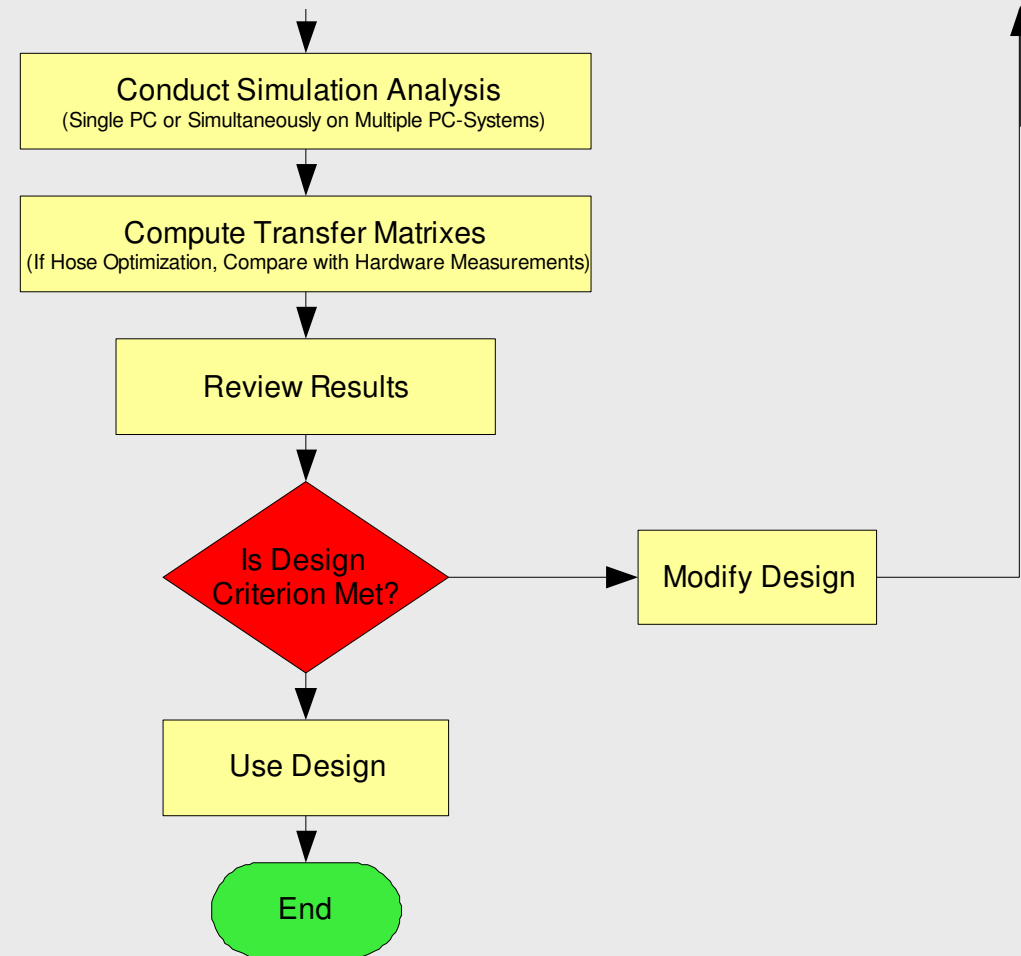
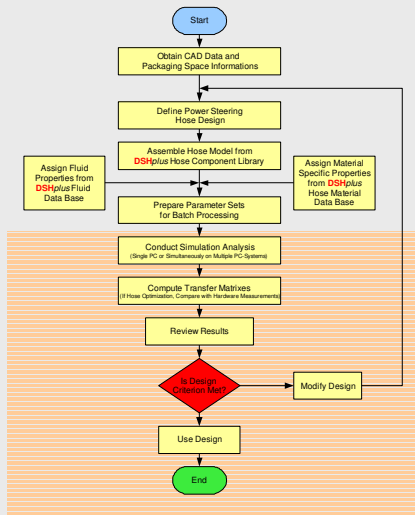
Development methodology for automotive hose assemblies

Entwicklungsmethodik für automobiler Dehnschlauchleitungen



Development methodology for automotive hose assemblies

Entwicklungsmethodik für automobiler Dehnschlauchleitungen



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5

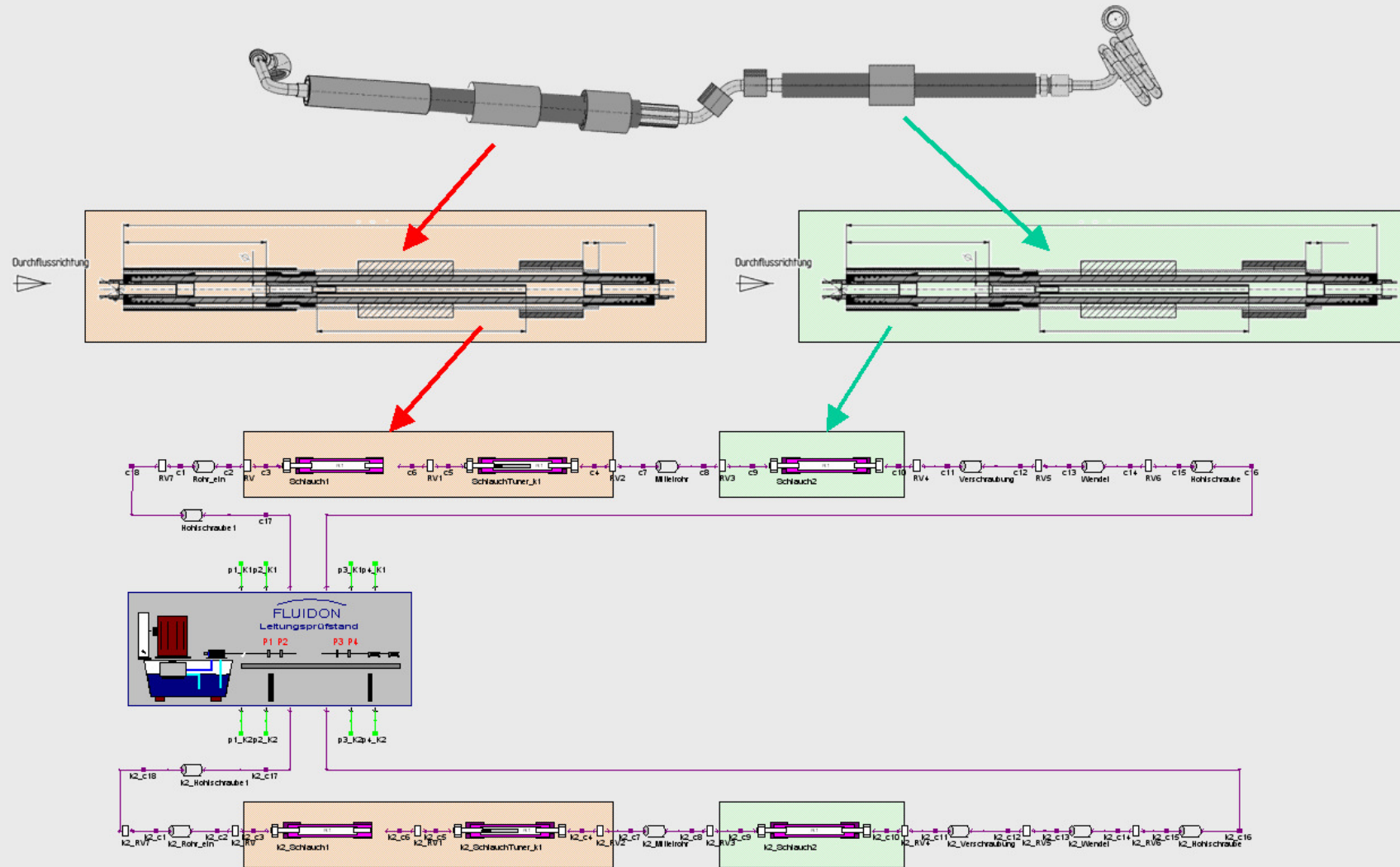
Presentation of example lines

6

Summary

Simulation model of a two-chamber line

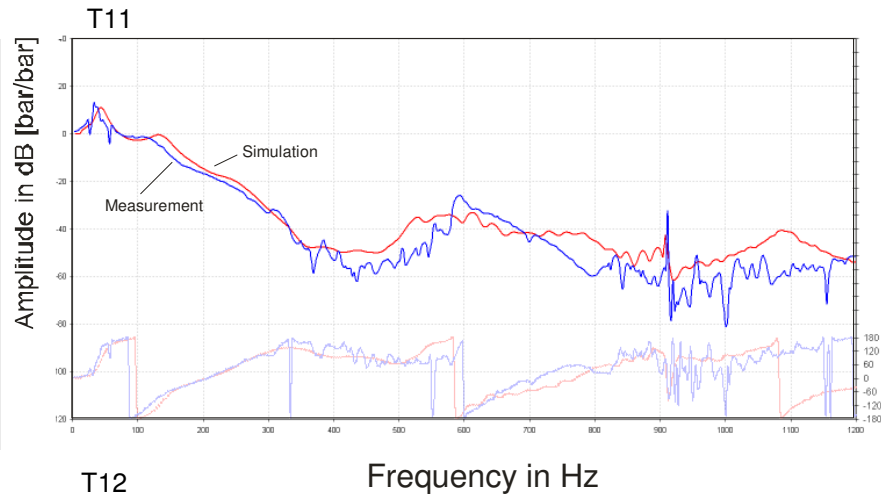
Simulationsmodell einer Zwei-Kammer-Leitung



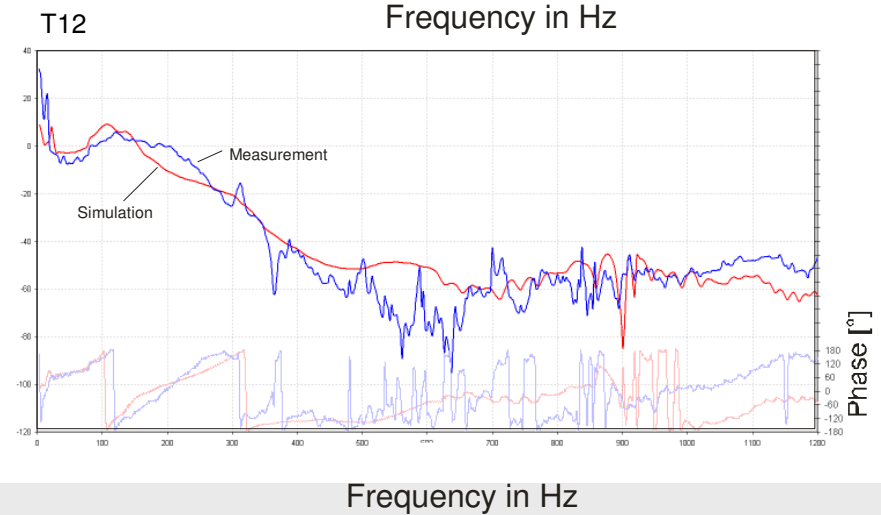
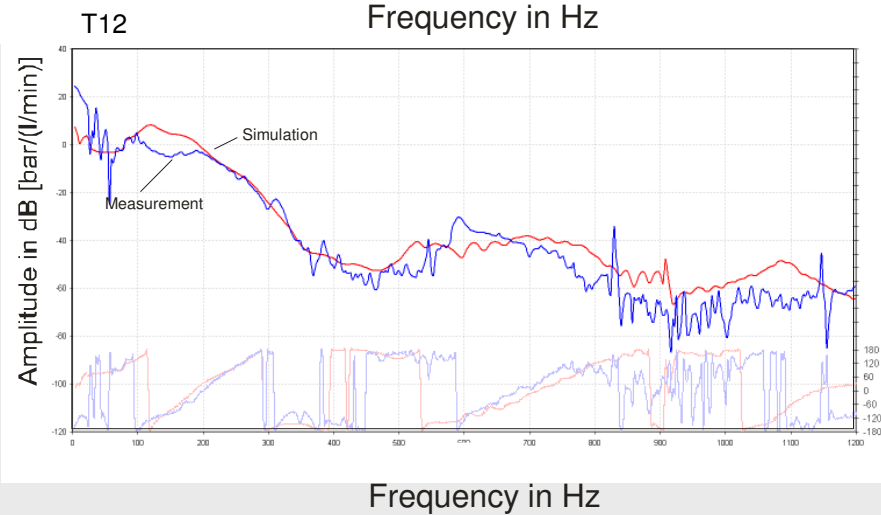
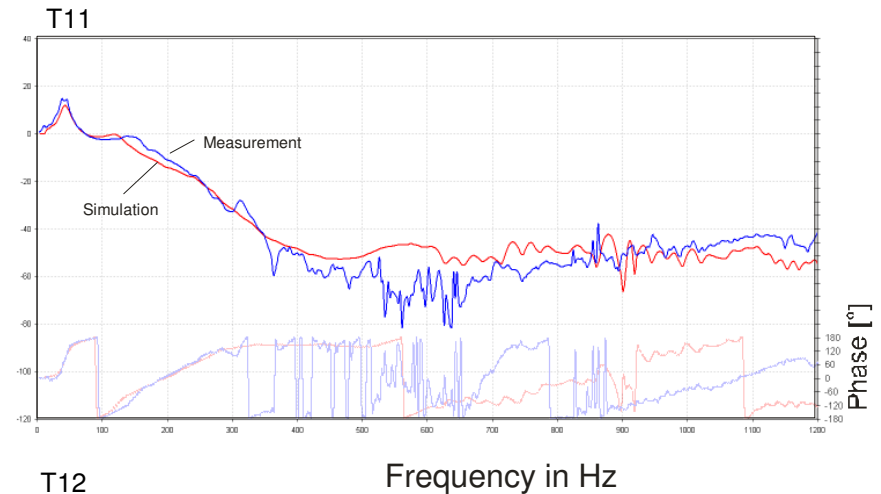
Example for an optimization of a two-chamber line

Beispiel für die Optimierung einer Zwei-Kammer-Leitung

Configuration A

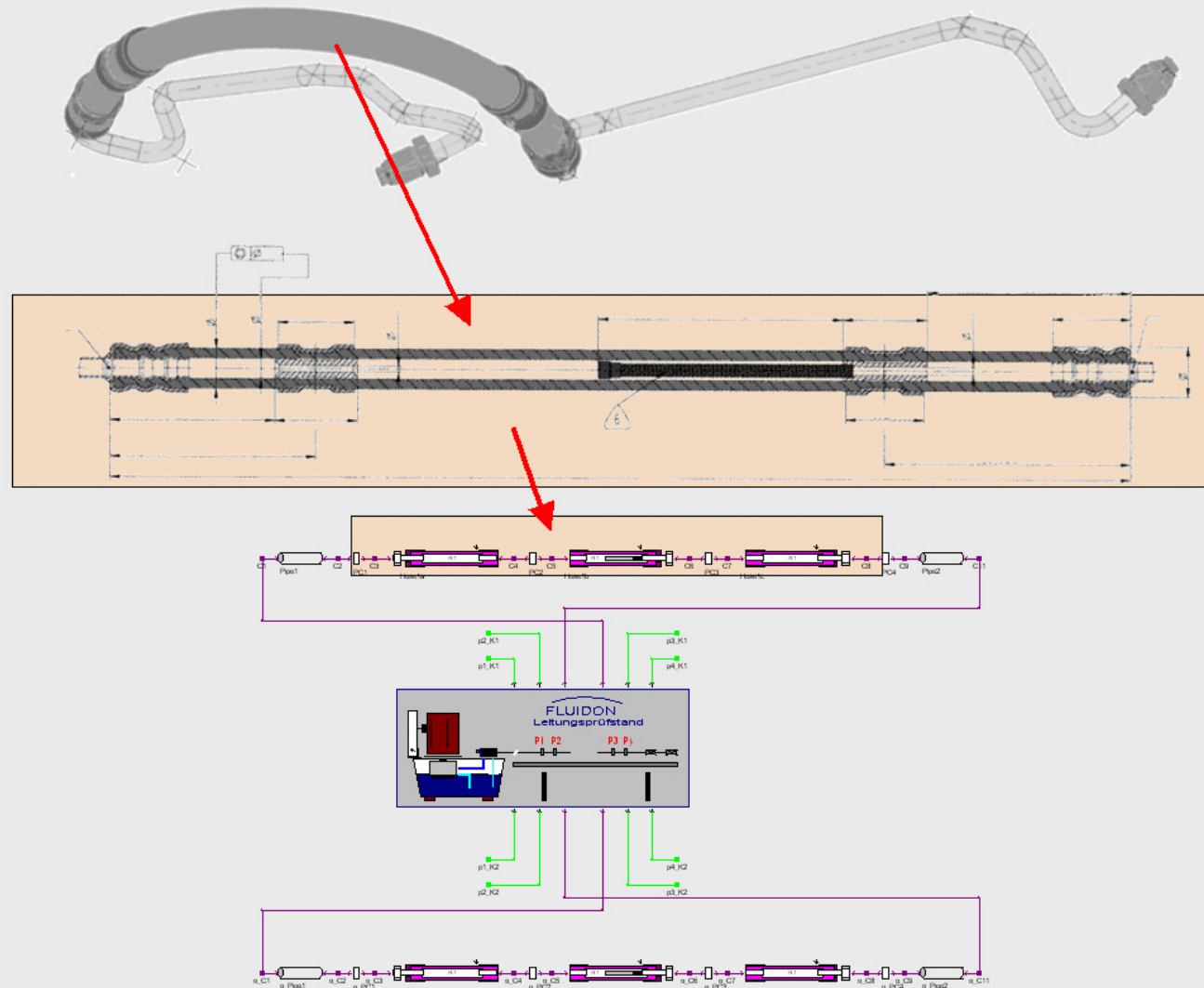


Configuration B



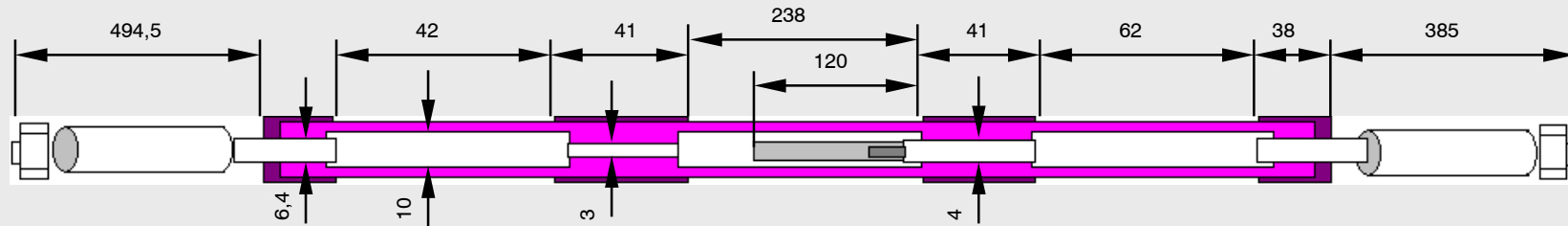
Simulation model of a one-chamber line with steel tuner

Simulationsmodell einer Ein-Kammer-Leitung Stahltuner



Example for a robustness analysis of the steel tuner line

Beispiel für eine Robustheitsanalyse der Stahltunerleitung

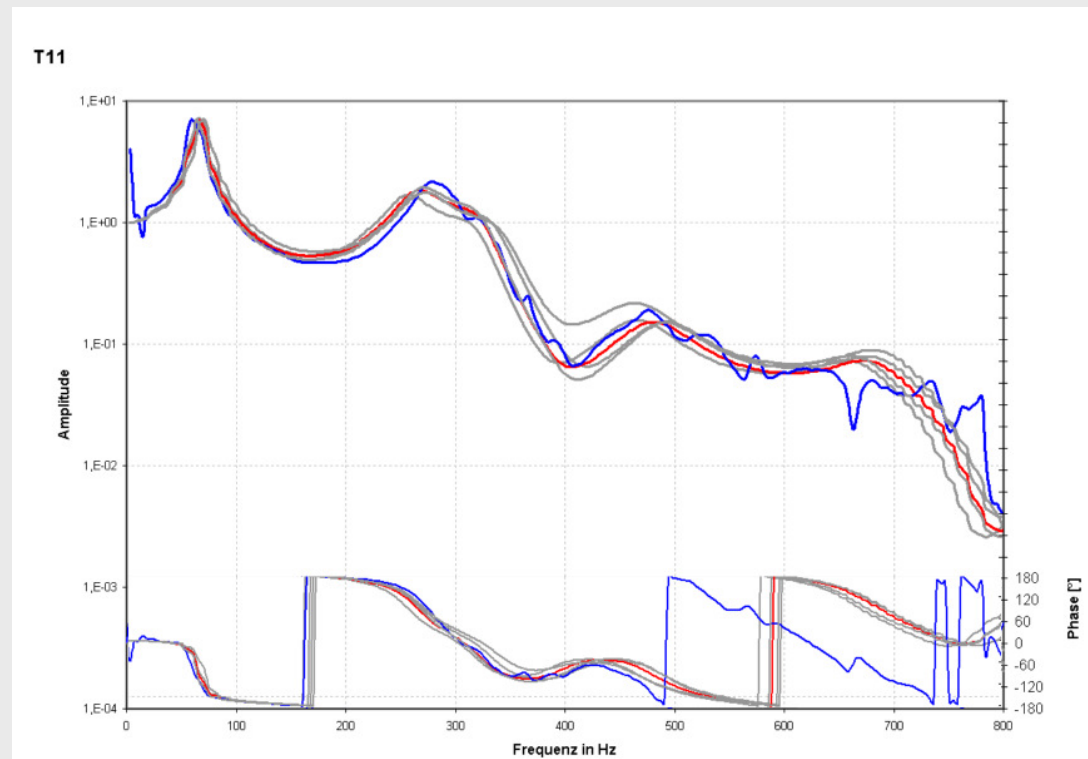


T11 represents the transfer function of pressure input (pump side) to pressure output (steering gear side)

Blue: Measured transfer function

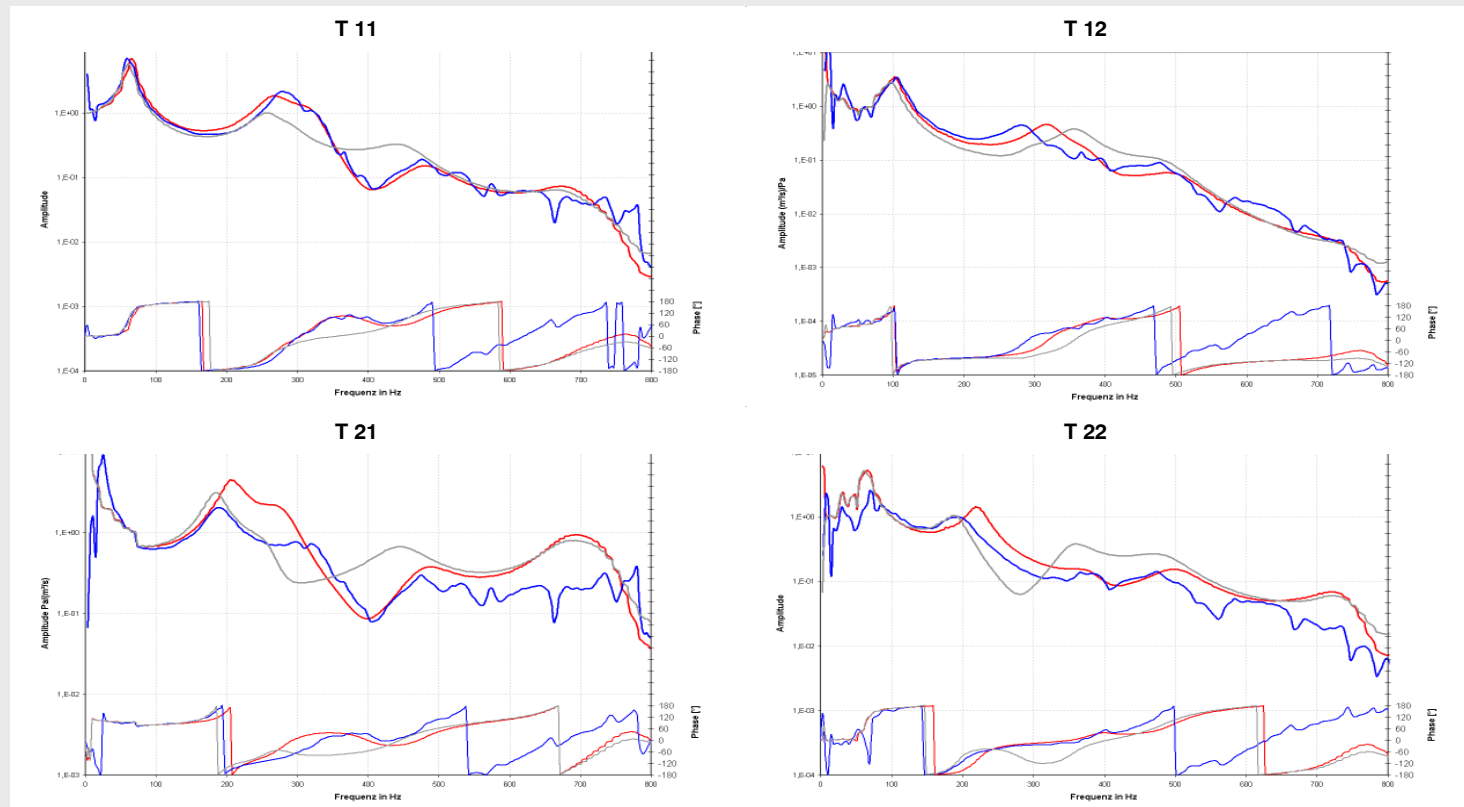
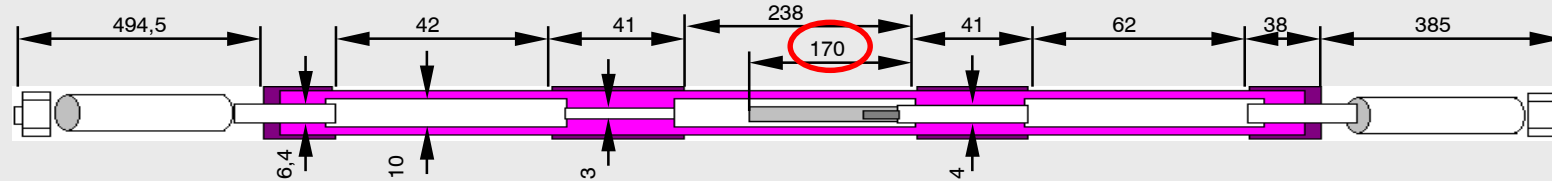
Red: Simulation with exact geometrical values

Grey: Simulation with tolerated geometrical values



Sensitivity analysis of the tuner length

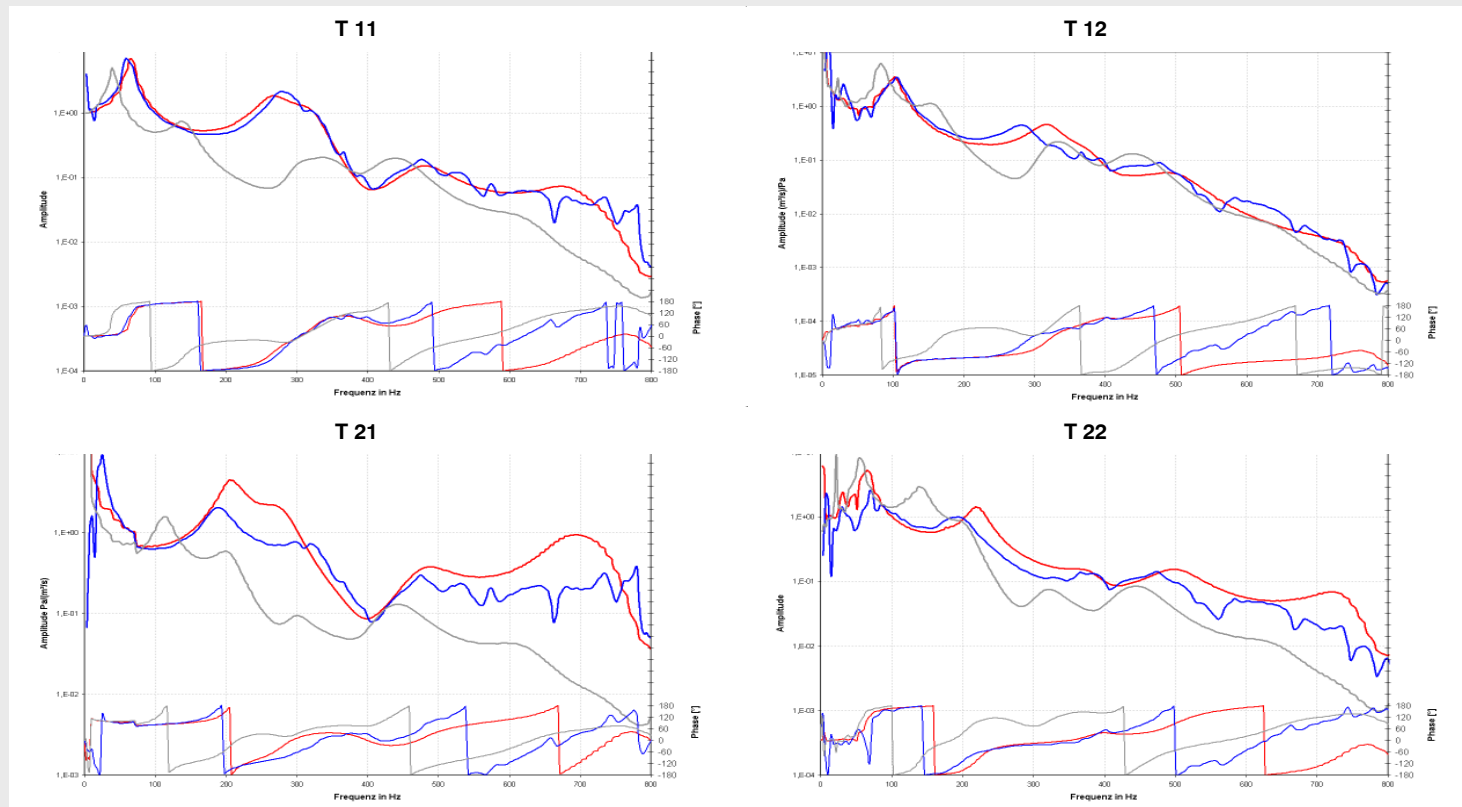
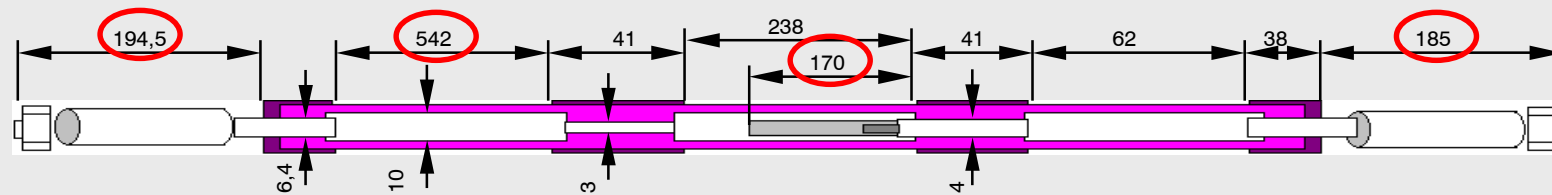
Sensitivitätsanalyse der Tunerlänge



$$l_{\text{Tuner}} = 170 \text{ mm (+50 mm)}$$

Sensitivity analysis of hose and pipe length

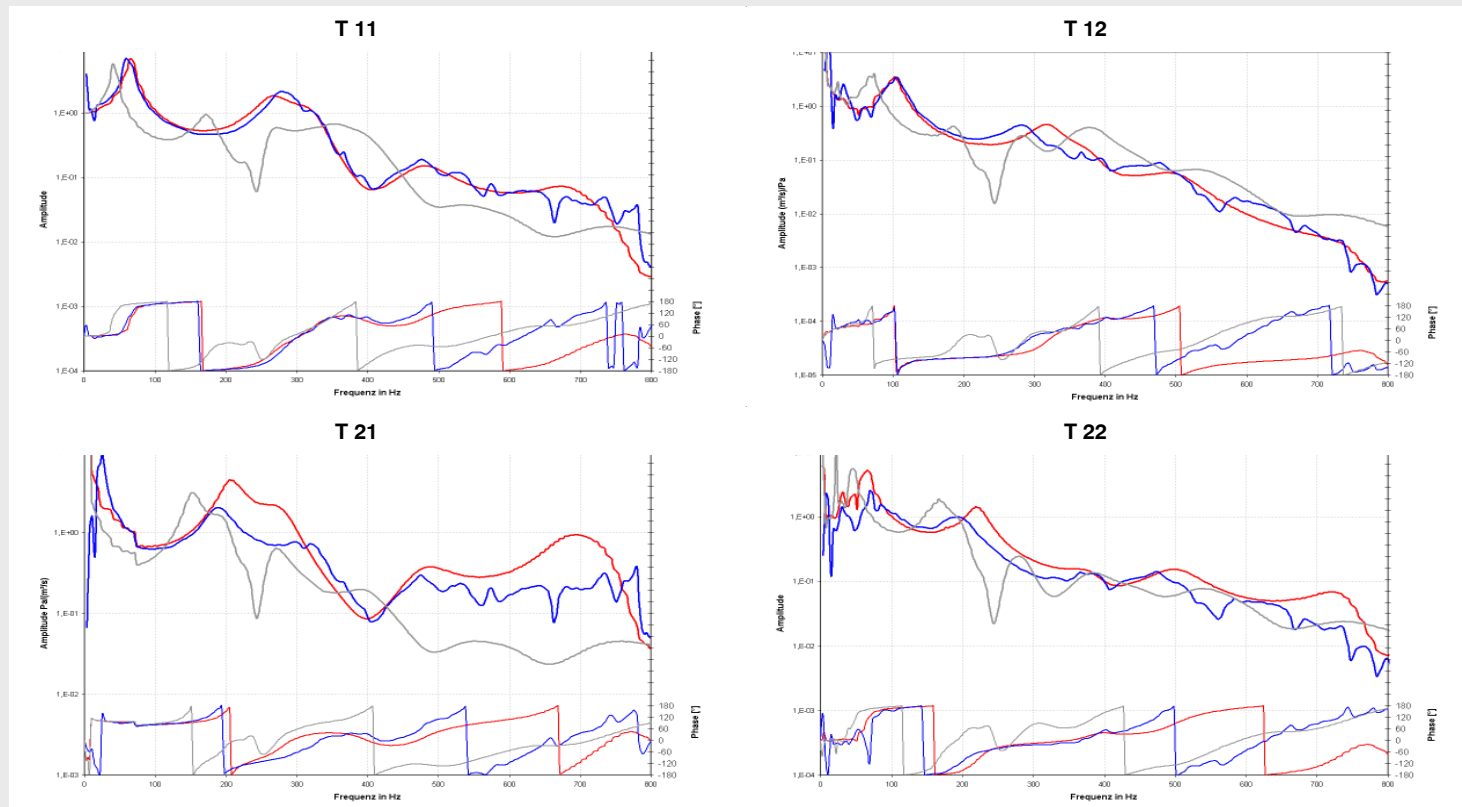
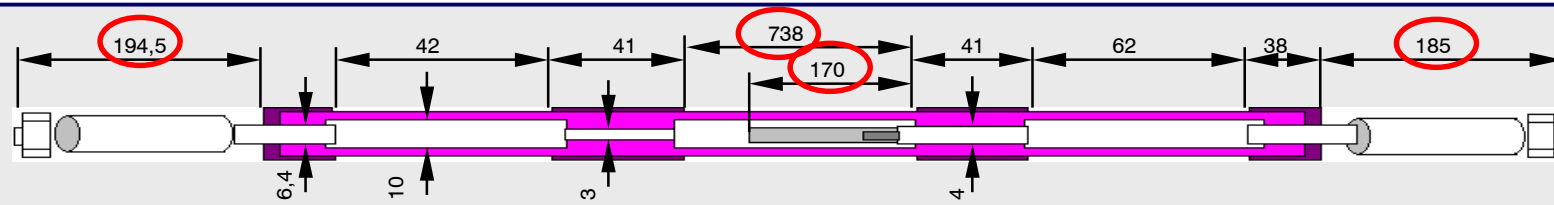
Sensitivitätsanalyse der Schlauch- und Rohrlänge



$$l_{\text{Tuner}} = 170 \text{ mm}, l_{\text{Hose}} \cdot 1a = + 500 \text{ mm}, \Sigma l_{\text{Pipe } 1, 2} = - 500 \text{ mm}$$

Sensitivity analysis of hose and pipe length

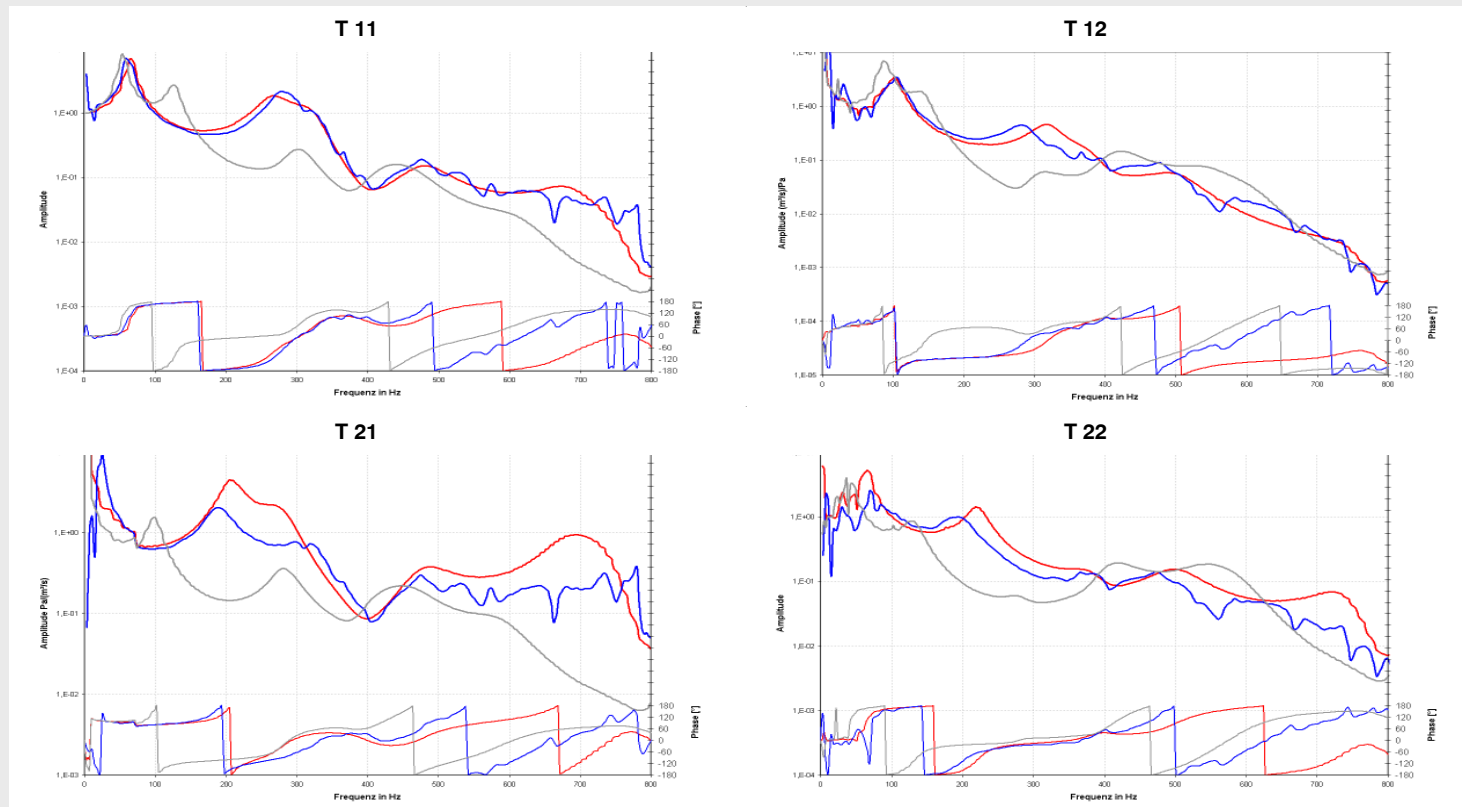
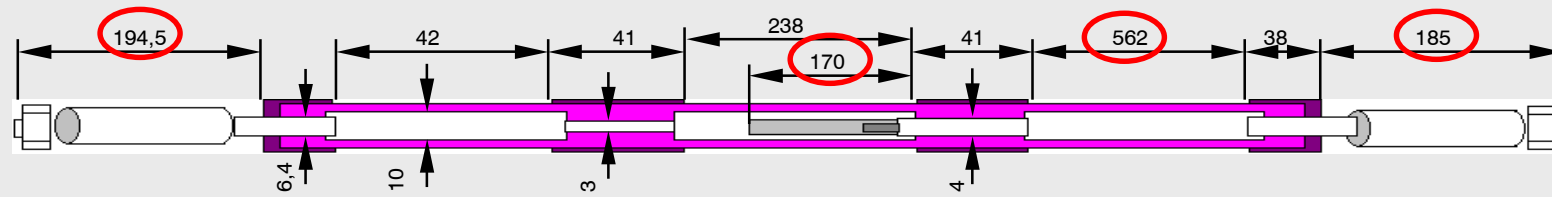
Sensitivitätsanalyse der Schlauch- und Rohrlänge



$$l_{\text{Tuner}} = 170 \text{ mm}, l_{\text{Hose}} \cdot 1b = + 500 \text{ mm}, \Sigma l_{\text{Pipe } 1, 2} = - 500 \text{ mm}$$

Sensitivity analysis of hose and pipe length

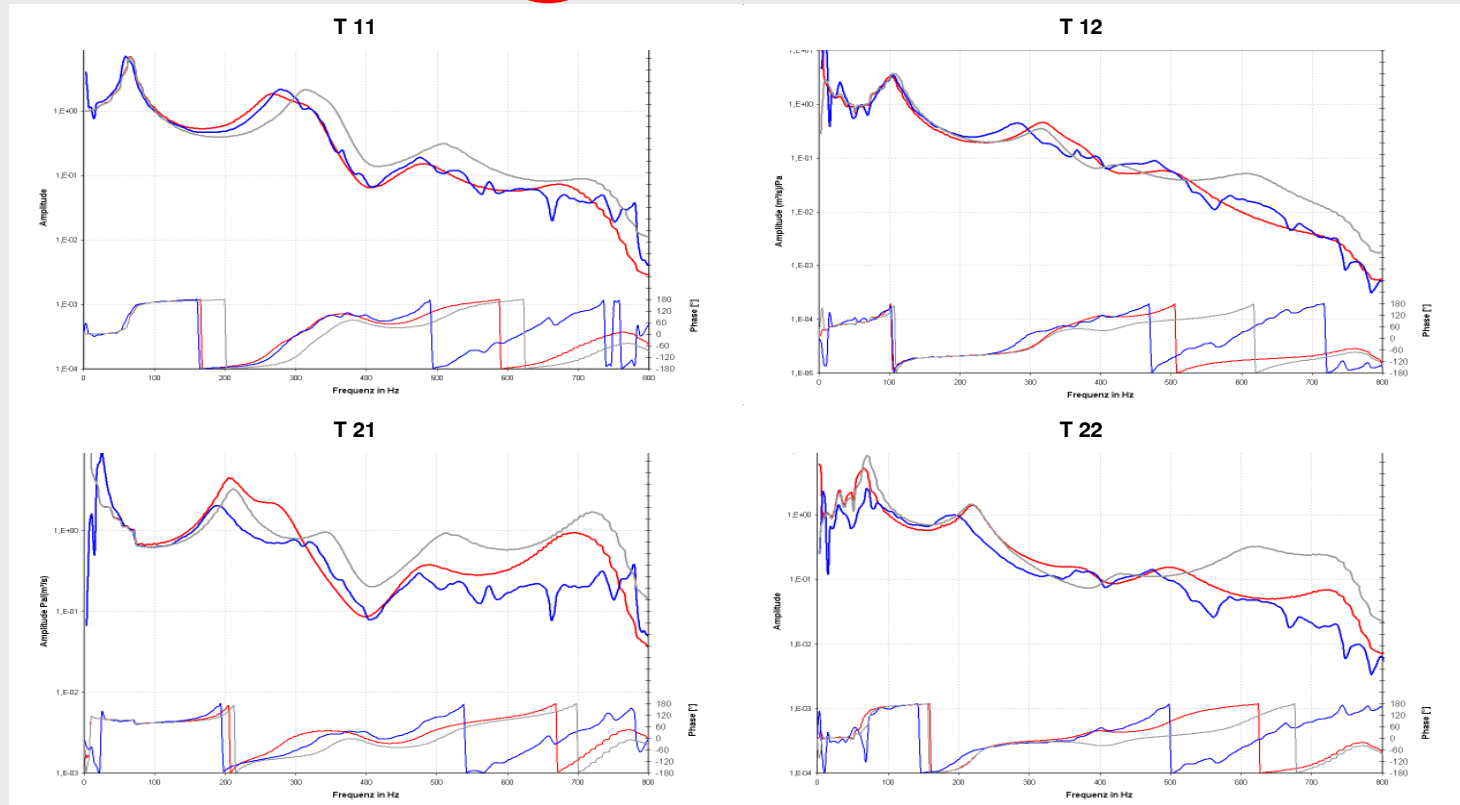
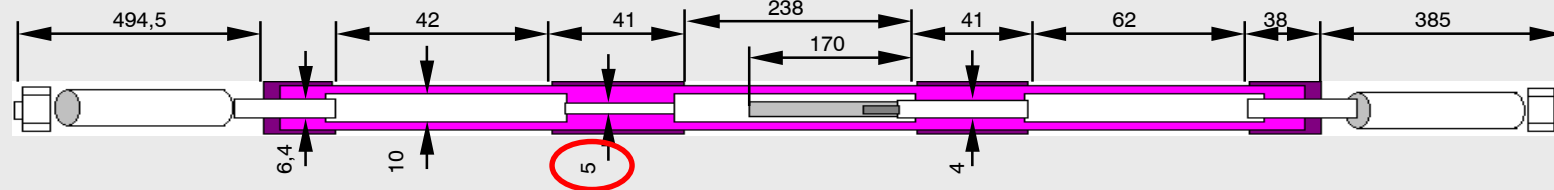
Sensitivitätsanalyse der Schlauch- und Rohrlänge



$$l_{\text{Tuner}} = 170 \text{ mm}, l_{\text{Hose}} \cdot 1c = + 500 \text{ mm}, \Sigma l_{\text{Pipe } 1, 2} = - 500 \text{ mm}$$

Sensitivity analysis of throttle diameter

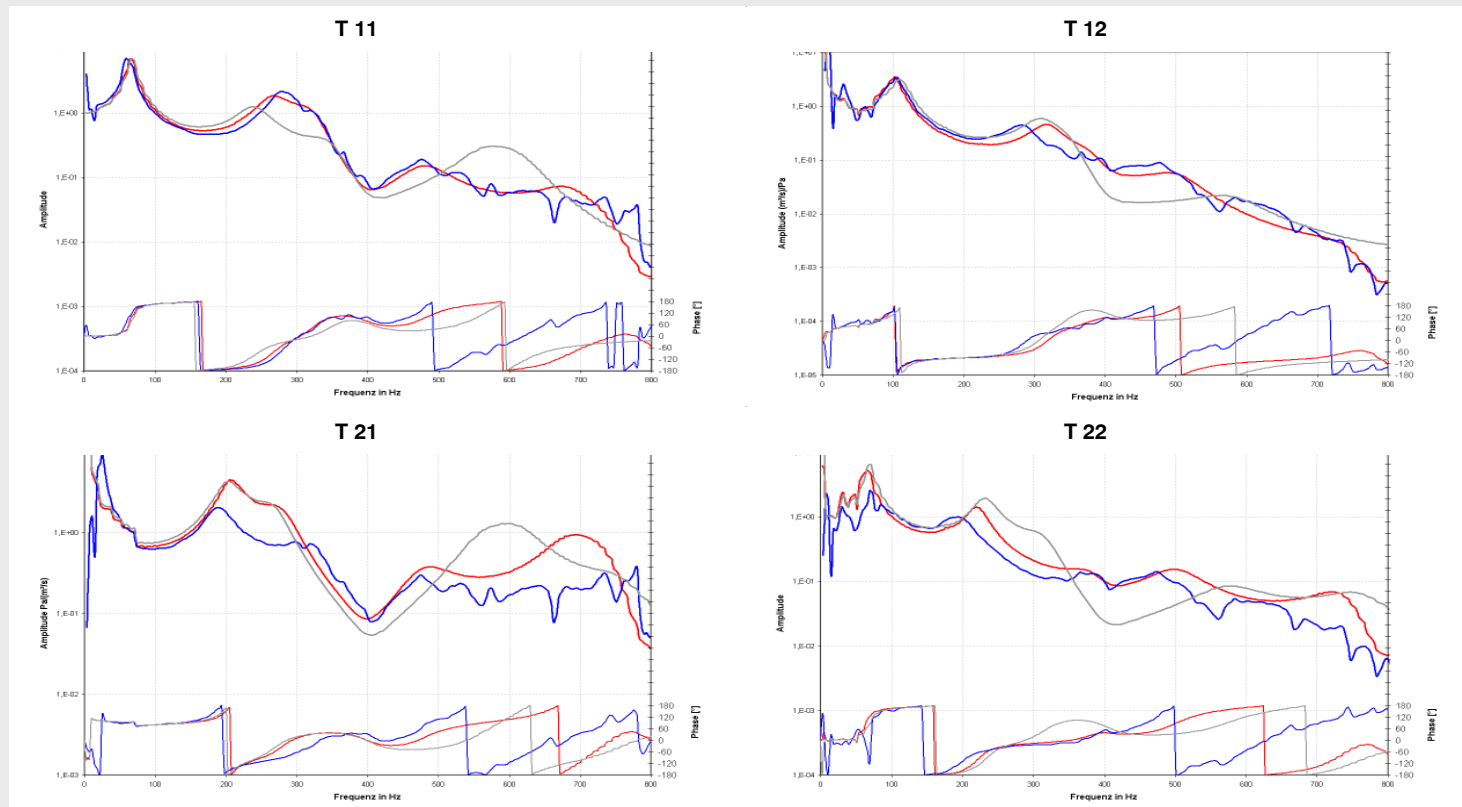
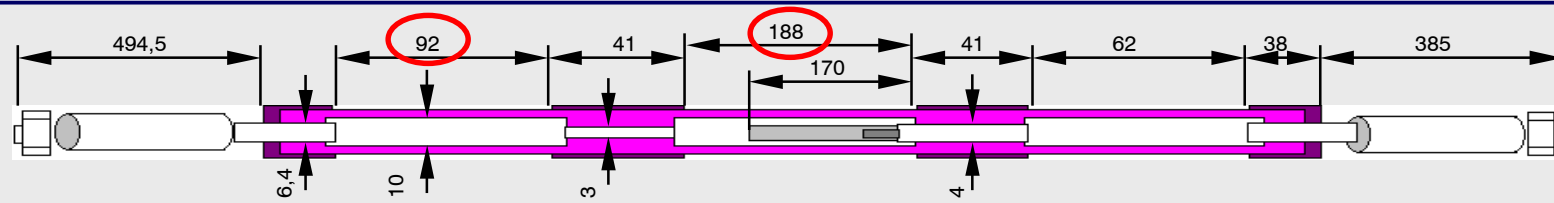
Sensitivitätsanalyse des Drosseldurchmessers



$$l_{\text{Tuner}} = 170 \text{ mm}, d_{\text{Throttle}} = 5 \text{ mm}$$

Sensitivity analysis of throttle position

Sensitivitätsanalyse des Drosselposition



$$l_{\text{Tuner}} = 170 \text{ mm}, l_{\text{Hose} \cdot 1a} = + 50 \text{ mm}, l_{\text{Hose} \cdot 1b} = - 50 \text{ mm},$$

1

Introduction

2

Current situation of hydraulic pipe and hose simulation

3

Development of a library for flexible hose elements

4

A development methodology for automotive lines

5

Presentation of example lines

6

Summary

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- By means of the new **DSH^{plus}** automotive hose library it is now possible to start the design of automotive lines using a virtual prototype. Based on a set of basic line elements the optimization of such lines can be automated using computer simulation.
- About variations of the geometry parameters a sensitivity and robustness analysis can very comfortably be carried out for the line design, e.g. by means of Doe techniques. The custom-designed application of automotive hose lines is not only accelerated by this, effort and costs for final tests with hardware prototypes are also reduced considerably.