

COMBUSTION AND EXHAUST EMISSION IN COMPRESSION IGNITION ENGINES WITH DUAL-FUEL SYSTEM

WLADYSLAW MITIANIEC

CRACOW UNIVERSITY OF TECHNOLOGY

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APPLICATIONS OF DUAL FUEL SYSTEMS IN CI ENGINES

- **Application of alternative fuels, particularly from biomass**
- **Air mixtures of ethanol or ethanol-diesel cannot be applied in CI engines due to physic-chemical properties (viscosity, surface tension, corrosion etc.)**
- **Diesel engines can work very well by using of dual fuelling system with chosen proportion of both fuels**
- **Electronically controlled multipoint port injection of ethanol and direct injection of diesel oil in CI engines**
- **Electronically controlled multipoint port injection of CNG as a main fuel and direct injection of diesel oil as a pilot fuel (initiation of self-ignition)**
- **Experimental works on dual fuel diesel engines in Poland since 1980 (Cracow University of Technology, Radom University of Technology, ATH Bielsko Biala)**

Diesel oil – ethanol fuelling system in direct injection CI engine

ENGINE SPECIFICATION

Engine type	- Andoria 1HC102 4-stroke CI
Cylinder number	- 1 horizontal
Bore	- 102 mm
Stroke	- 120 mm
Capacity	- 980 cm³
Compression ratio	- 17
Nominal power	- 11 kW/2200 rpm
Number of inlet valve	- 1
Number of exhaust valve	- 1
Injector	- 1
Position of injector	- 45° to cylinder axis

Analysis of engine work fuelled with diesel oil + ethanol:

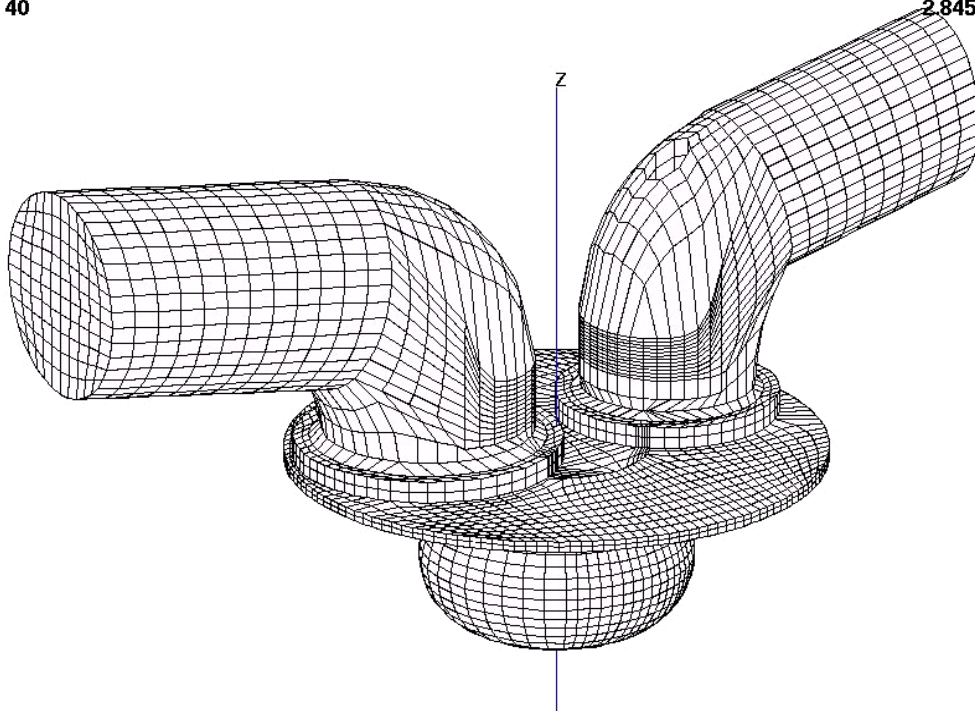
- 1. Simulation study by CFD KIVA3V program**
- 2. Experimental tests on dynamometer stand**

SIMULATION OF DUAL FUEL COMBUSTION in Andoria 1HC102 diesel engine (program KIVA3V)

ENGINE MESH

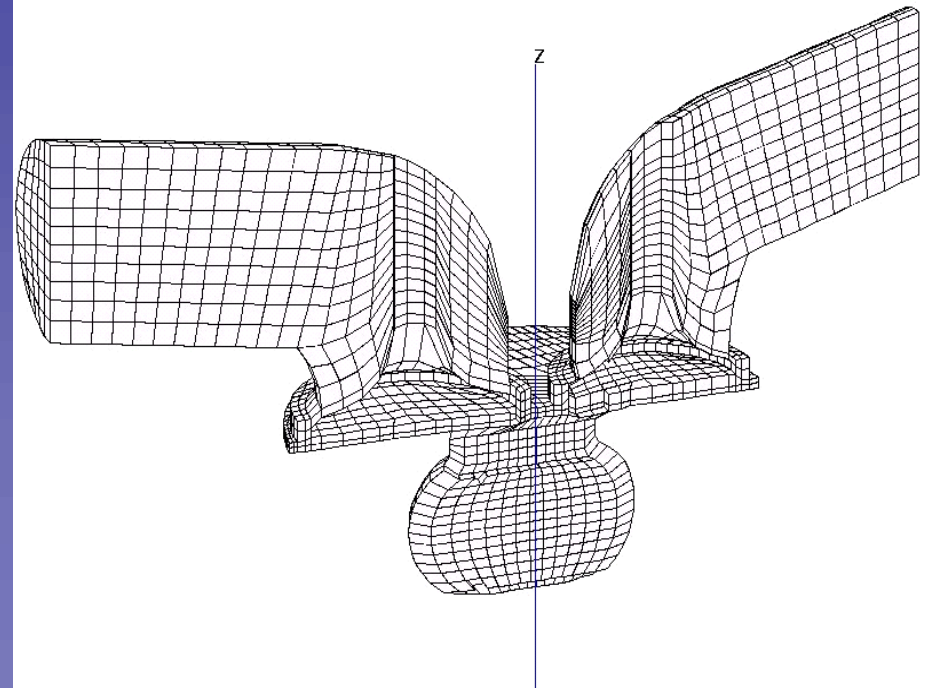
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Experimental stand of dual fuel CI engine (ethanol + DF)

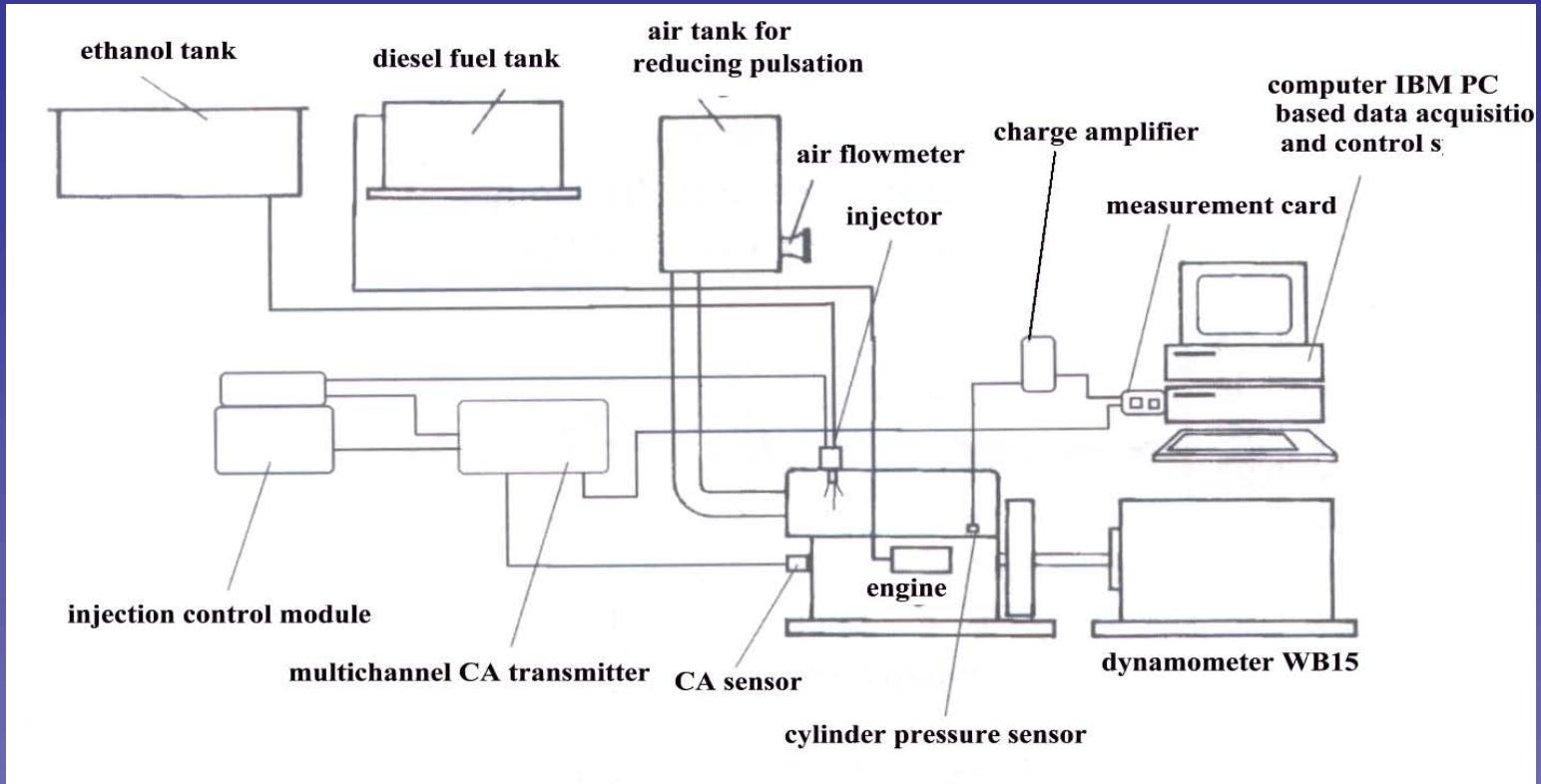
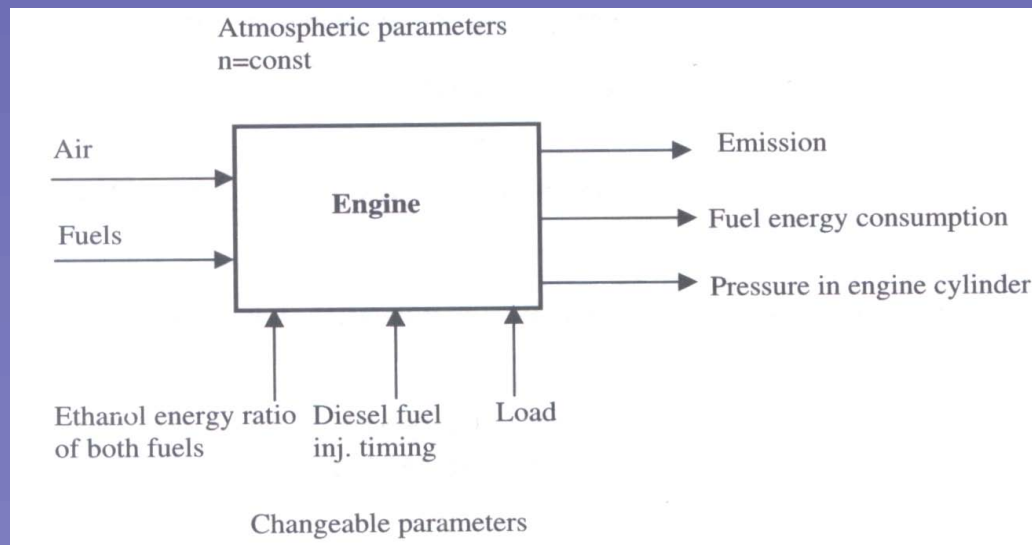
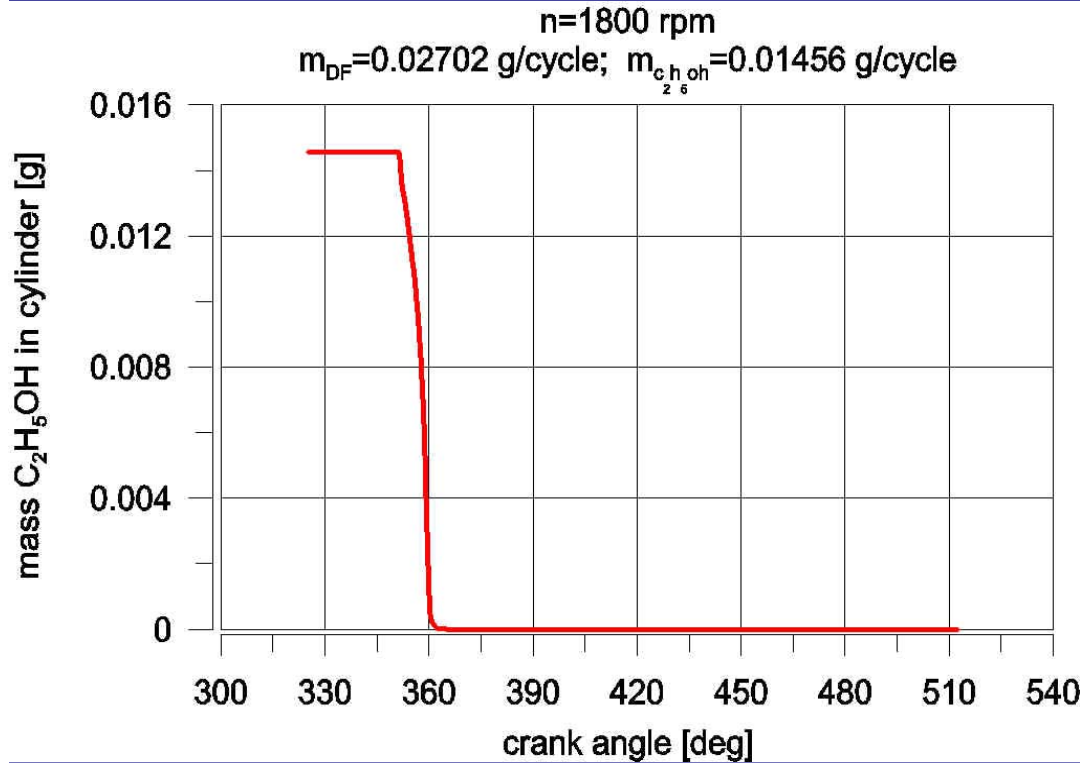


Diagram of dual fuel system

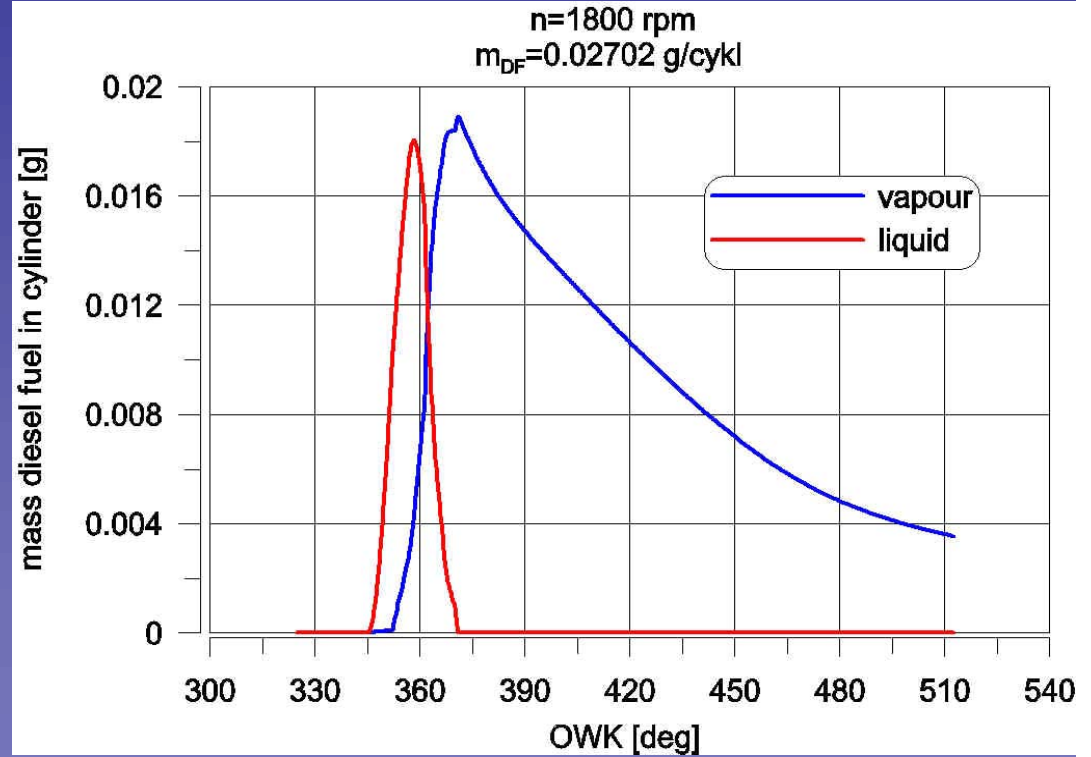


Simulation results

Combustion of ethanol at 1800 rpm



Evaporation and combustion of diesel fuel at 1800 rpm

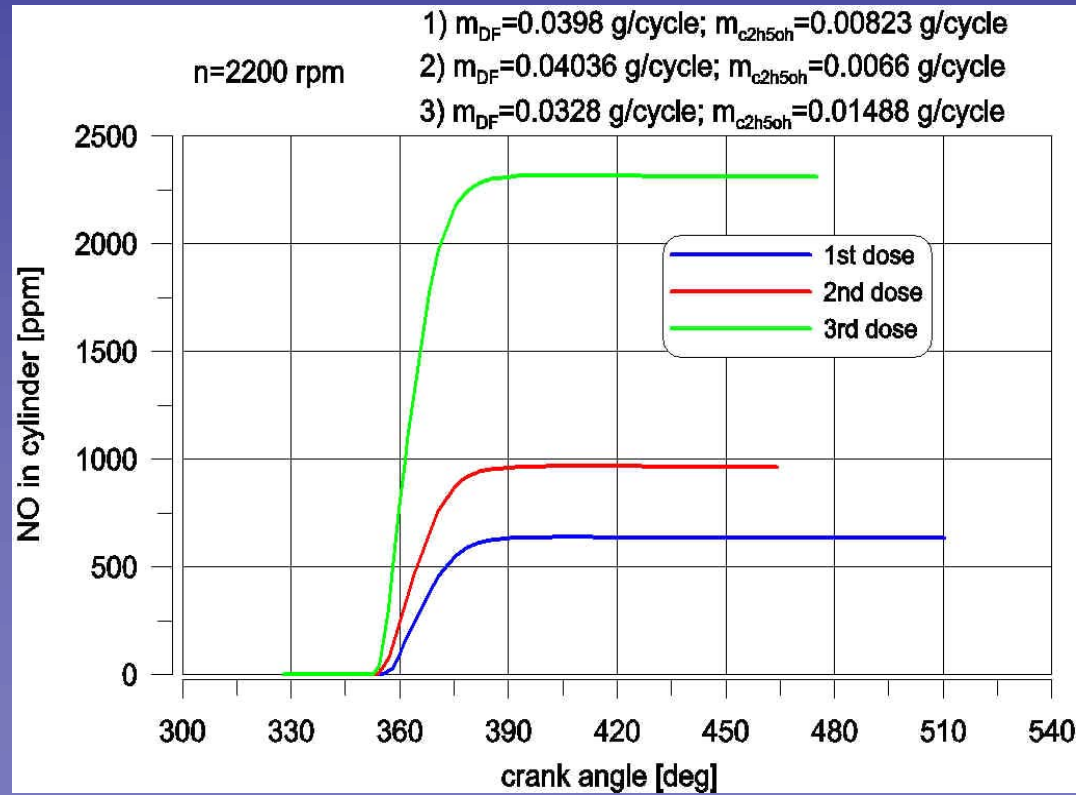
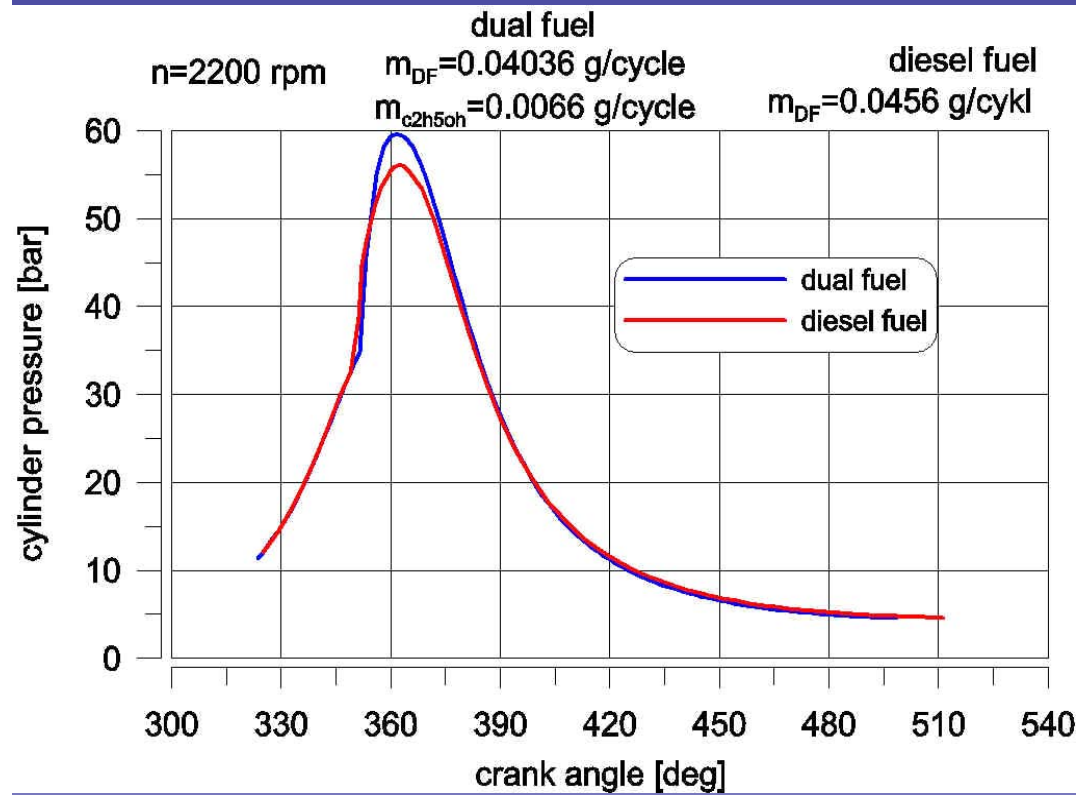


Simulation results

n=2200 rpm

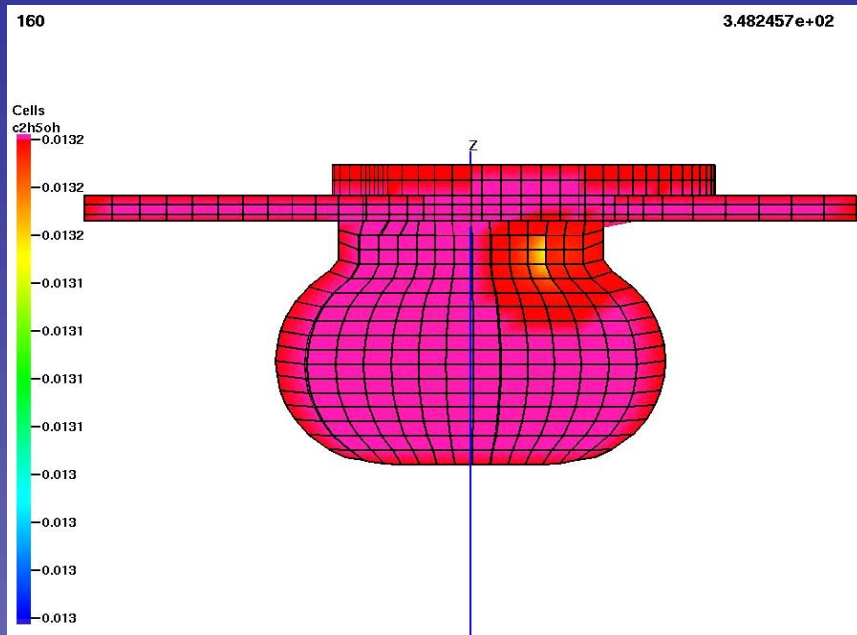
Comparison of cylinder pressure at 2000 rpm for diesel fuel and dual fuel (ethanol + DF)

NO cylinder mass concentration for different dual fuel mixtures

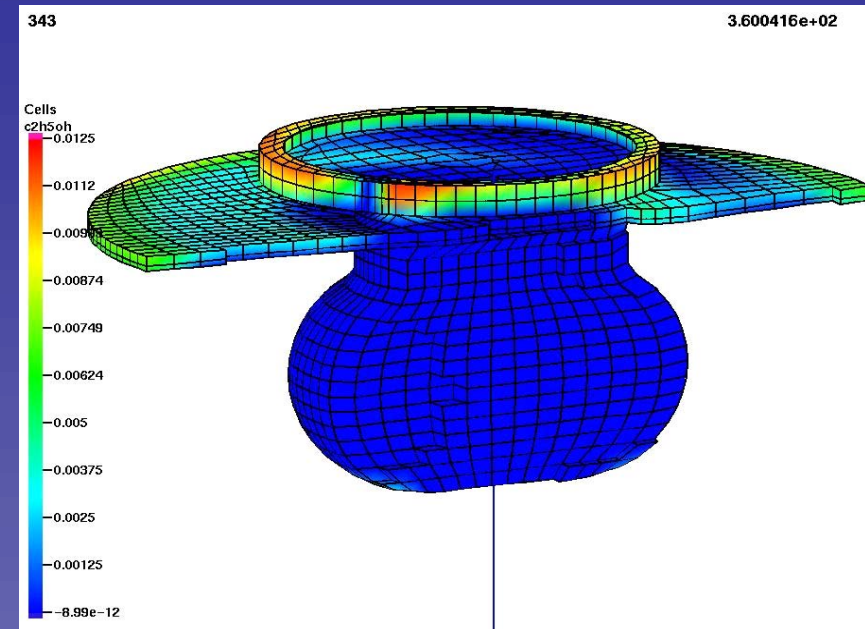


Simulation results

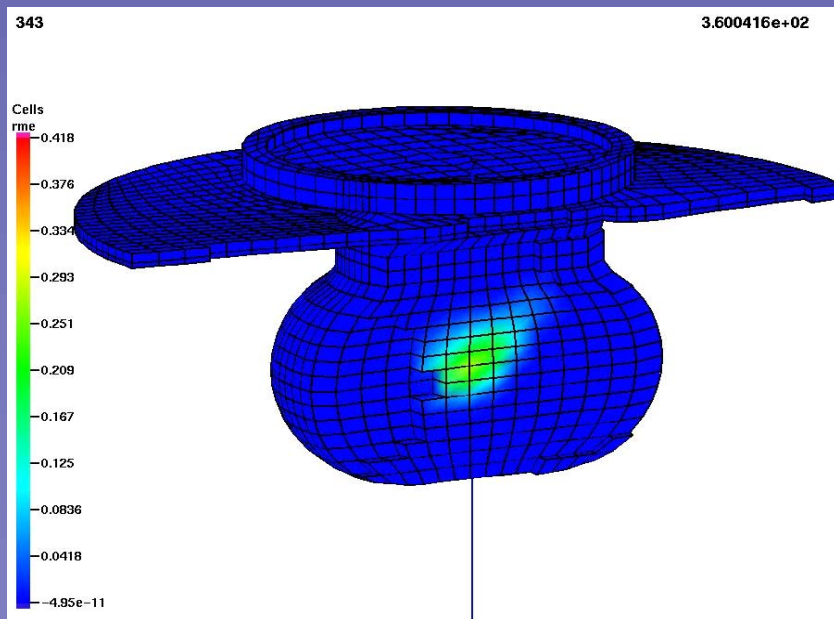
Ethanol mass ratio at 12 deg BTDC



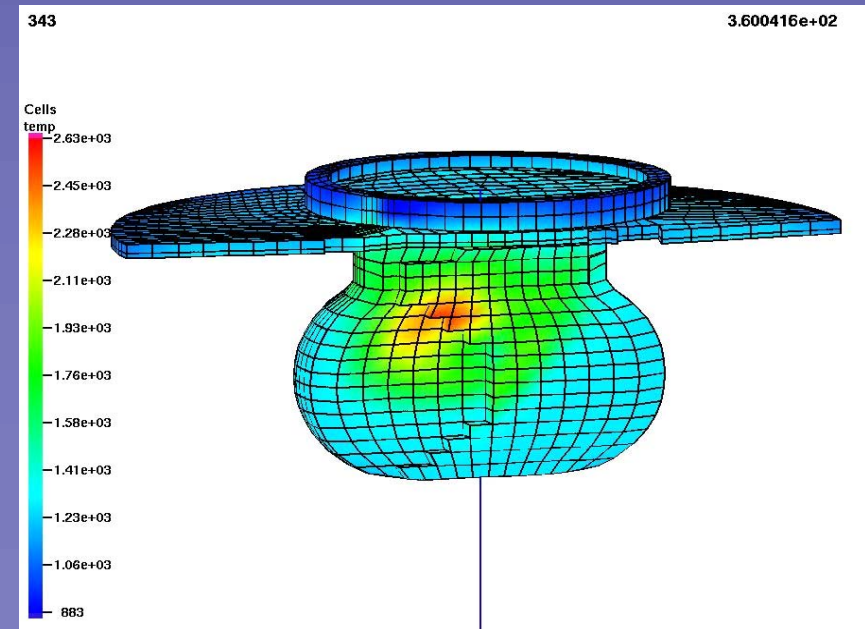
Ethanol mass ratio at TDC



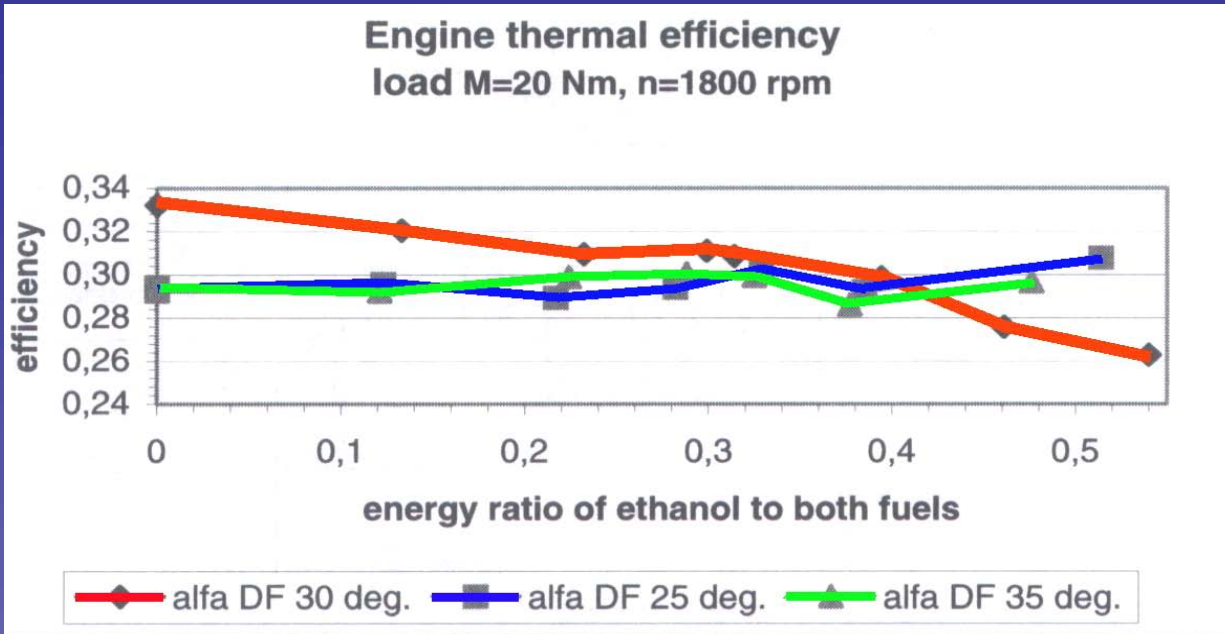
DF vapour mass ratio at TDC



Temperature at TDC

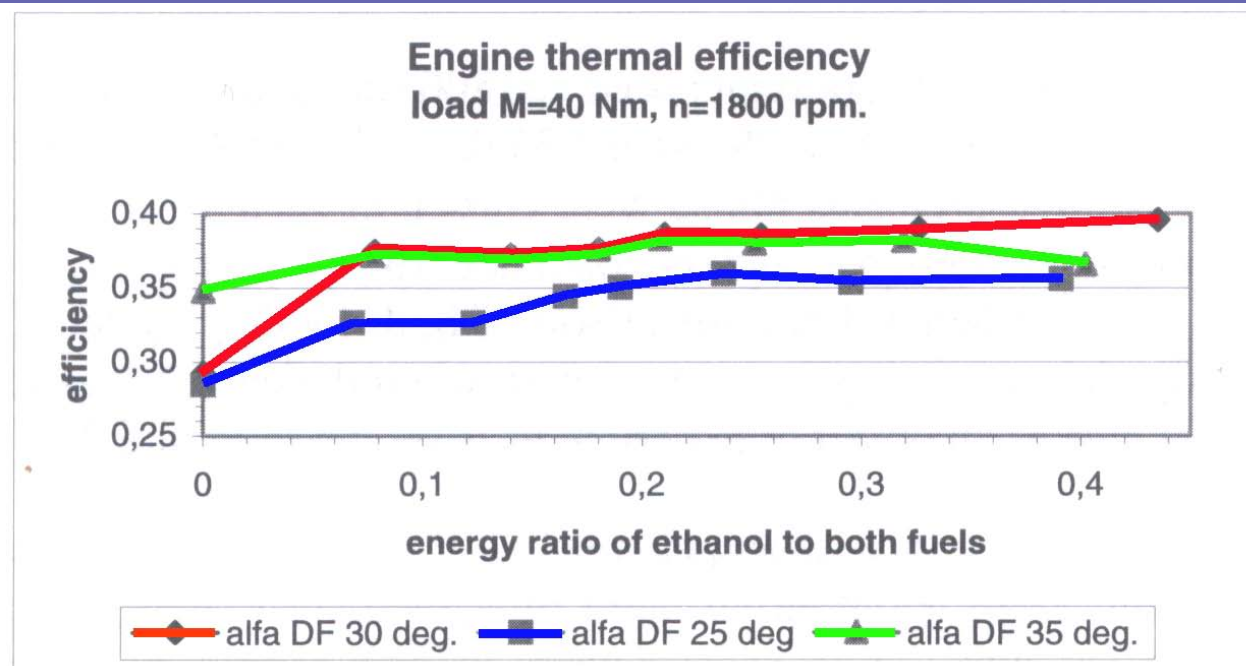


Engine thermal efficiency for different loads and energy ratio of ethanol to both fuels



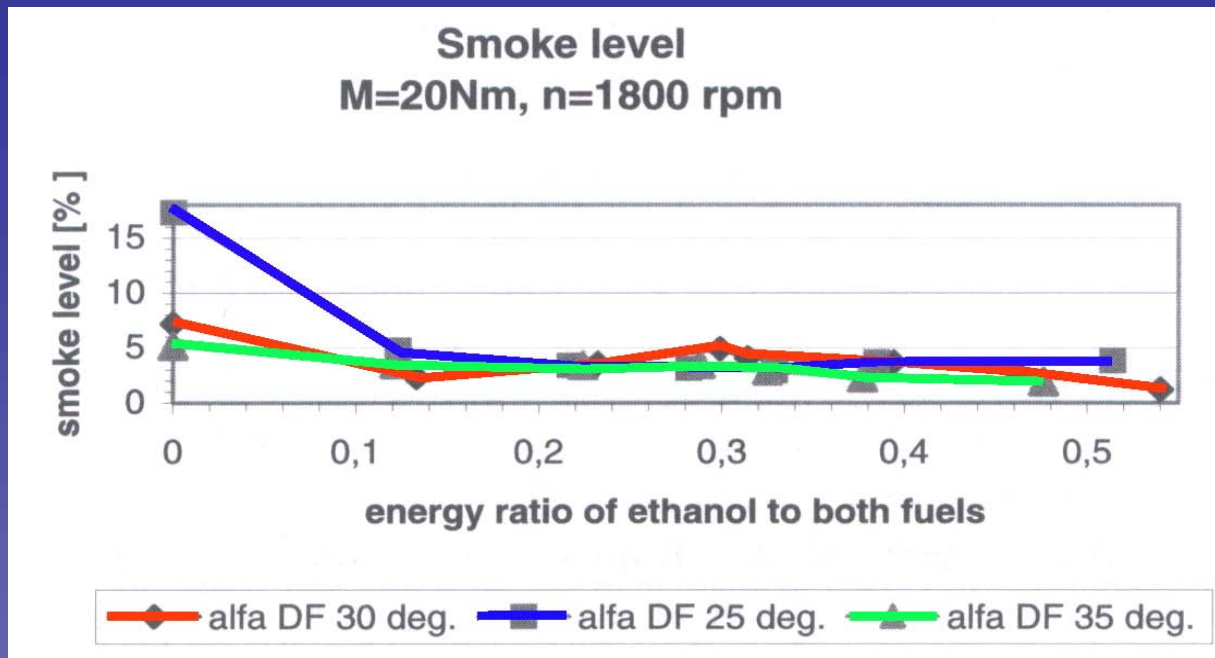
Experimental results

alfa DF – injection timing of DF

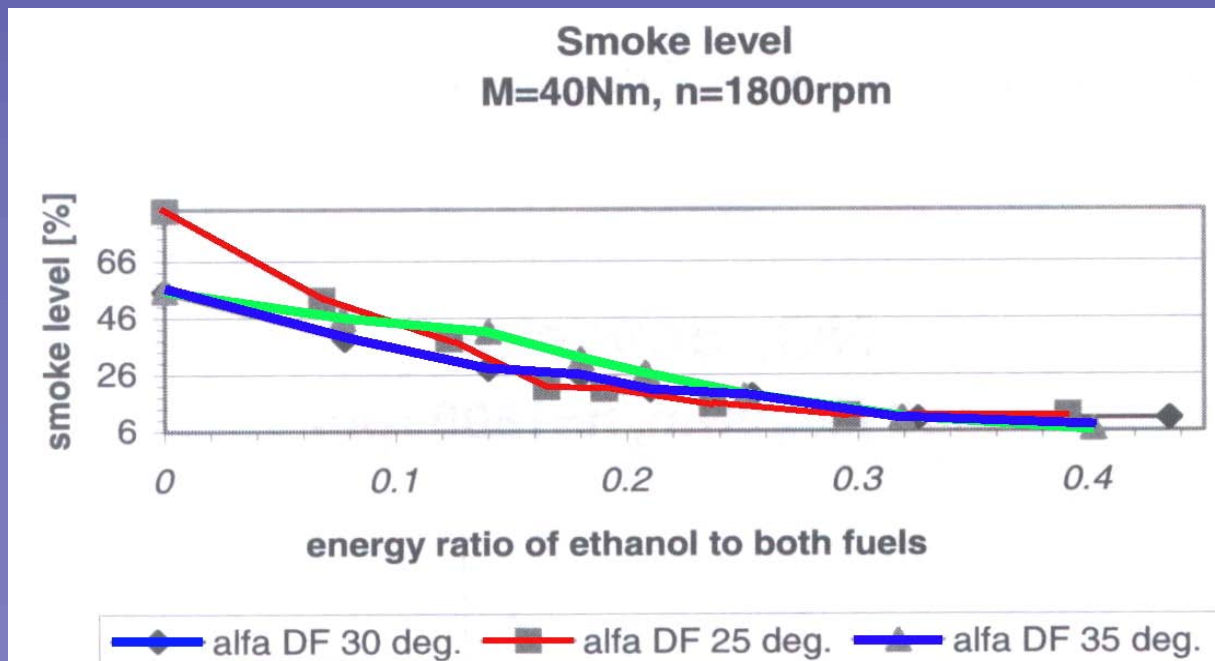


Engine smoke level for different loads and energy ratio of ethanol to both fuels

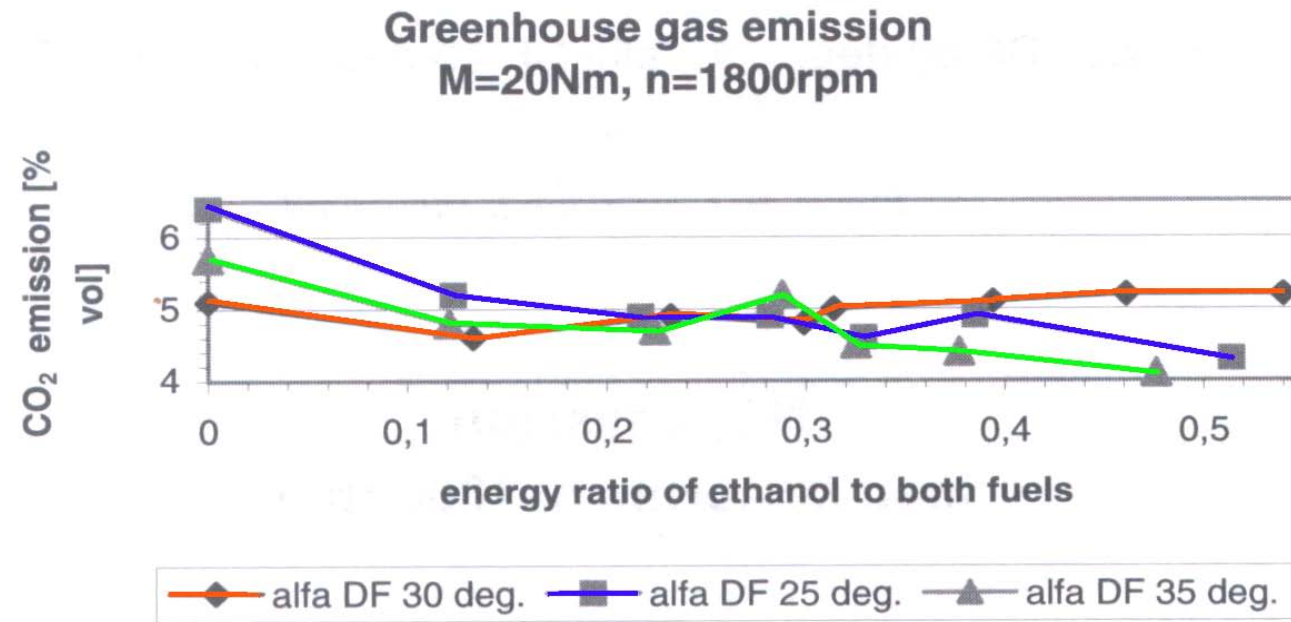
Experimental results



alfa DF – injection timing of DF

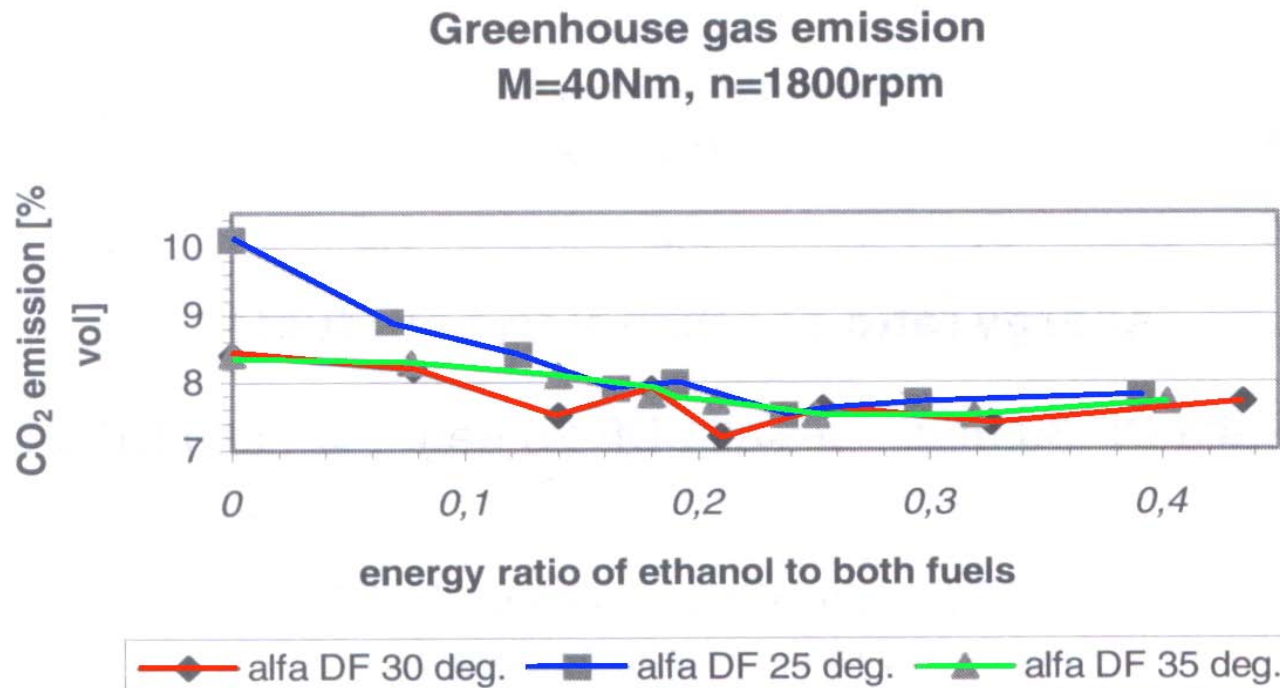


Engine CO₂ volume concentration for different loads and energy ratio of ethanol to both fuels



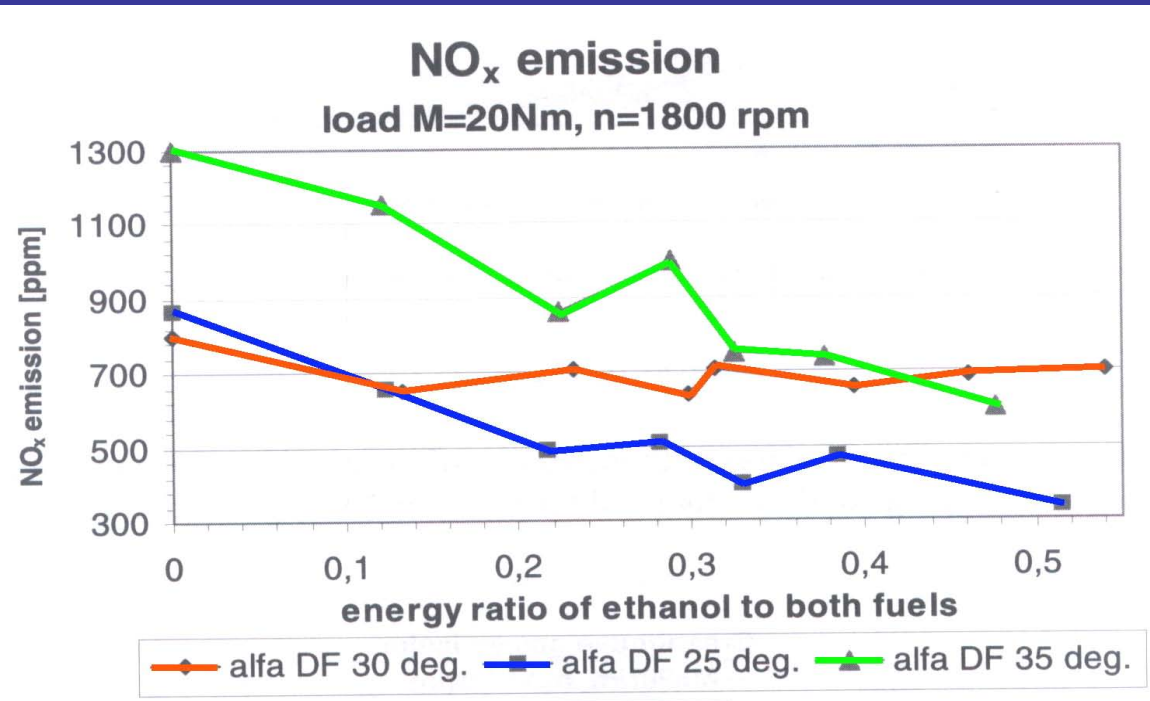
Experimental results

alfa DF – injection timing of DF

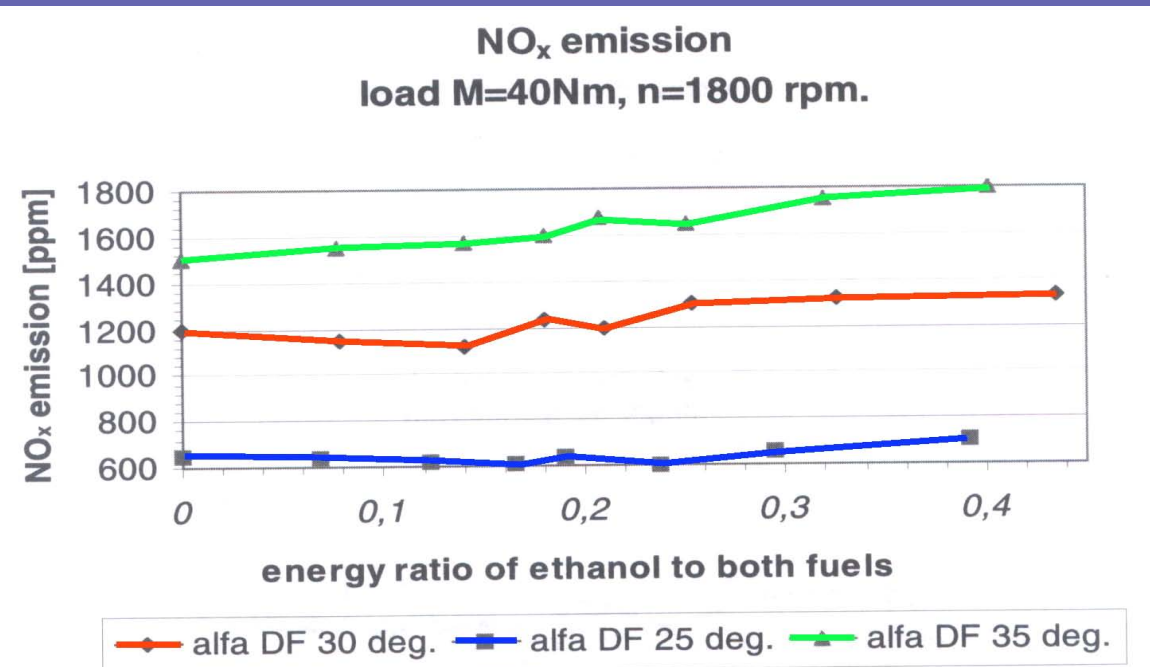


Engine NO_x volume concentration for different loads and energy ratio of ethanol to both fuels

Experimental results

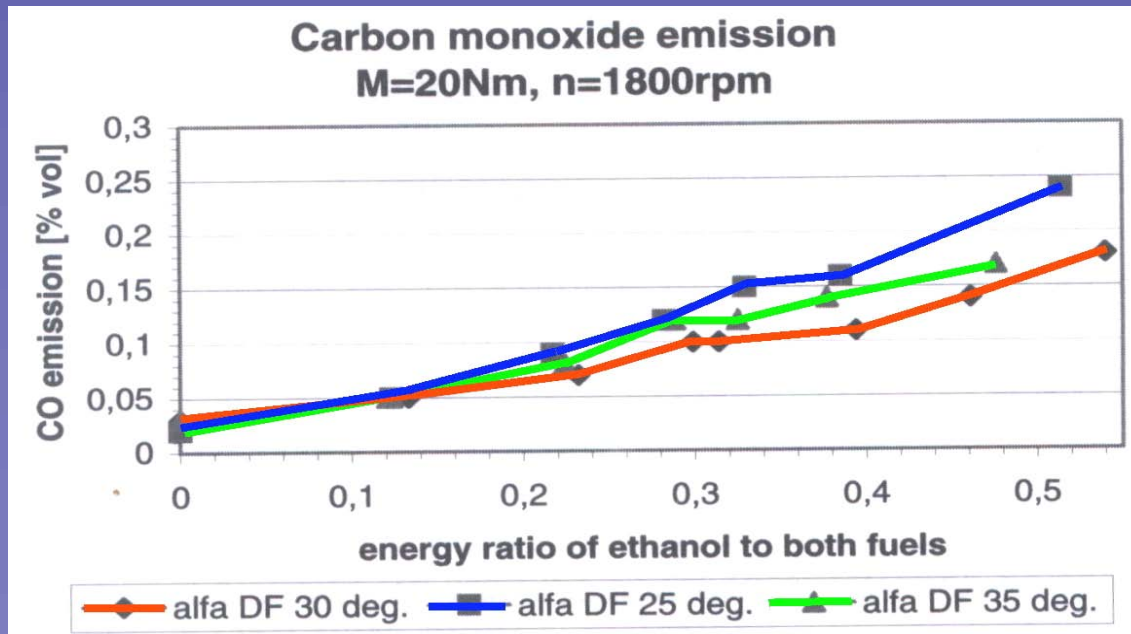
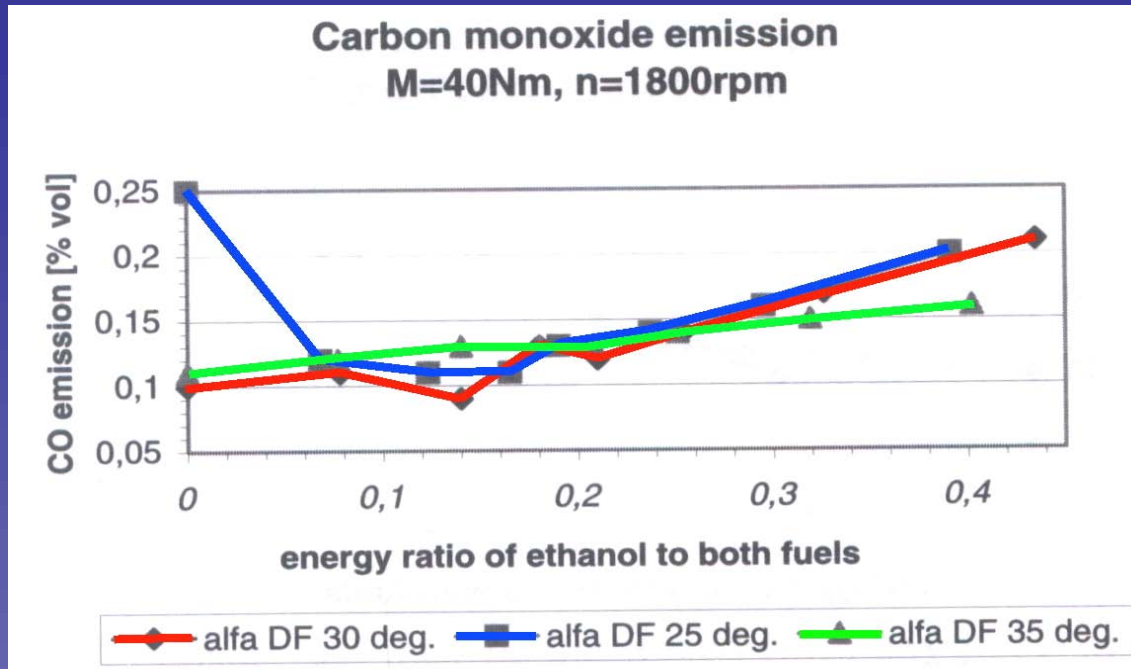


alfa DF – injection timing of DF



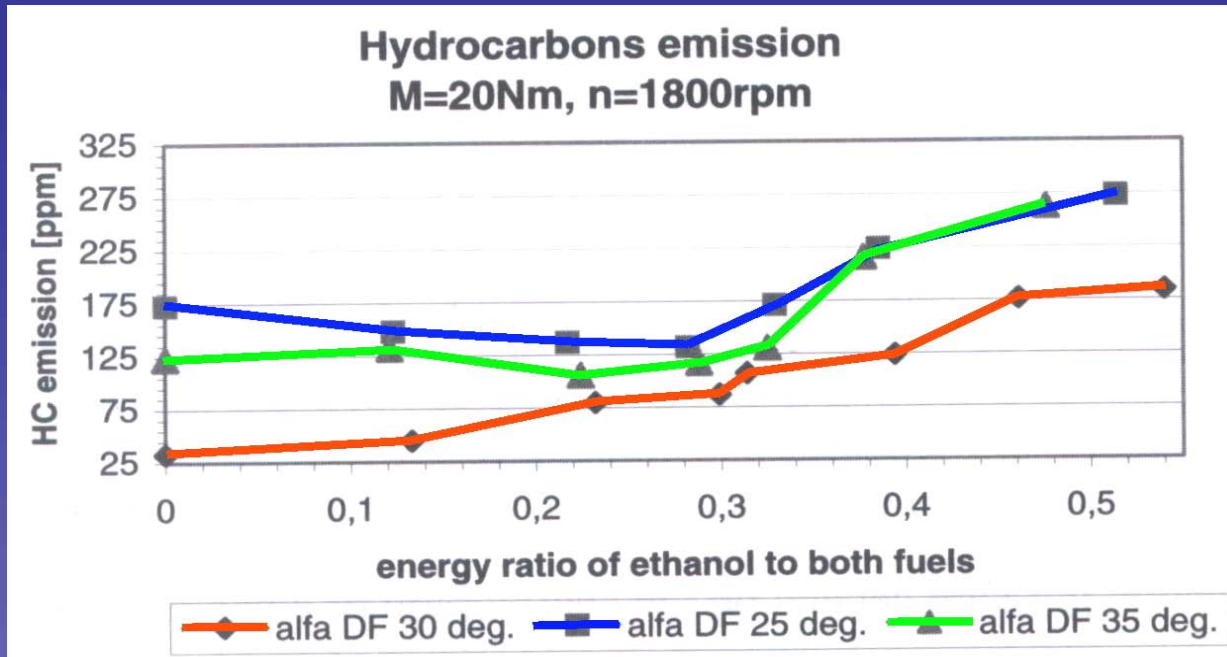
Engine CO volume concentration for different loads and energy ratio of ethanol to both fuels

Experimental results

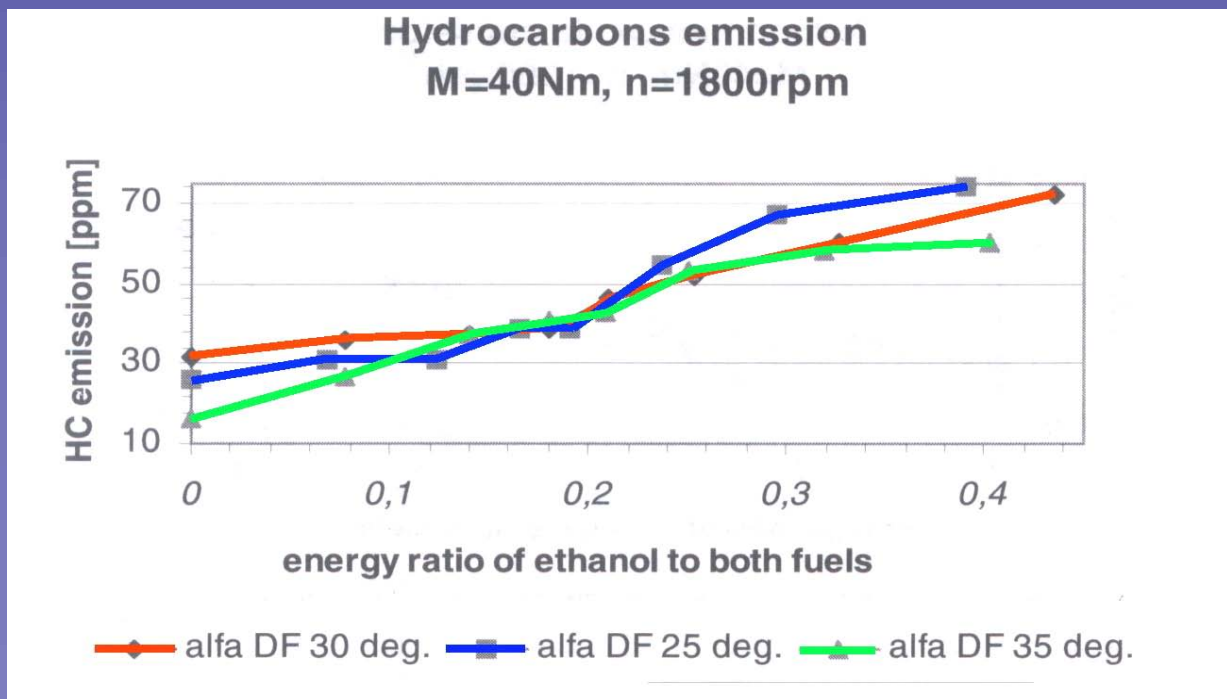


alfa DF – injection timing of DF

Engine hydrocarbons volume concentration for different loads and energy ratio of ethanol to both fuels

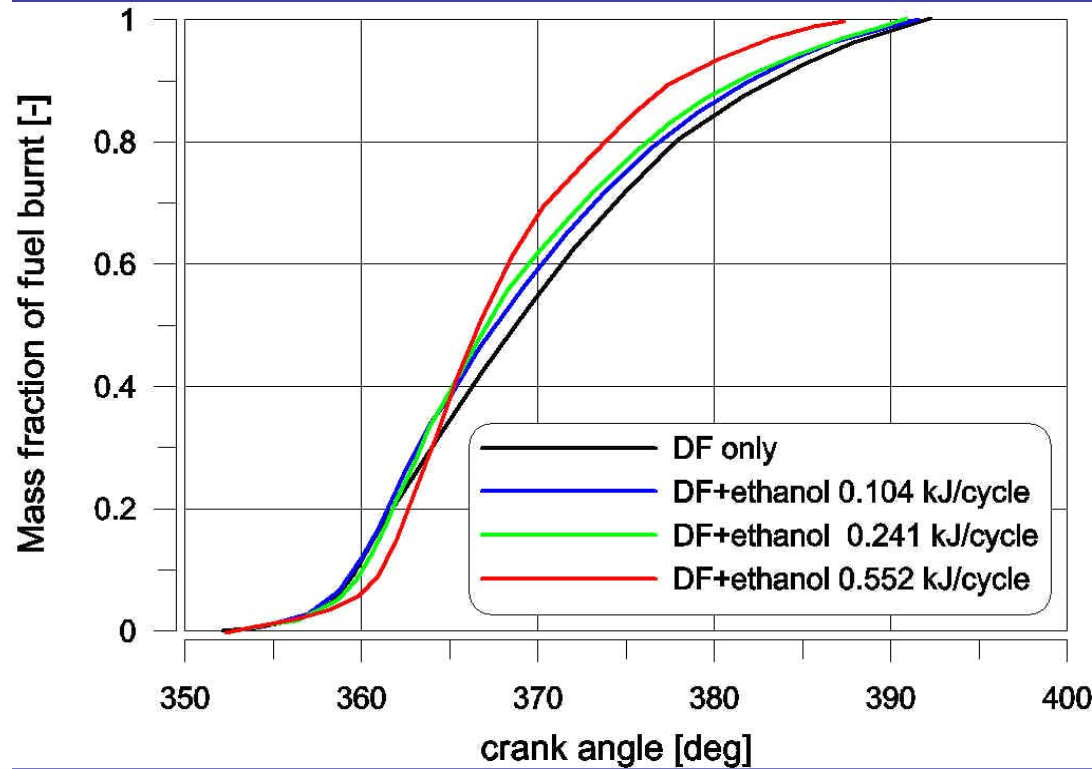


alfa DF – injection timing of DF

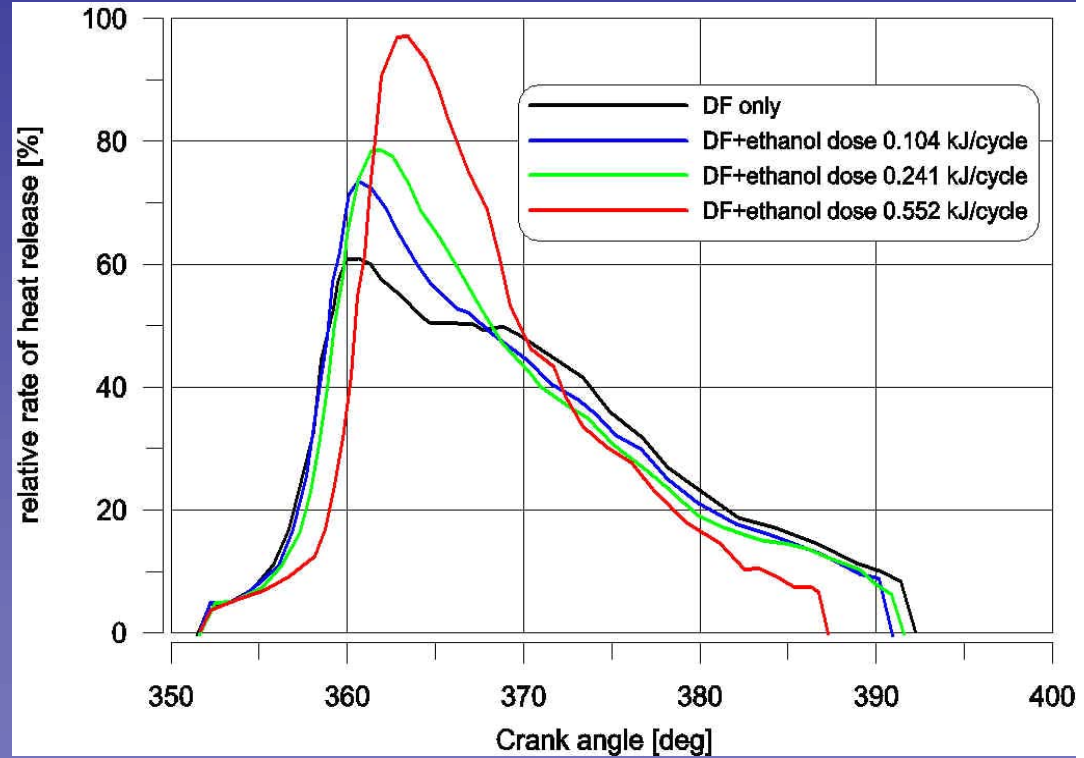


Combustion characteristics of ethanol + DF in CI engine

Mass fraction of fuel burnt



Relative ratio of heat release



CNG + DF FUELLING SYSTEM

- **CNG port injection → homogenous CNG-air mixture in cylinder**
- **Pilot dose of diesel oil → autoignition**
- **Autoignition temperature of CNG is higher than diesel oil**
- **CNG combustion is initiated by the first burnt evaporated fuel droplets outside of the injected diesel oil stream**
- **Applying of the homogenous air-natural gas mixture enable using the same conventional diesel engine without reducing of the compression ratio**
- **Big dose of pilot diesel fuel can cause higher hydrocarbon emission and smoke level**
- **Combustion process of CNG and DF depends on mass ratio of both fuels and spray characteristic of injectors**

Modelling thermo-chemistry

Chemical oxidation reaction of diesel oil:



Chemical oxidation reaction of natural gas:



Mass of CNG for the same combustion energetic value

$$m_{\text{CNG}} = (m_{1\text{DF}} - m_{2\text{DF}}) \frac{Q_{w\text{DF}}}{Q_{w\text{CNG}}}$$

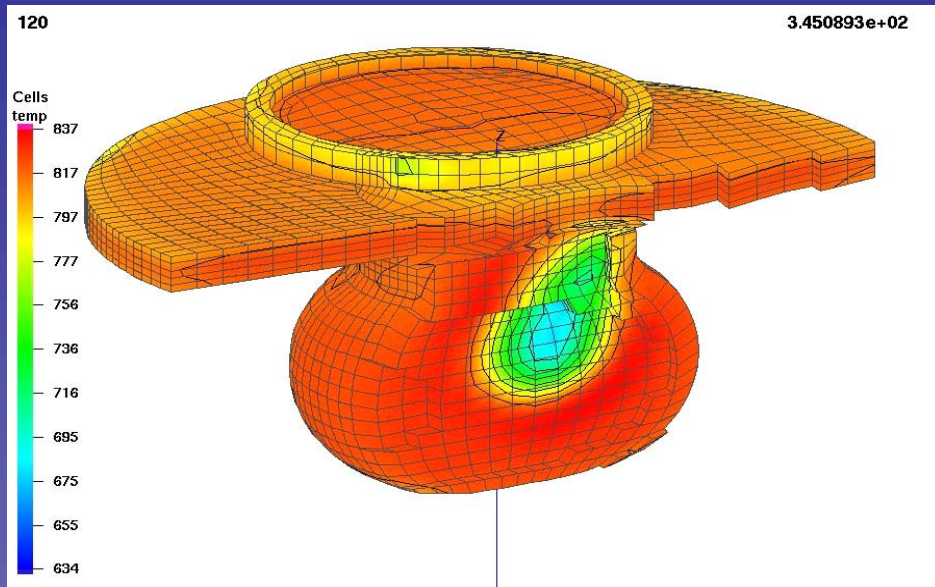
Calculated mass of CNG for full loads and one work cycle:

- | | | |
|----|----------------|--------------|
| 1. | 0,0169 g/cycle | n = 1200 rpm |
| 2. | 0,3276 g/cycle | n = 1800 rpm |
| 3. | 0,0436 g/cycle | n = 2200 rpm |

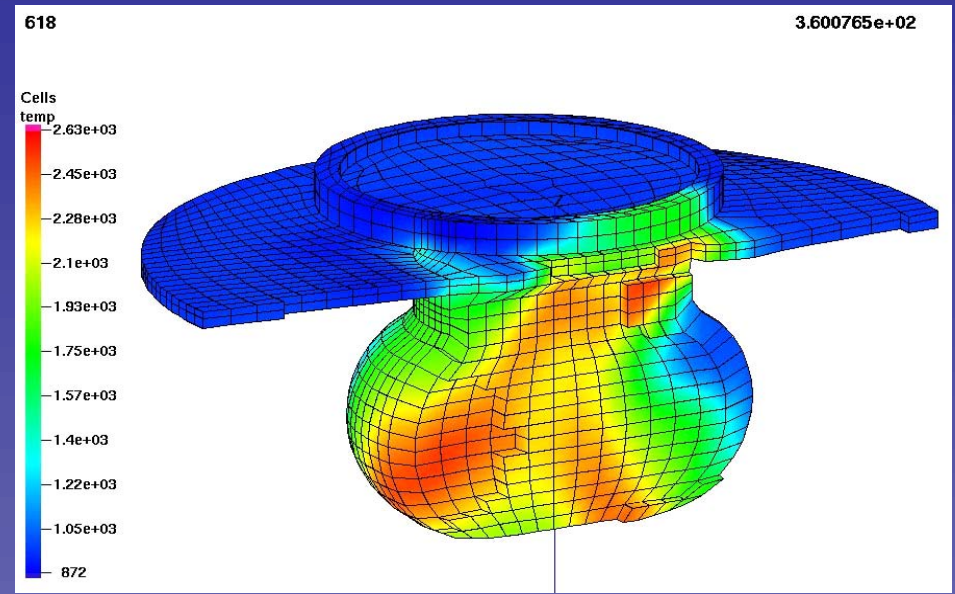
$$\lambda_r = \frac{m_{air}}{m_{\text{DF}} \left(\frac{A}{F} \right)_{\text{DF}} + m_{\text{CNG}} \left(\frac{A}{F} \right)_{\text{CNG}}}$$

Cylinder temperature

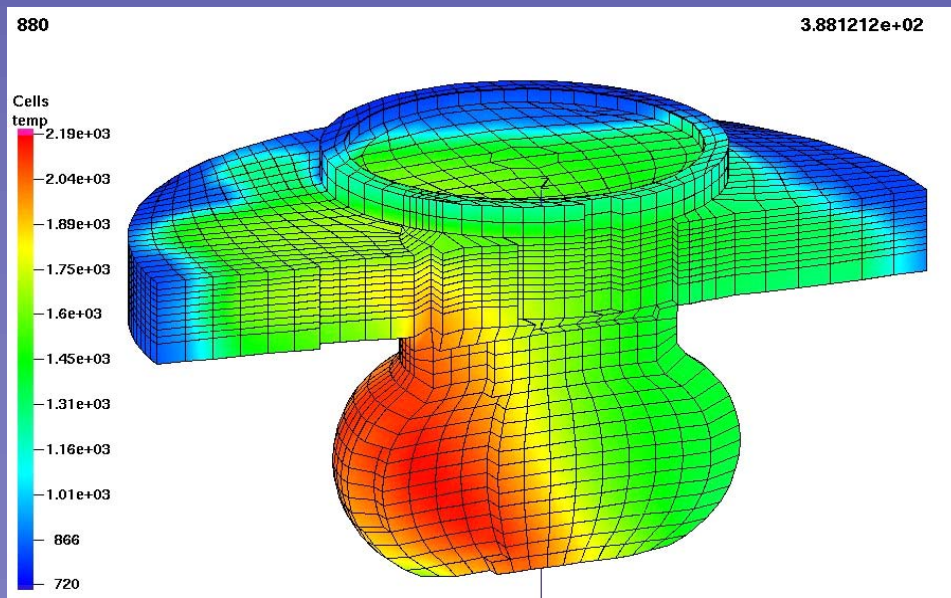
15 deg BTDC



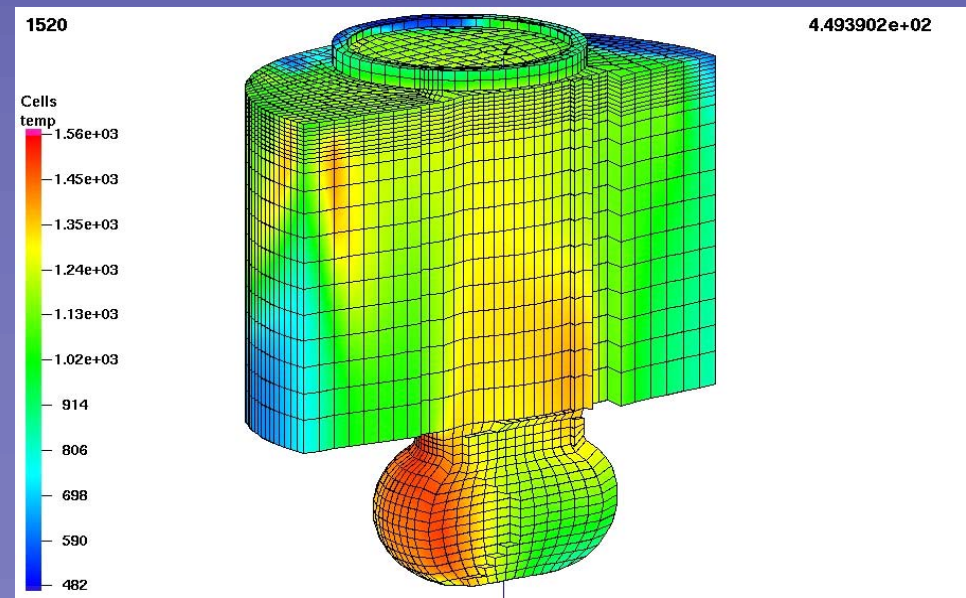
TDC



28 deg ATDC

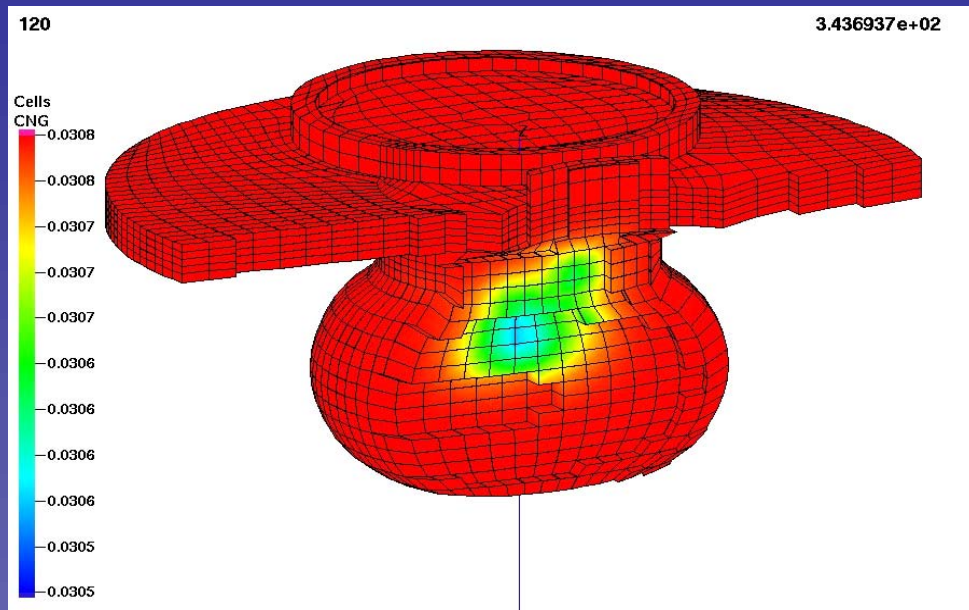


89 deg ATDC

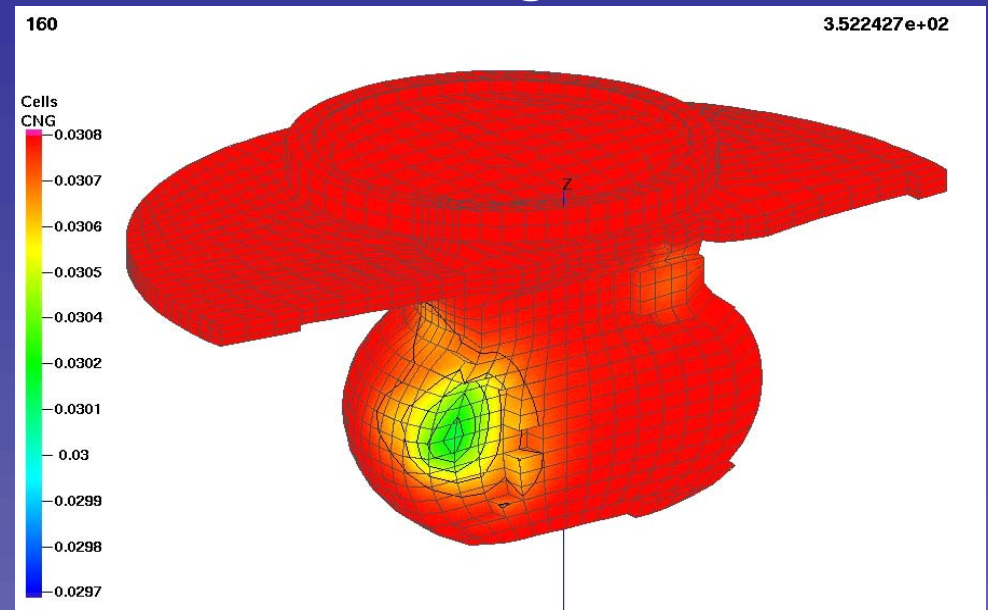


Mass concentration of CNG – 1800 rpm

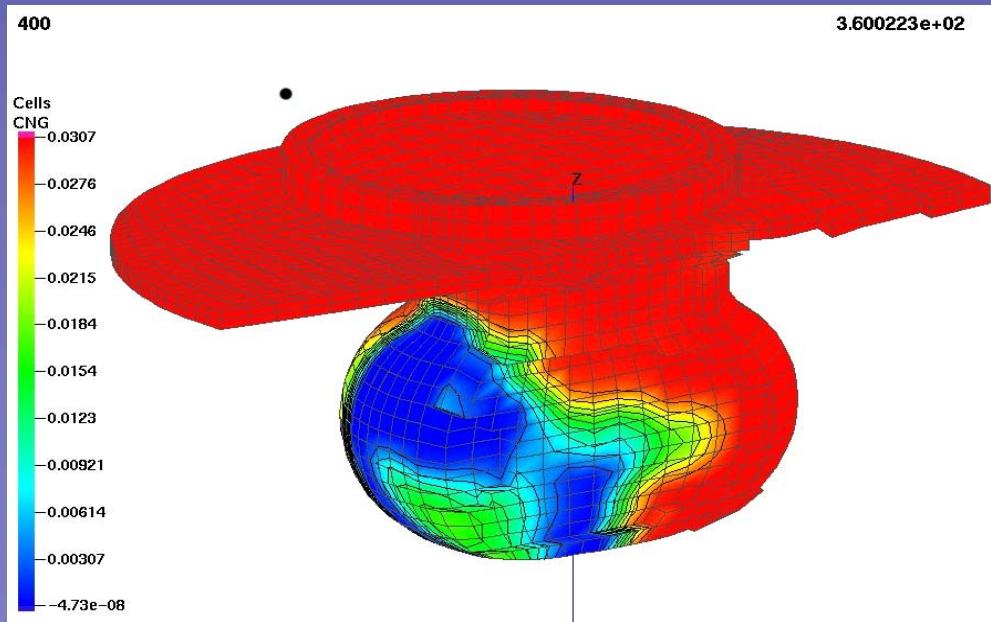
16 deg BTDC



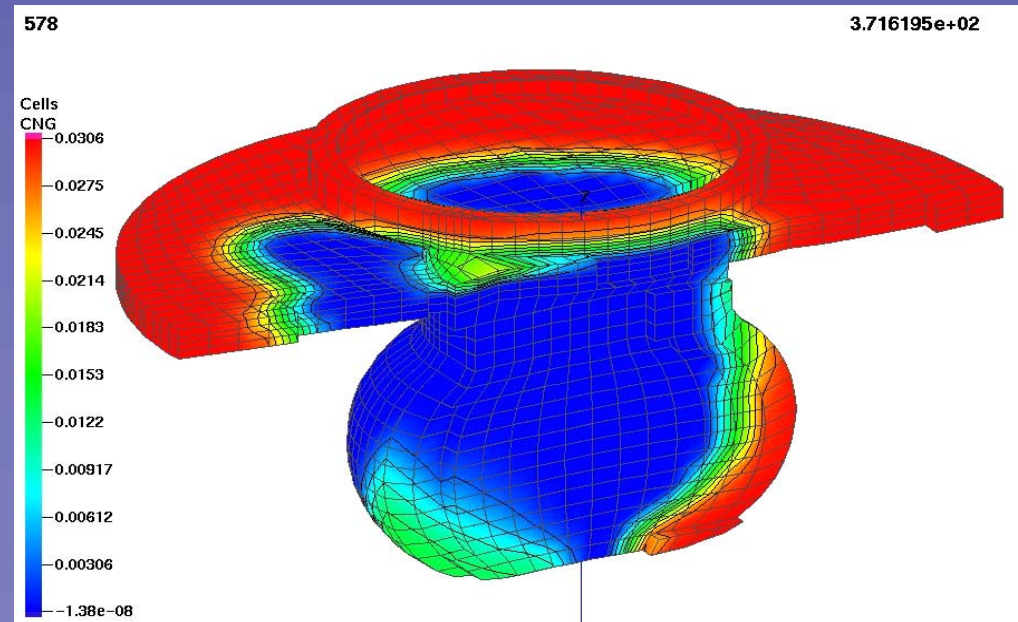
8 deg BTDC



TDC

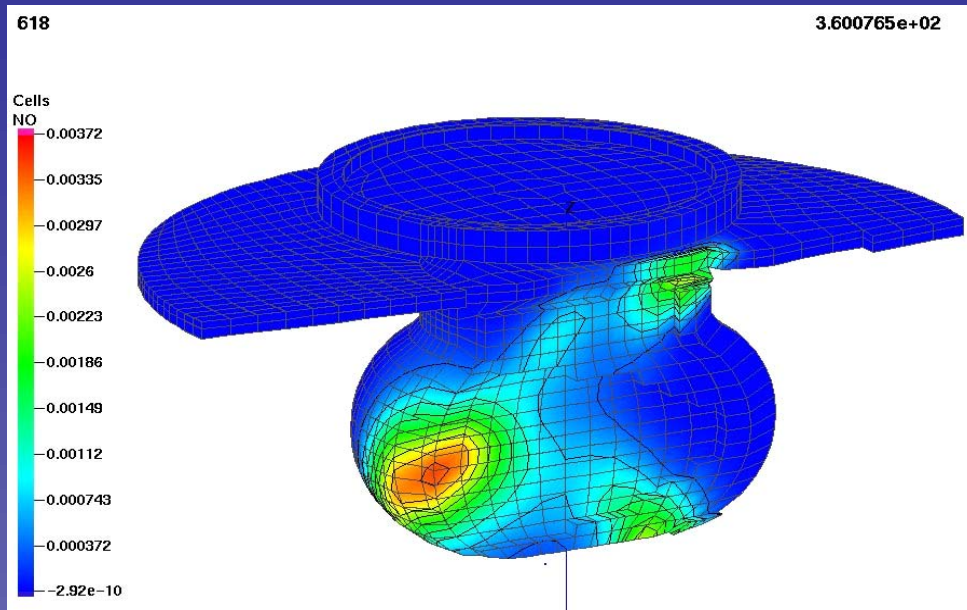


11 deg ATDC

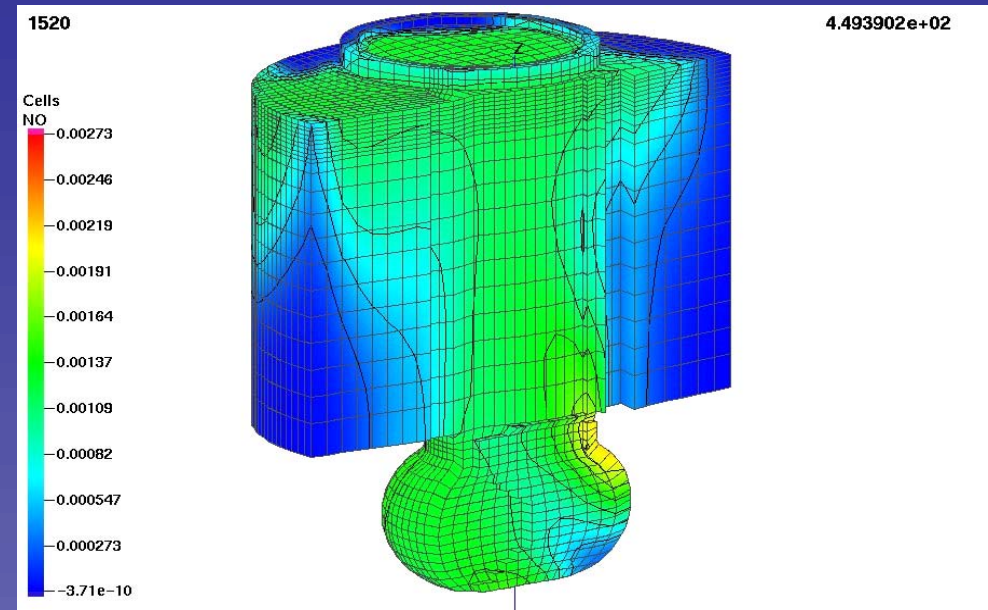


NO concentration – 1200 rpm

TDC

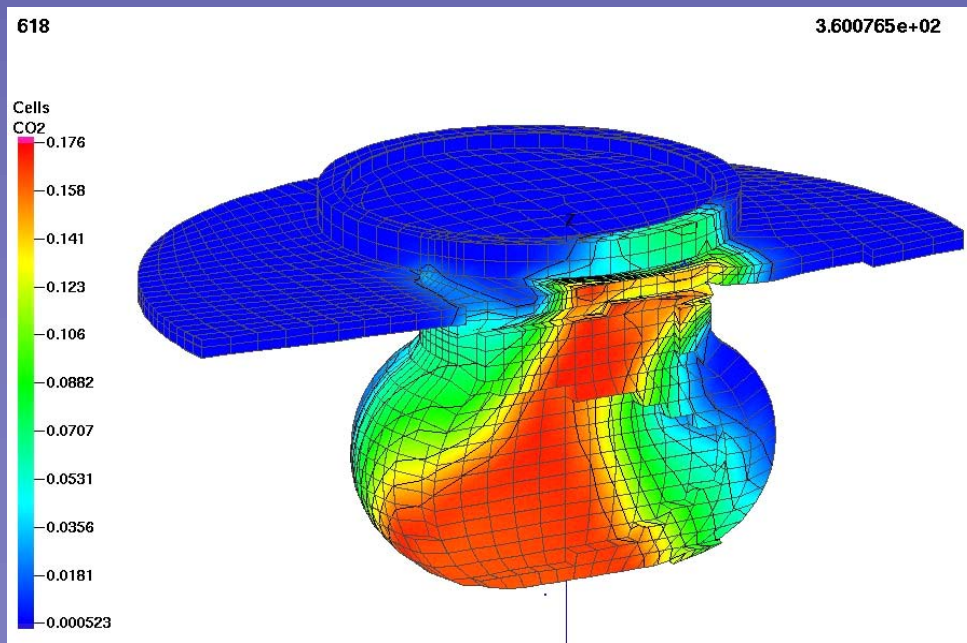


90 deg ATDC

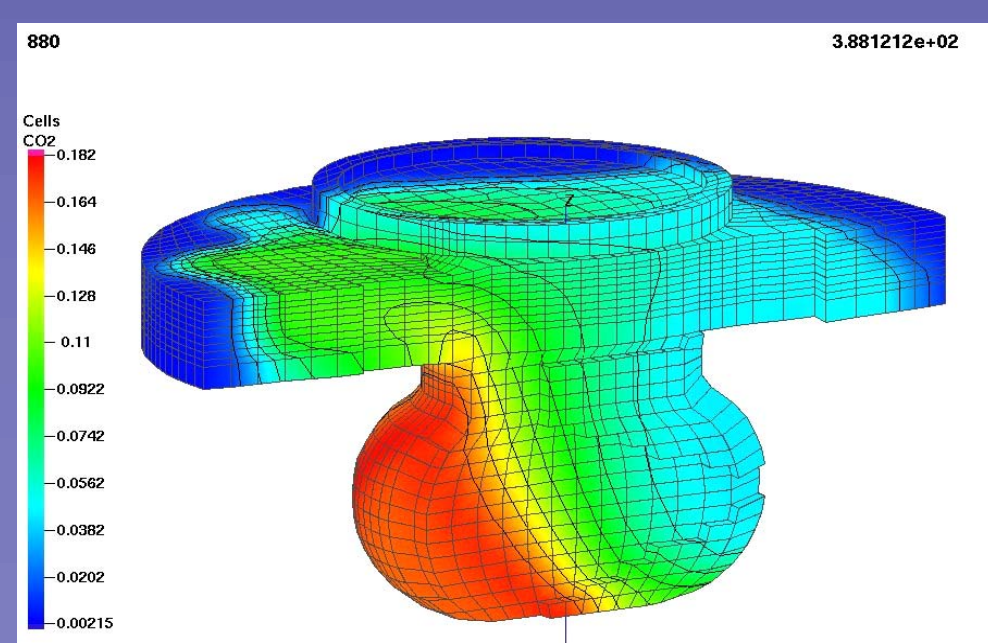


CO₂ mass concentration – 1200 rpm

TDC



28 deg ATDC

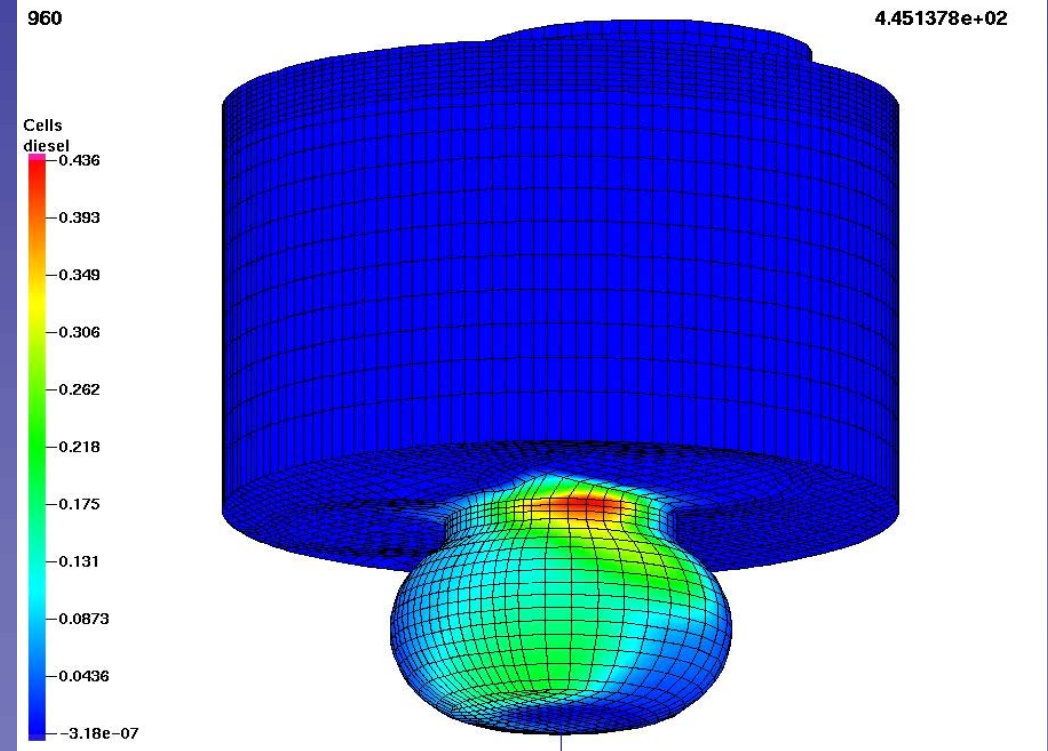
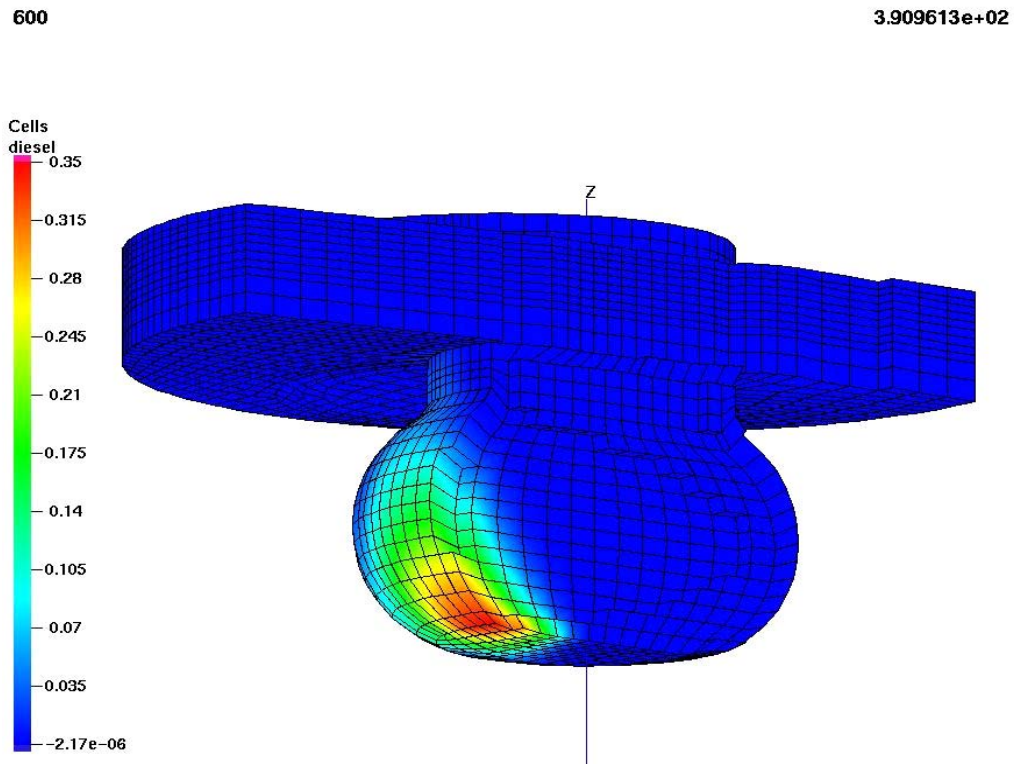


Simulation results Andoria 1HC 102

Diesel oil mass concentration – 2200 rpm

30 deg ATDC

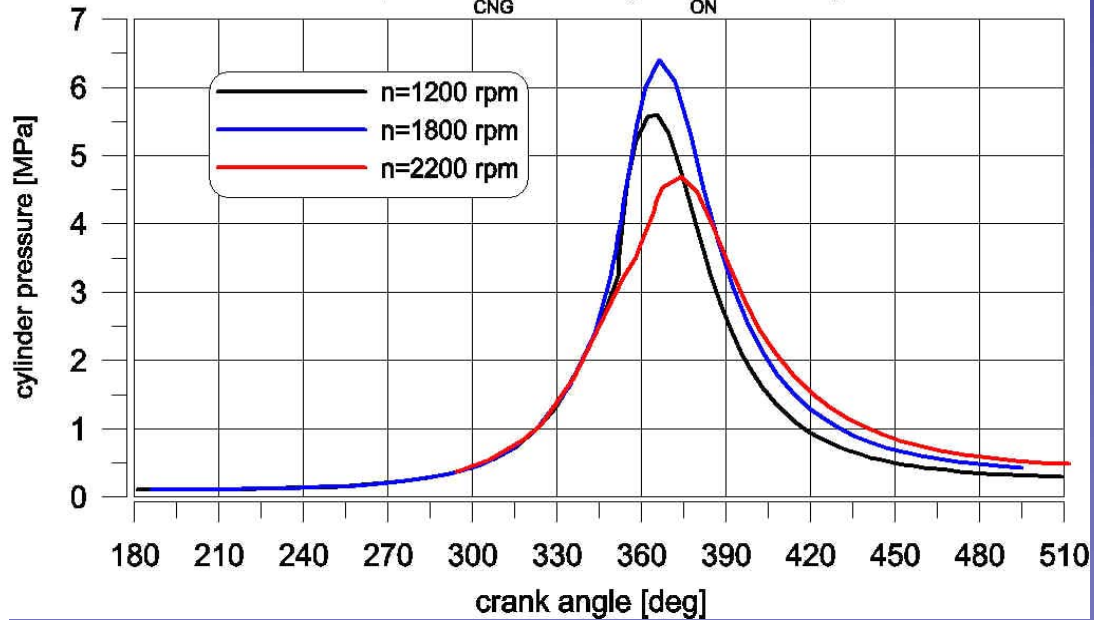
90 deg ATDC



Simulation results Andoria 1HC 102

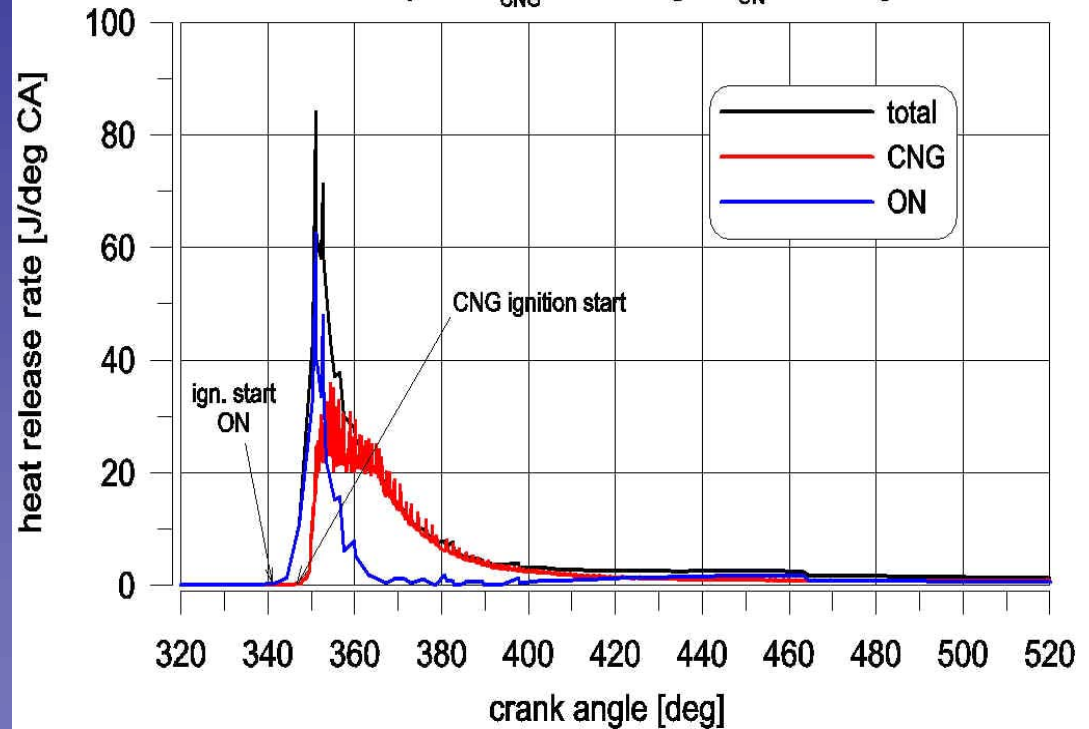
Cylinder pressure

n=1200 rpm; $m_{\text{CNG}} = 0,01695\text{g}$; $m_{\text{ON}} = 0,0173\text{g}$
n=1800 rpm; $m_{\text{CNG}} = 0,03276\text{g}$; $m_{\text{ON}} = 0,0173\text{g}$
n=2200 rpm; $m_{\text{CNG}} = 0,0436\text{g}$; $m_{\text{ON}} = 0,0173\text{g}$



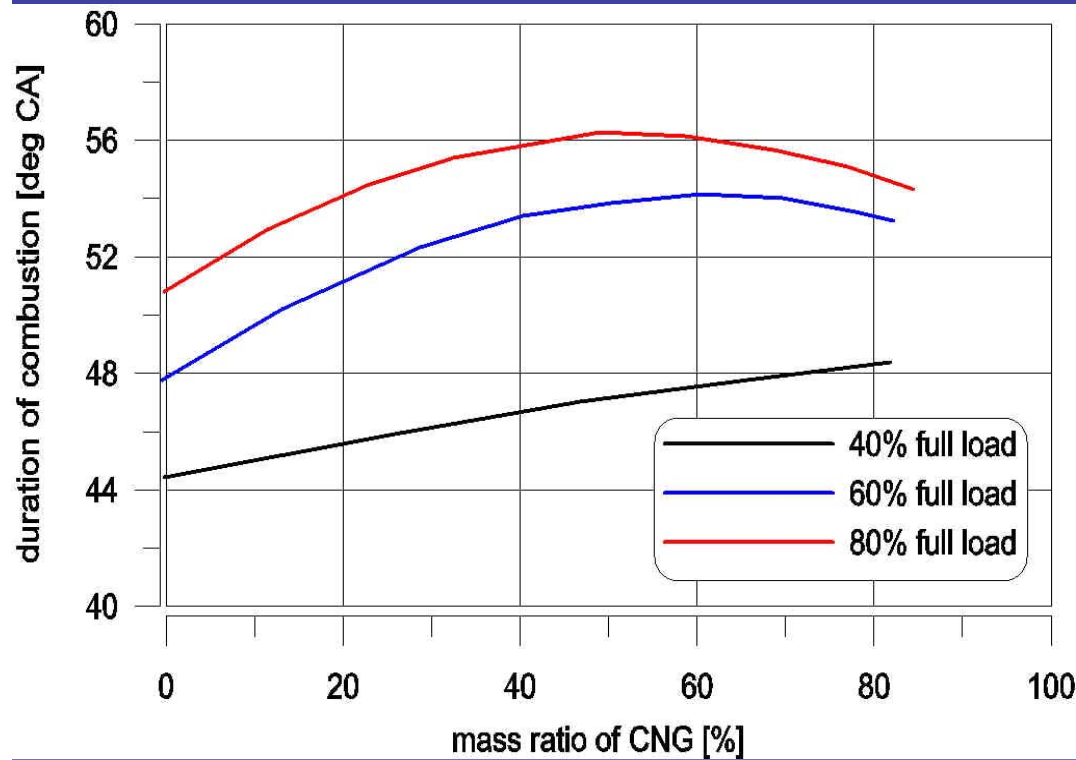
Heat release

n=1200 rpm; $m_{\text{CNG}} = 0,01695\text{g}$; $m_{\text{ON}} = 0,0173\text{g}$

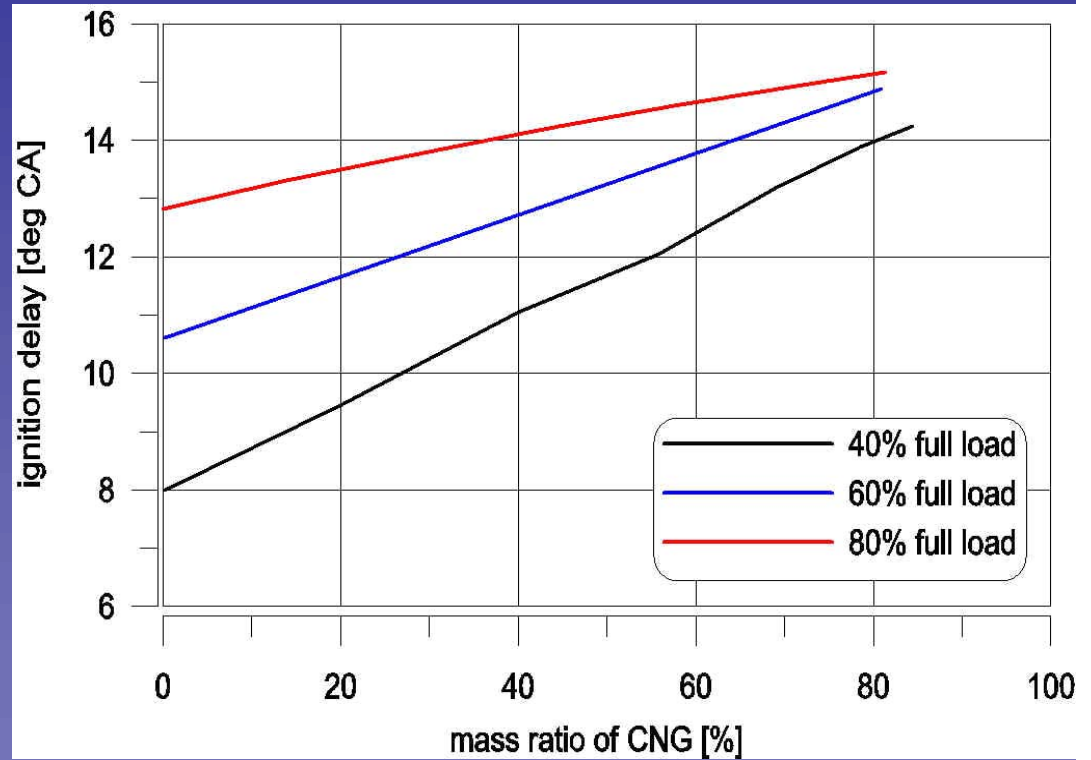


Experimental tests on CNG-diesel oil CI Andoria 4CT90 engine

Duration of combustion



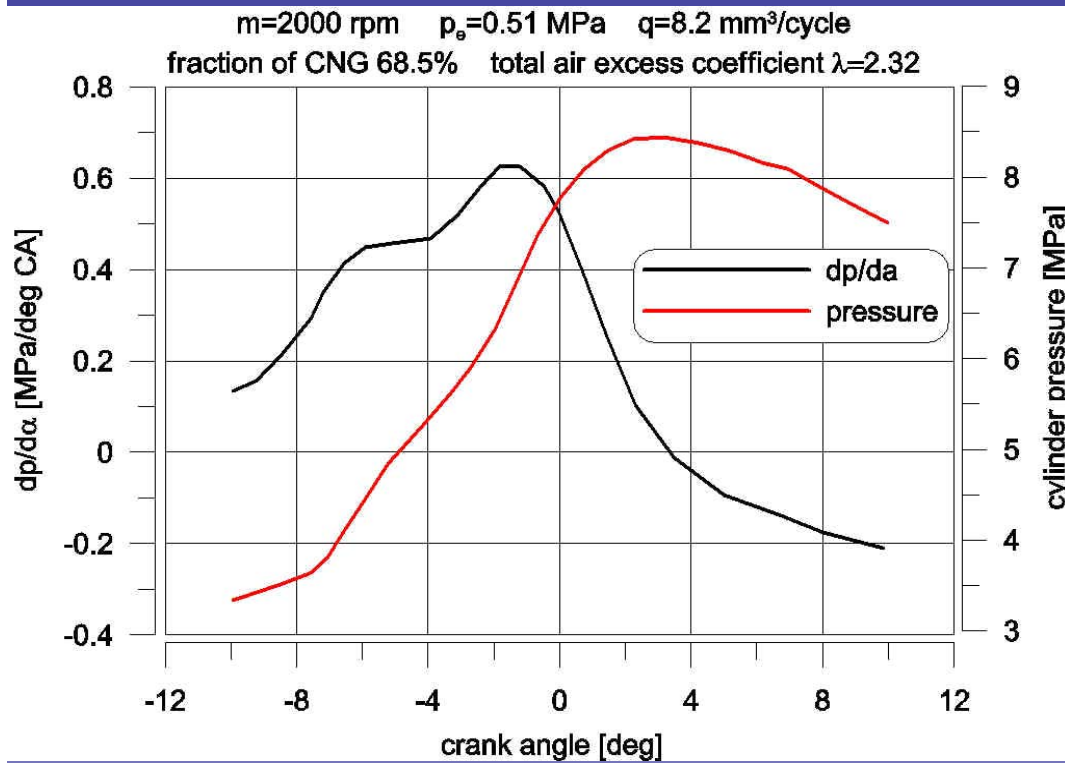
Ignition delay



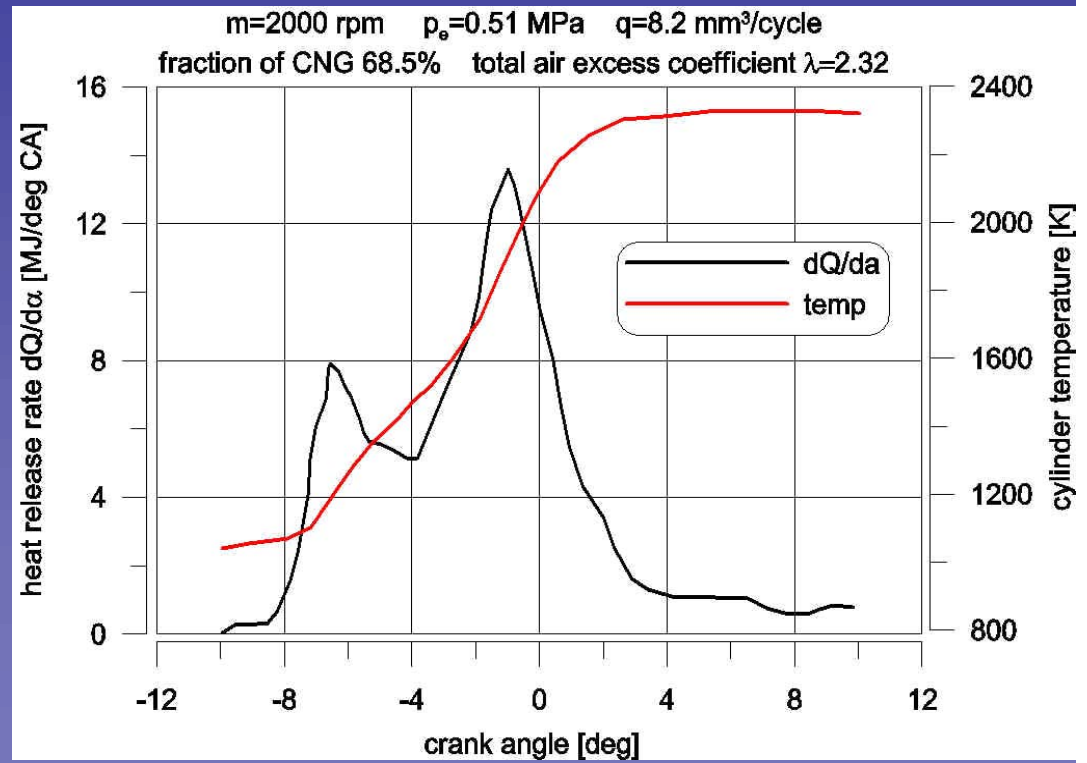
Experimental tests on CNG-diesel oil CI Andoria 4CT90 engine

$n=2000$ rpm

Pressure and pressure rise rate

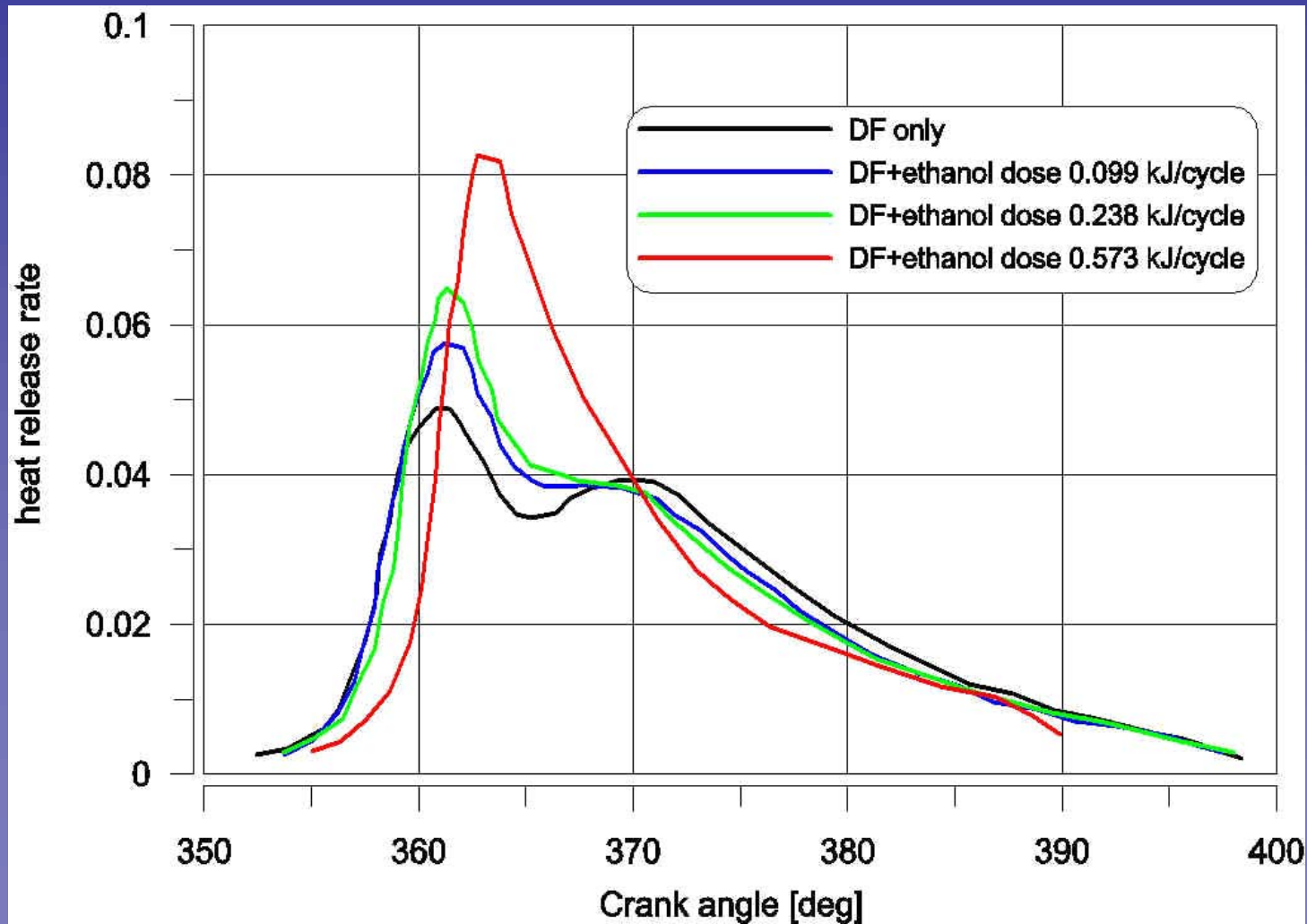


Temperature and heat release rate



Experimental tests on CNG-diesel oil CI Andoria 4CT90 engine

Heat release for different dual fuel mixtures at 1200 rpm
M=40 Nm; timing DF – 25 deg BTDC

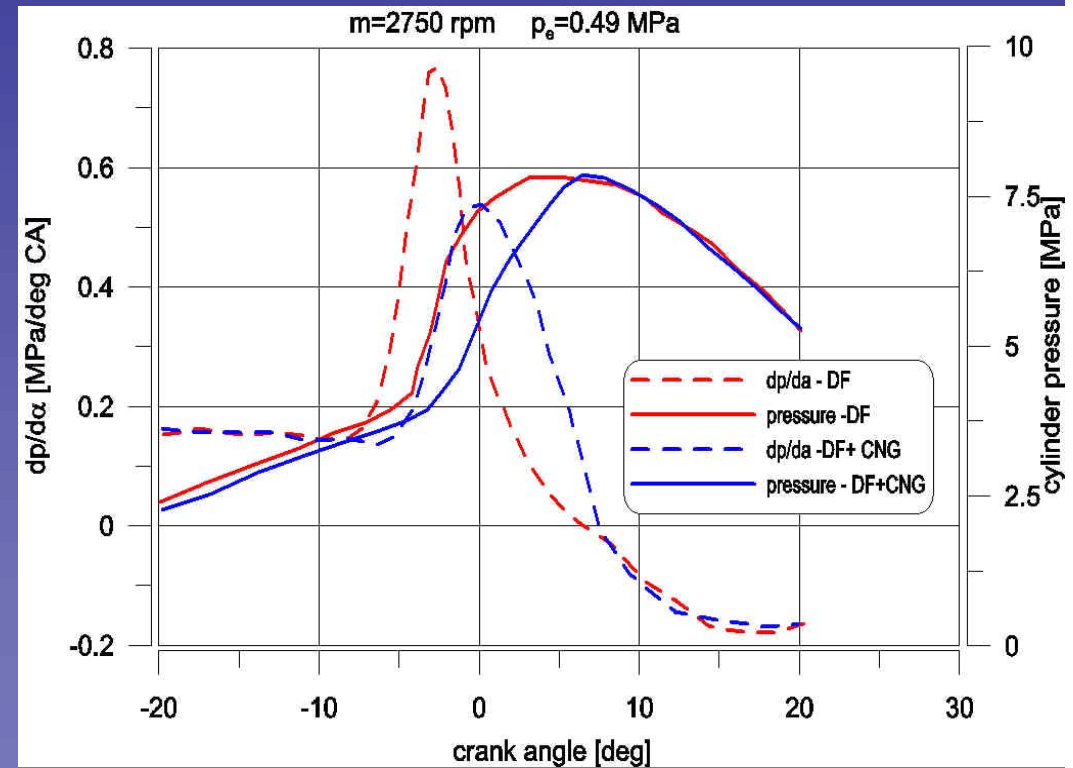
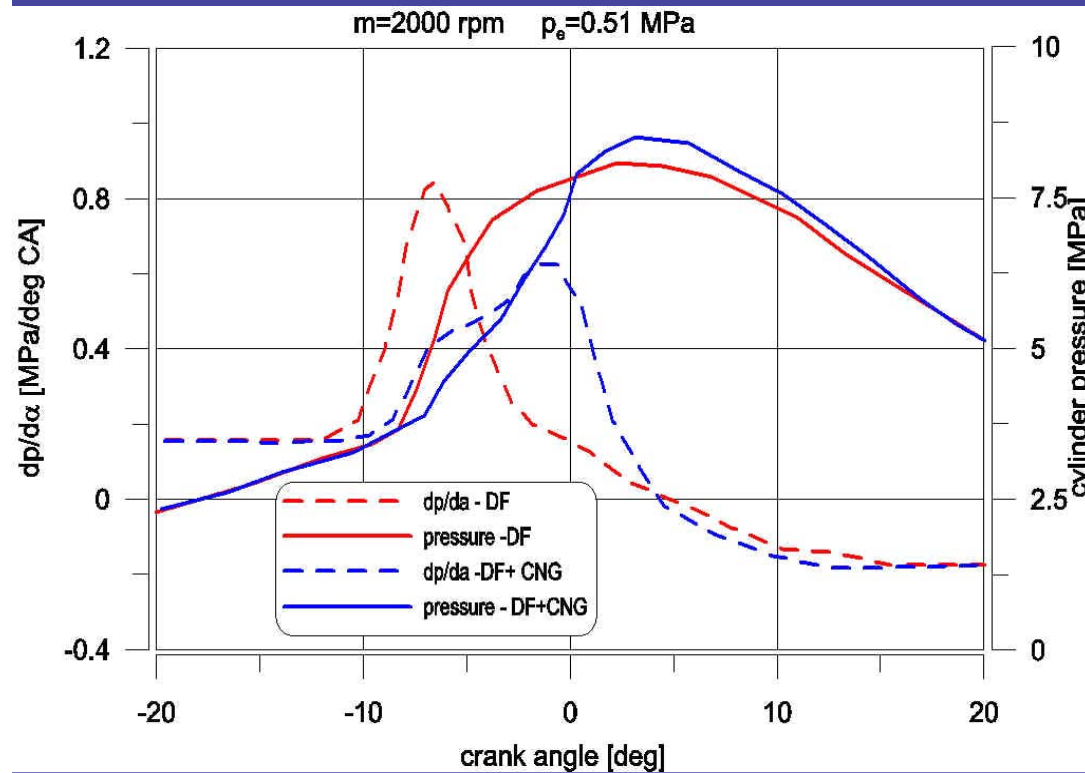


Experimental tests on CNG-diesel oil CI Andoria 4CT90 engine

Cylinder pressure and pressure rise rate for diesel fuel and dual fuel (CNG+DF)

$n=2000$ rpm; $b_{mep} = 0.51$ MPa

$n=2750$ rpm; $b_{mep} = 0.49$ MPa



CONCLUSIONS

1. Ethanol and natural gas may be a good additional fuels for CI engines when being injected into inlet port in a proper proportion to diesel fuel
2. Brake fuel conversion efficiency of dual fuel engines is better than pure diesel engine.
3. Dual fuelling results on lower CO₂ emission and smoke level. However, NOx emission increases when using CNG as additional fuel. For the other hand ethanol decreases NOx emission.
4. Ratios of ethanol or CNG to diesel fuel may be optimized regarding efficiency or toxic components of exhaust gases
5. Injection timing of diesel fuel should also be optimized for total efficiency, NOx emission and lower noise
6. Ignition and combustion in dual fuel natural gas engines is yet not fully recognized (combustion duration, kinetics and diffusion controlled combustion, noise, knock and cycle-by-cycle variation
7. Optimization of control parameters in dual fuel diesel engine is still an open problem

Thank you for your attention