

# Aerospace Testing EXPO2005

## Method for Category III (a) Autoland Performance Check

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EMBRAER

- **Objective**
- **Introduction**
- **Standard Procedures**
- **Methods Description**
- **Analysis and Results**
- **Conclusion**

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## ■ Objective

**Present a method for longitudinal and lateral distance determination for the Category III (a) Autoland touchdown performance evaluation.**

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## ■ Introduction

- Difficulties for DGPS antennas installation when conducting flight test on airports outside Brazil due to EMI/EMC polices restriction;
- Runway survey in order to get runway equations for data reduction is not practical in some airports
- Time and cost savings;
- Accuracy and precision shall be enough to allow adequate correlation with Monte Carlo Simulation.
- Two Methods for touchdown performance evaluation and crosscheck (one will be backup once proved equivalence);

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## ■ Standard Procedures

- DGPS
- Glideslope/Localizer signals
- Belly Camera.
- WAAS

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## ■ Methods Description

- Two Methods were developed for the Autoland Performance Check with crosscheck/backup purposes:
  - Method I: FPA Corrected Category III (a) Autoland Performance Check
  - Method II: Airport Aids Category III (a) Autoland Performance Check
  
- DGPS was (and is still being) used for method validation (only some Brazilian Airports)
  
- Belly Cam will be available for all flights in order to sort out doubts as necessary (in case of Certification request)

## ■ Method I

- This method is a Visual Basic based program using the Excel with DDE (Dynamic Data Exchange) feature for feeding data on the required input strings for real time calculation.
  
- Program Features:
  - Airport Database
  - Parameters Setting
  - Results Summary Table
  - Longitudinal and Lateral Distance Graphic
  - Touchdown Rate Graphic
  - Runway Localizer Beam Survey Plot

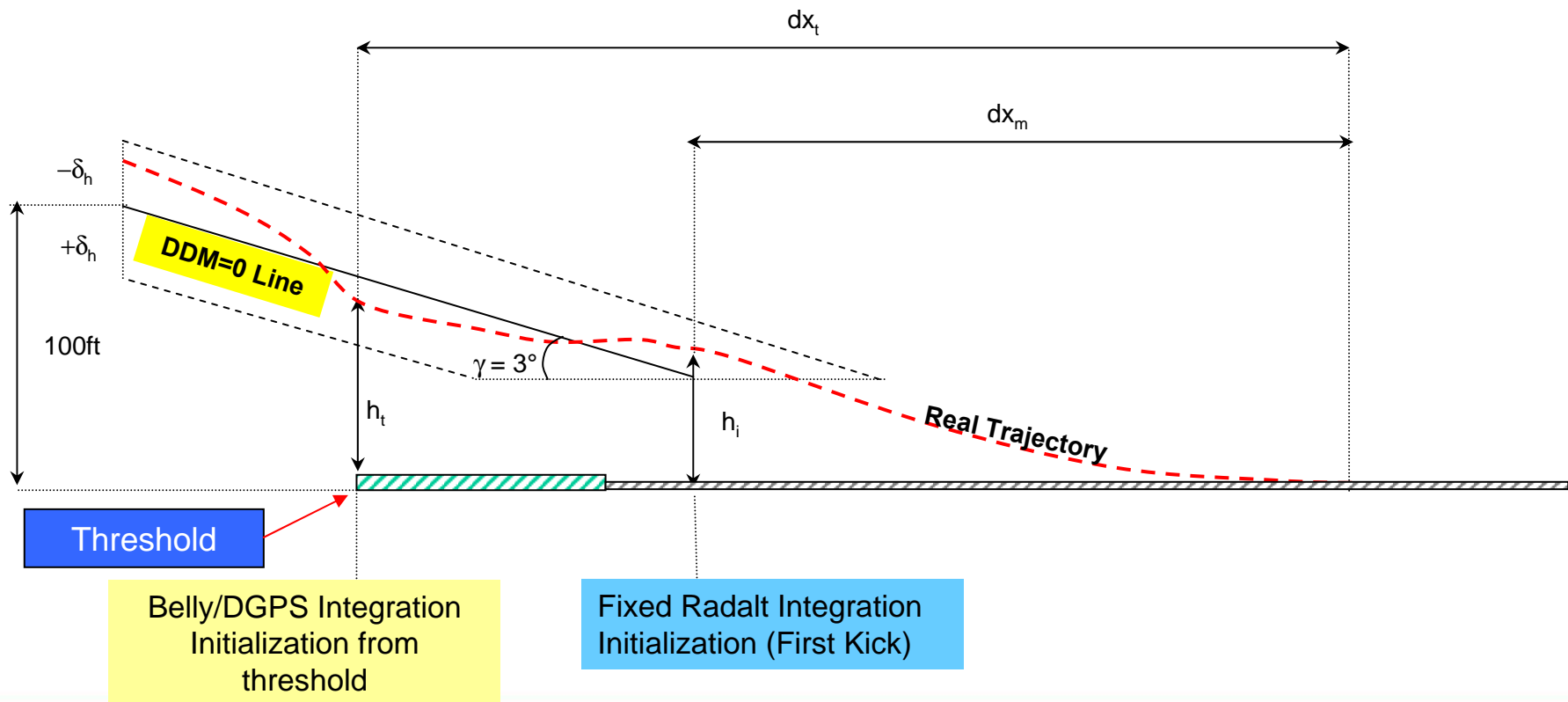
## ■ Method I

- Calculation: Longitudinal Distance (dx)
  - Integrates the distance from the initialization point.
  - Some main questions to be answered:
    - What should be the initialization triggering point?
    - How to determine this point?
    - How is the expected accuracy in order to have an adequate correlation to the Monte Carlo simulation?

## ■ Method I

- Calculation: Longitudinal Distance (dx)
  - **Fixed Radalt**

$h_t$  : Real Threshold Height  
 $h_i$  : Initial Estimated Height



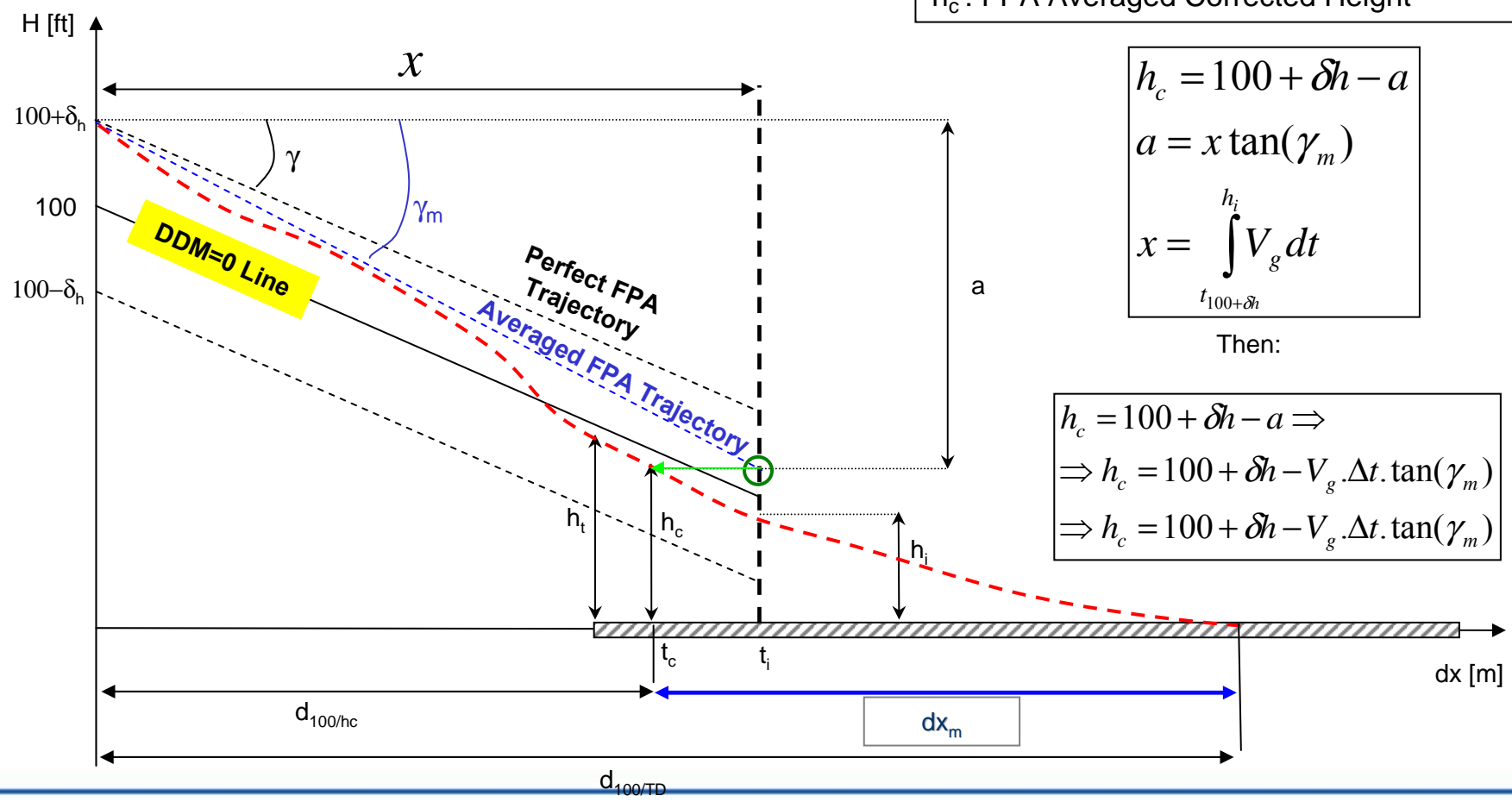
## ■ Method I

- Calculation: Longitudinal Distance ( $dx$ )
  - Fixed Radalt
    - Whenever  $h_t \neq h_i$  longitudinal distance error will be  $dx_t - dx_m$
    - How to set  $h_i$  in order to minimize error since  $h_t$  is unknown?
  - Some boundary or relevant conditions:
    - $\delta h$  (100ft)  $\in [-12, 12]$ ft, otherwise aircraft would get Excess Dev. (AC 120-29A)
    - Autoland Control law will shift to the 3° flight path angle command between 100ft and 50ft
    - Keeping the 3° FPA between 100ft and 50ft will keep the aircraft parallel to the glideslope DDM=0 line, i.e. within  $[-12, 12]$ ft.
    - Aircraft does not necessarily fly a perfect parallel FPA trajectory from the DDM=0 Line
    - Flare Control Law initiates at 50ft

## Method I

- Calculation: Longitudinal Distance (dx)

$h_t$  : Real Threshold Height  
 $h_i$  : Initial Estimated Height  
 $h_c$  : FPA Averaged Corrected Height



$$h_c = 100 + \delta h - a$$

$$a = x \tan(\gamma_m)$$

$$x = \int_{t_{100+\delta h}}^{h_i} V_g dt$$

Then:

$$h_c = 100 + \delta h - a \Rightarrow$$

$$\Rightarrow h_c = 100 + \delta h - V_g \cdot \Delta t \cdot \tan(\gamma_m)$$

$$\Rightarrow h_c = 100 + \delta h - V_g \cdot \Delta t \cdot \tan(\gamma_m)$$

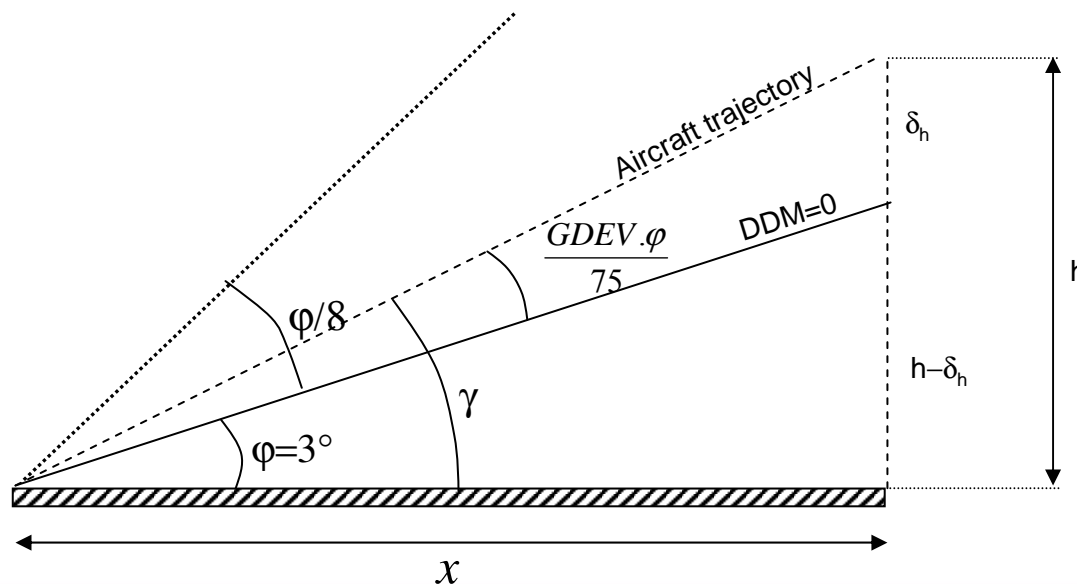
## ■ Method I

- Calculation: Longitudinal Distance (dx)
  - $t_i$  is the moment when the aircraft reached  $h_i$
  - $h_c$  is calculated from averaged FPA along with the trajectory
  - The instant  $t_c$  is obtained through a routine which looks for the moment when the aircraft reached the height  $h_c$
  - In the same way, distance  $d_{100/h_c}$  is calculated from the moment when the aircraft reached  $100 \pm \delta_h$  to  $h_c$ .
  - But: still missing the calculation of  $\delta_h$ .

## ■ Method I

### ■ Calculation: Longitudinal Distance (dx)

- Consider the figure below:
- ICAO Annex 10



$$\tan(\gamma) = \frac{h}{x}$$

$$\tan(\varphi) = \frac{h - \delta h}{x}$$

$$\frac{h}{\tan(\gamma)} = \frac{h - \delta h}{\tan(\varphi)} \Rightarrow \delta h = \left[ 1 - \frac{\tan \varphi}{\tan \gamma} \right] h$$

## ■ Method I

- Calculation: Longitudinal Distance (dx)
  - For 75uV, we have 0.175/2 DDM which is  $\varphi/8$  (ICAO)  
But  $\gamma = \varphi + (GDEV/75).(\varphi/8)$  (from the drawn)

- Finally:

$$\delta h = \left[ 1 - \frac{\tan \varphi}{\tan \left( 1 + 0.125 \cdot \frac{GDEV}{75} \right) \cdot \varphi} \right] h$$

## ■ Method I

- Calculation: Longitudinal Distance (dx)
  - Propose: Fixed Radalt with FPA trajectory estimation (Cont.)
    - Calculate the longitudinal distance from (100ft +  $\delta_h$ ) RA point to the touchdown point;
    - Calculate the longitudinal distance as being:

$$dx_m = d_{100/TD} - d_{100/hc}$$

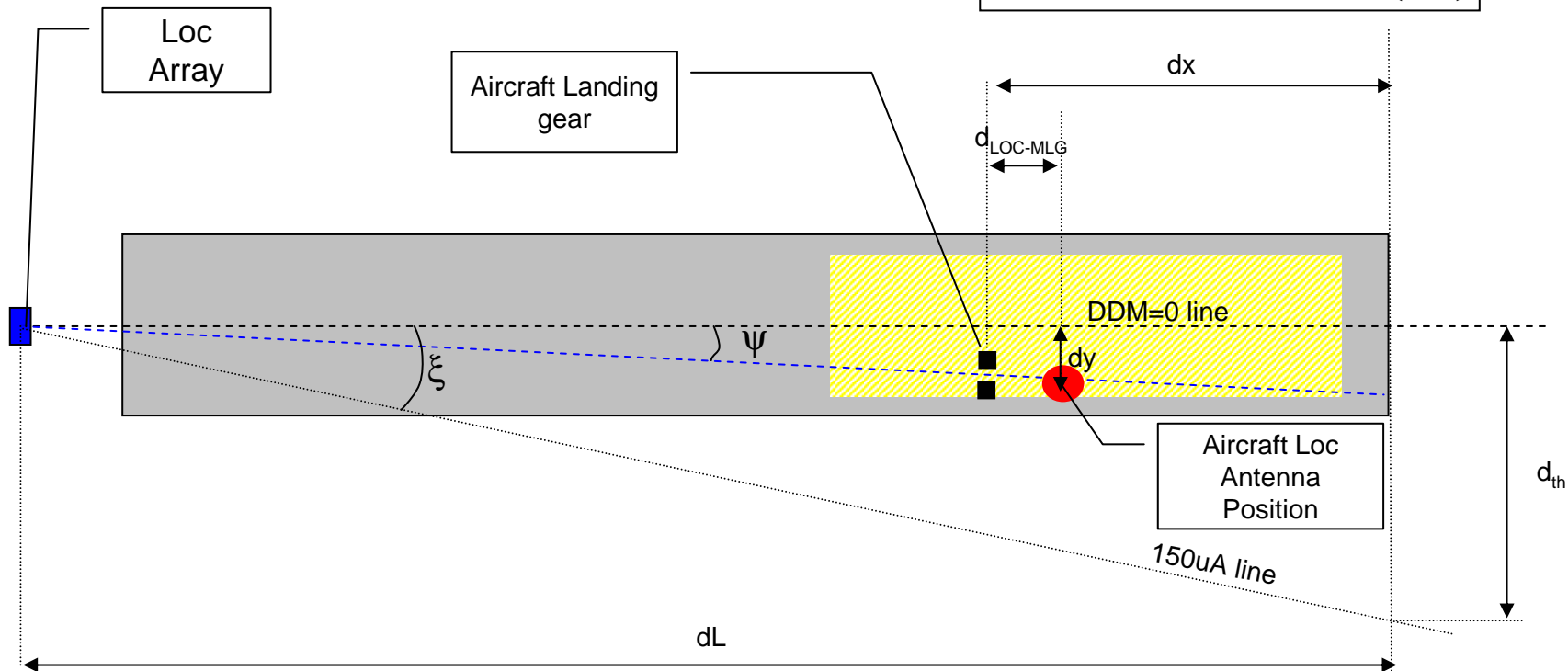
# Method for Autoland Performance Check

## Method I

- Calculation: Lateral Distance ( $dy$ )

$$\psi = LOCDEV \cdot \frac{\xi}{150}$$

$$\tan(\xi) = \frac{d_{th}}{dL} \Rightarrow \xi = \arctan\left(\frac{d_{th}}{dL}\right)$$

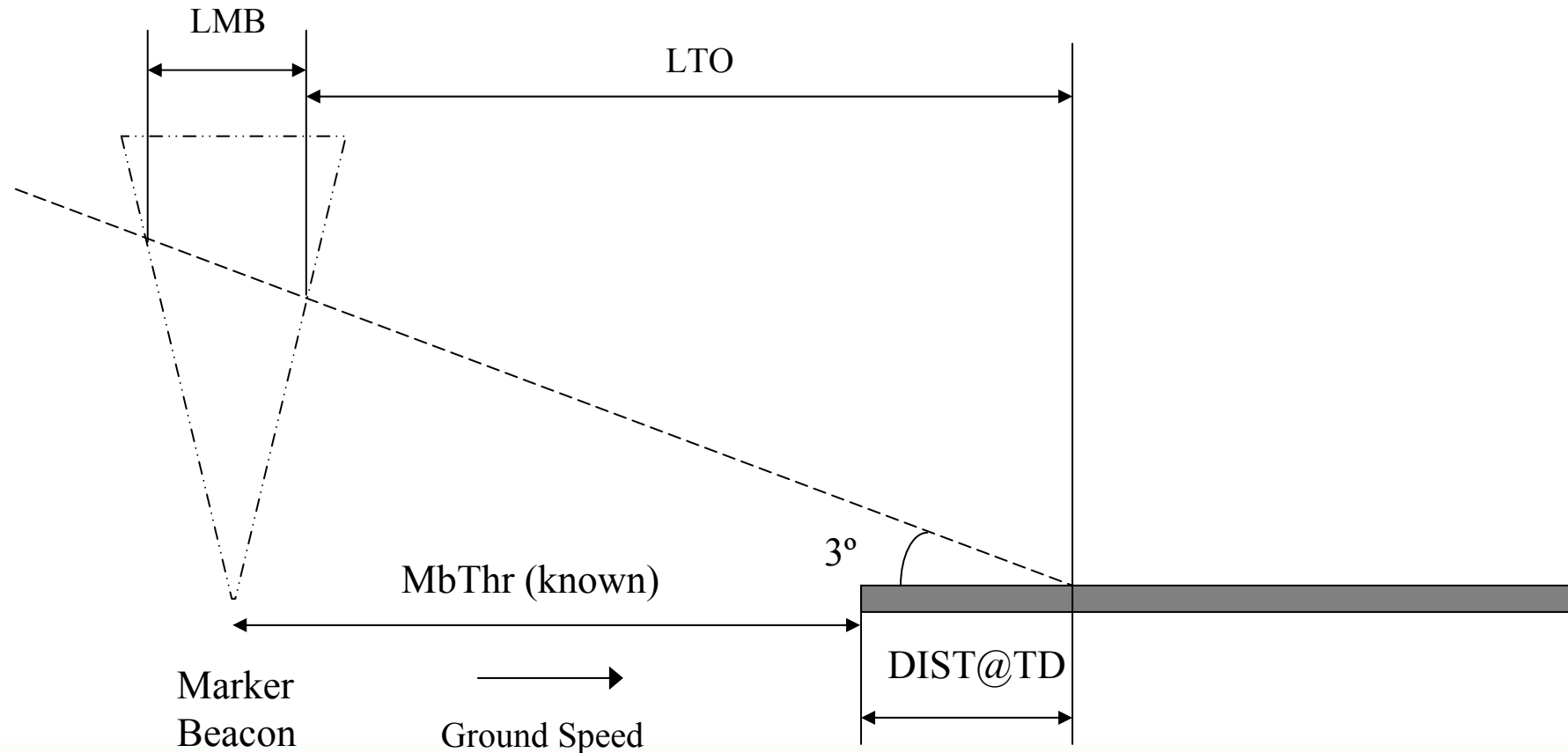


$$\tan(\psi) = \frac{dy}{(dL - dx + d_{LOC-LG})} \Rightarrow dy = (dL - dx + d_{LOC-LG}) \cdot \tan\left(\frac{LOCDEV}{150} \cdot \arctan\left(\frac{d_{th}}{dL}\right)\right)$$

## ■ Method II

- Calculation: Longitudinal Distance

$$\text{DIST@TD} = \text{LTO} + 0.5(\text{LMB}) - \text{MbThr}$$

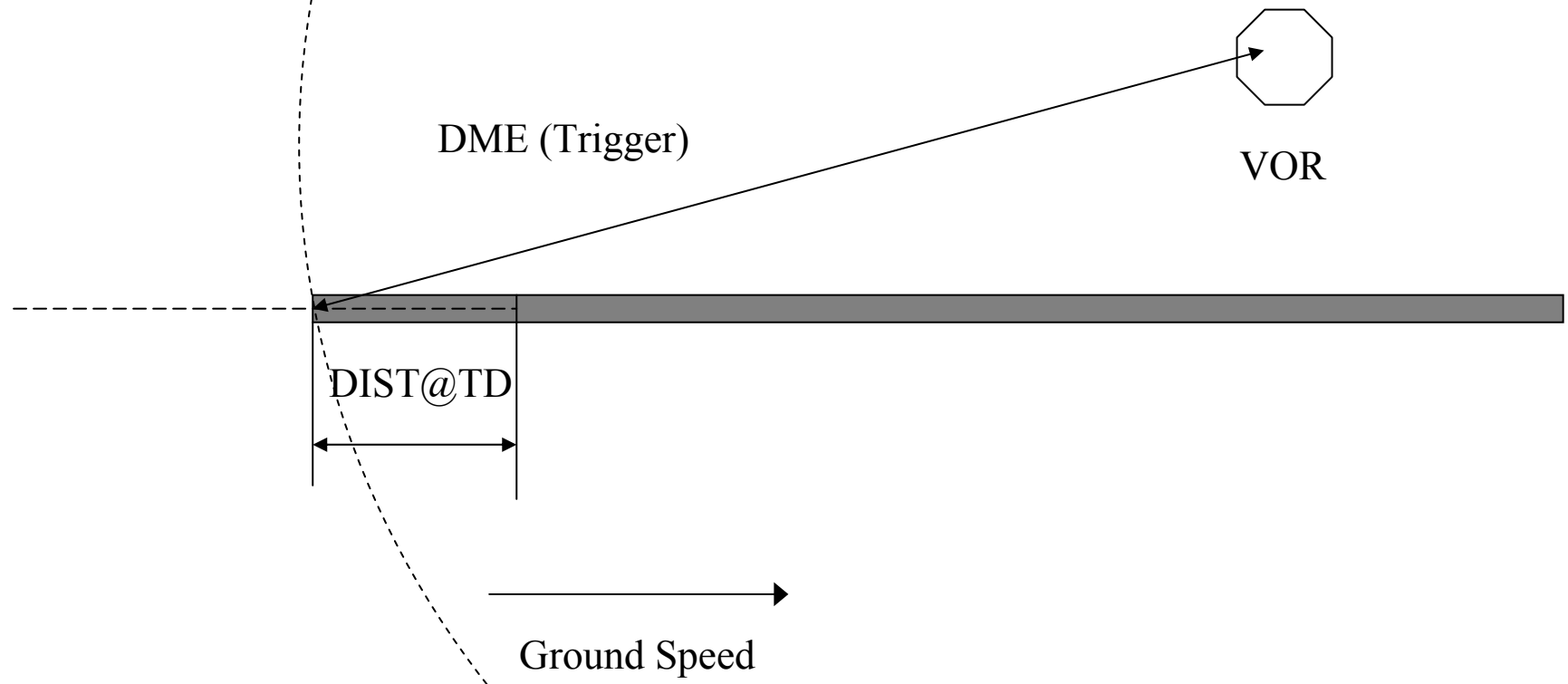


# Method for Autoland Performance Check

## ■ Method II

- Calculation: Longitudinal Distance

DIST@TD Triggered by DME



- Objective
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- **Analysis and Results**
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## ■ Analysis and Results

- **Uncertainty Analysis** has been conducted following the general uncertainty theory:

Measurements	Uncertainty Method I [m]	Uncertainty Method II [m]
Longitudinal Distance ( $U_{dx}$ )	10.10	10.72
Lateral Distance ( $U_{dy}$ )	0.89	0.41

## ■ Analysis and Results

- 2 Sigma Confidence Interval Study
- DGPS, Belly Camera, Method 1, Method 2, Comparisons
- Comparison to 2 sigma for the tested points from the desired footprint
- Comparison to 2 sigma from Monte Carlo Dispersion from the desired footprint

## ■ Analysis and Results

### ■ Methods x DGPS

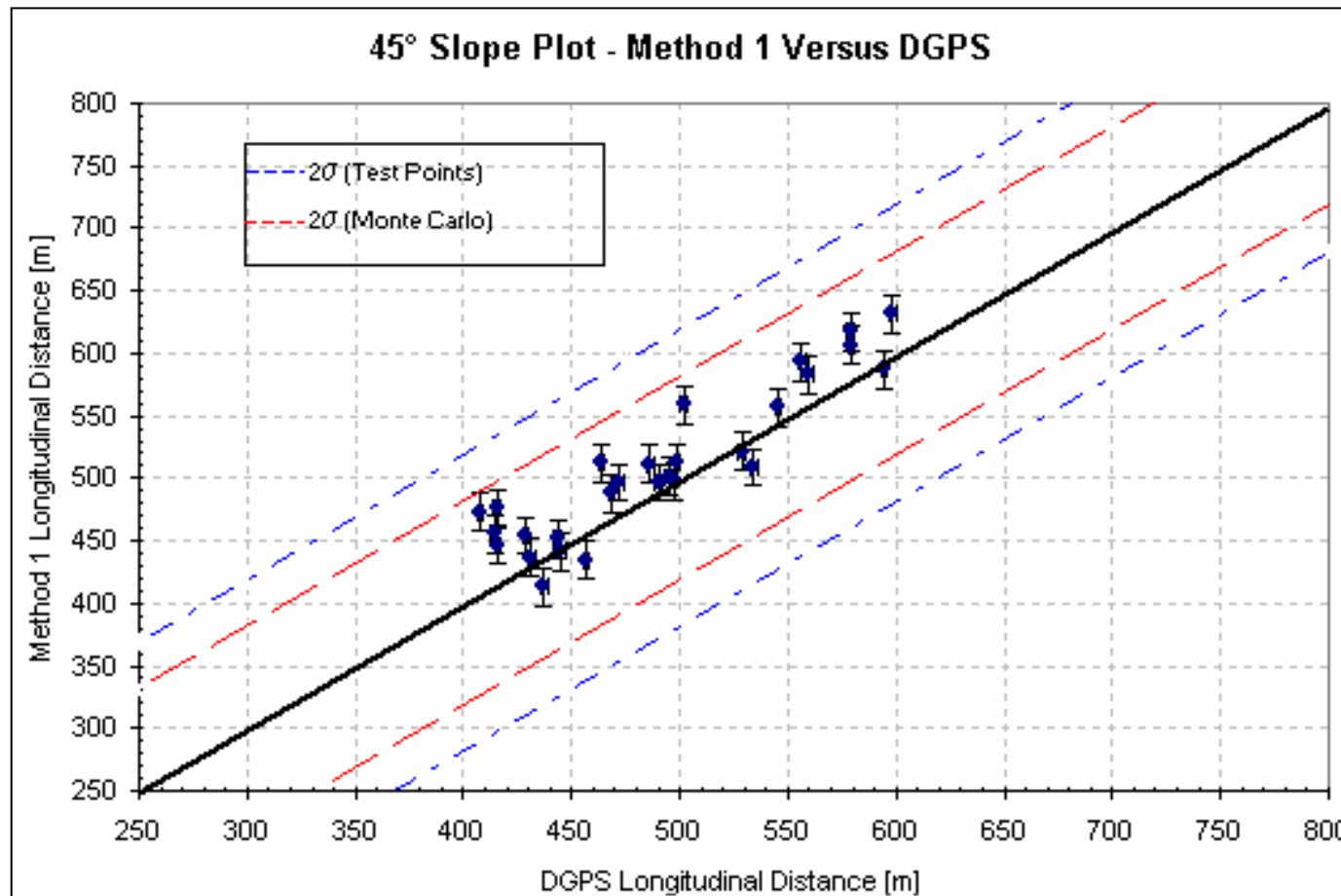
DGPS (27 Test Points)					
	Longitudinal Distance Method 1	Longitudinal Distance Method 2	Longitudinal Distance DGPS	Lateral Distance	Lateral Distance (Belly)
	[m]	[m]	[m]	[m]	[m]
Average	514.65	494.96	490.89	0.28	0.03
Sigma	62.34	55.80	59.30	2.54	2.19

### ■ Methods x Belly Camera

Belly (89 Test Points)					
	Longitudinal Distance Method 1	Longitudinal Distance Method 2	Longitudinal Distance BELLY	Lateral Distance	Lateral Distance (Belly)
	[m]	[m]	[m]	[m]	[m]
Average	434.77	419.68	426.01	1.36	0.96
Sigma	91.10	94.86	84.51	3.19	3.16

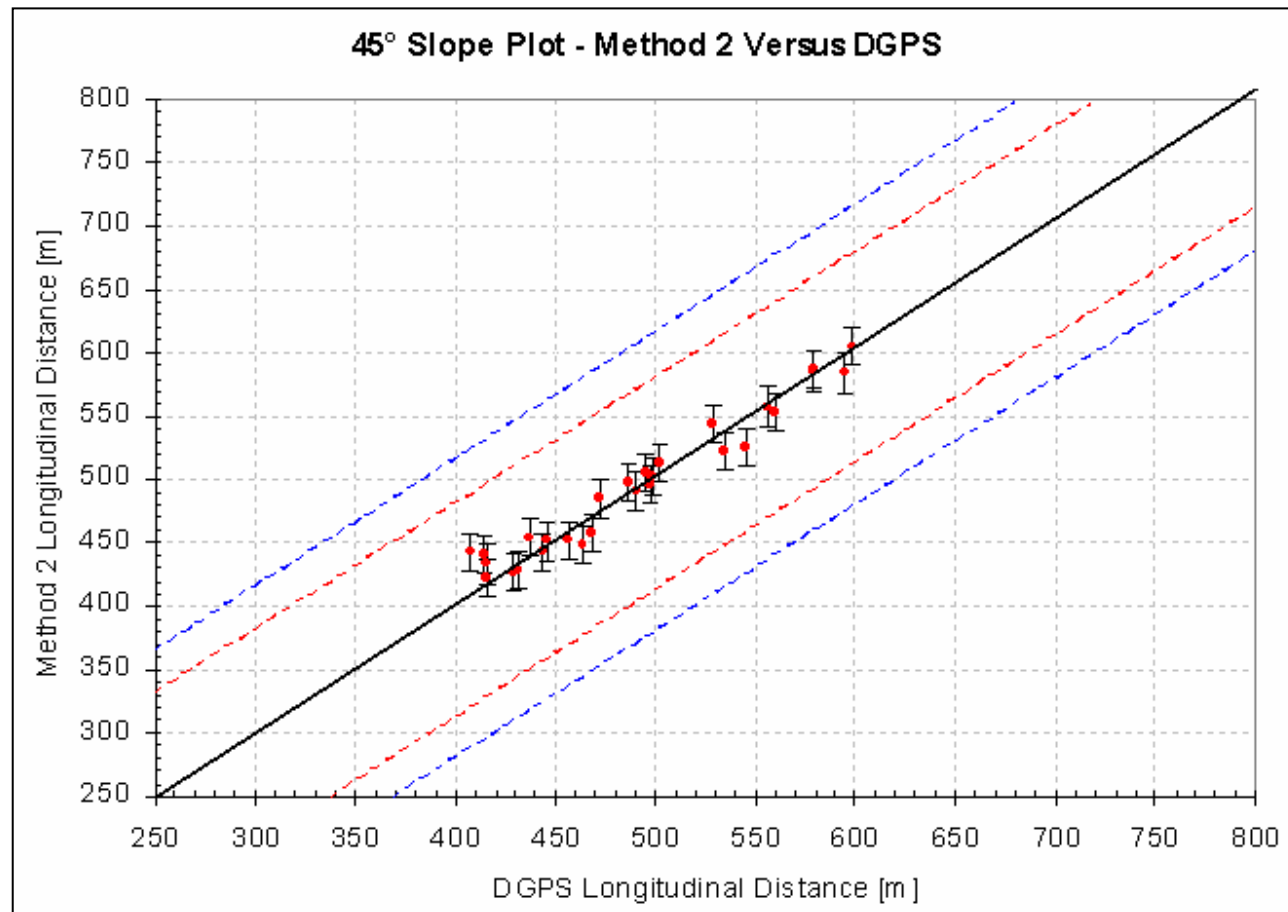
## ■ Analysis and Results

### ■ Method 1 x DGPS



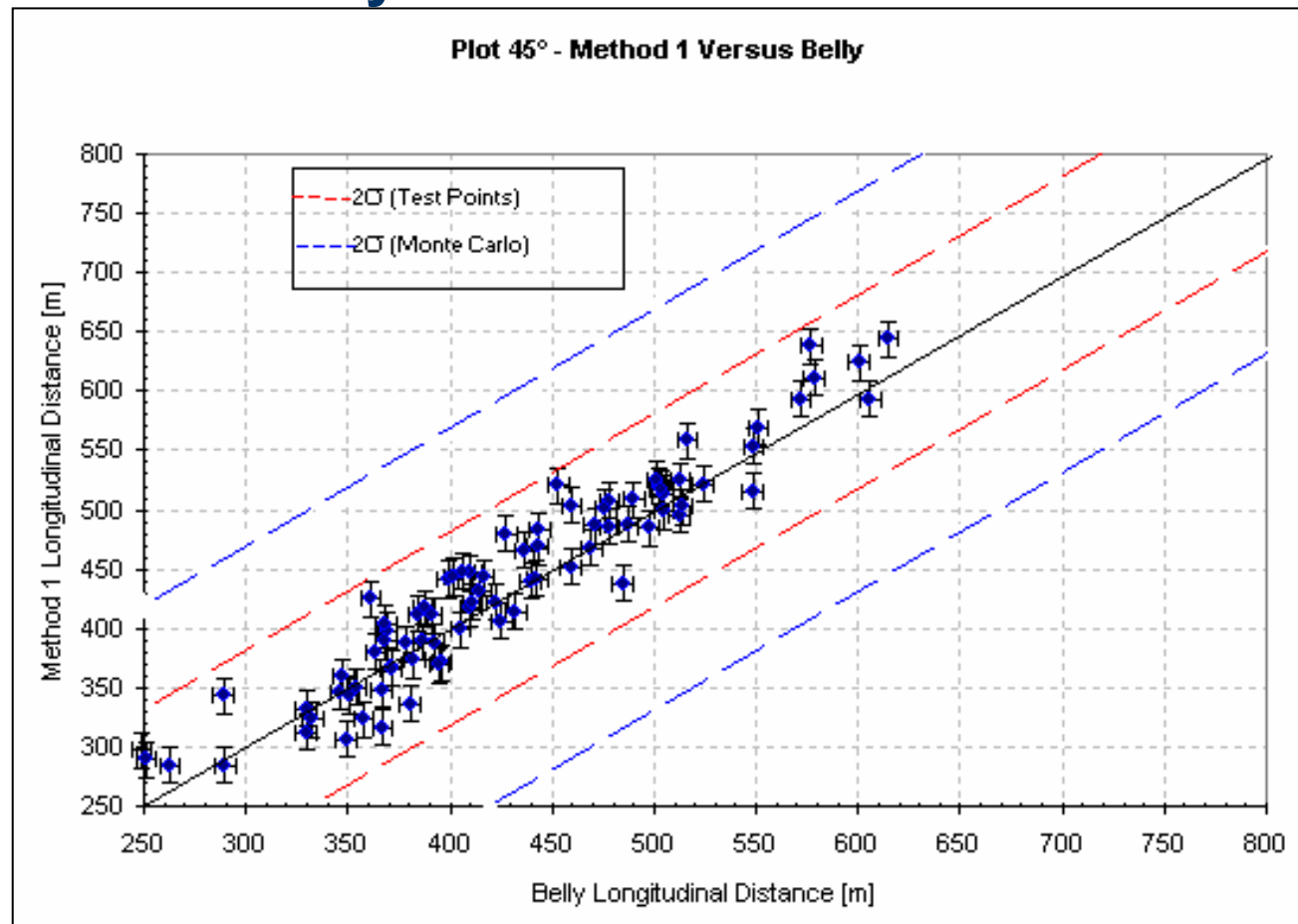
## ■ Analysis and Results

### ■ Method II x DGPS

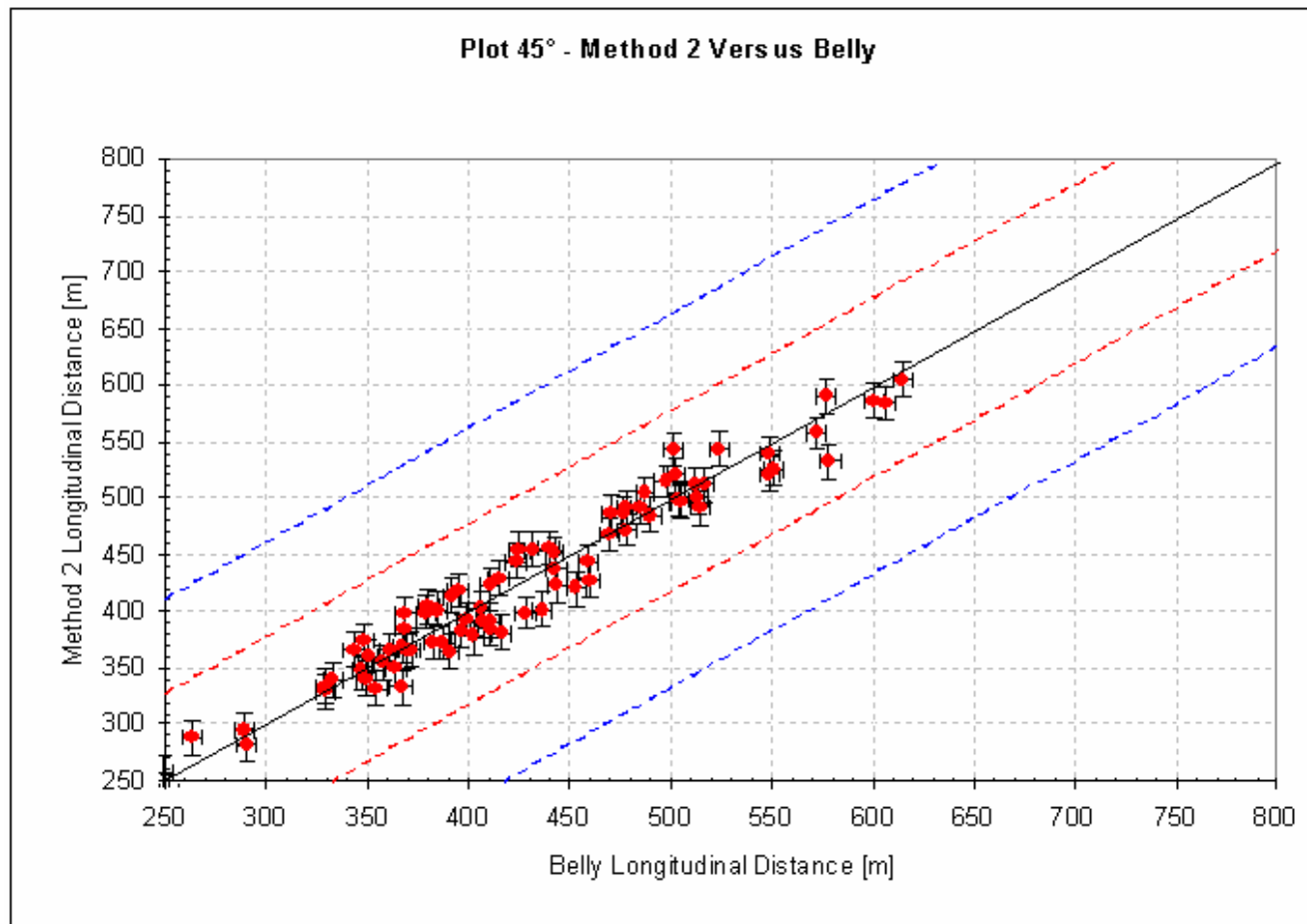


## ■ Analysis and Results

### ■ Method I x Belly Camera

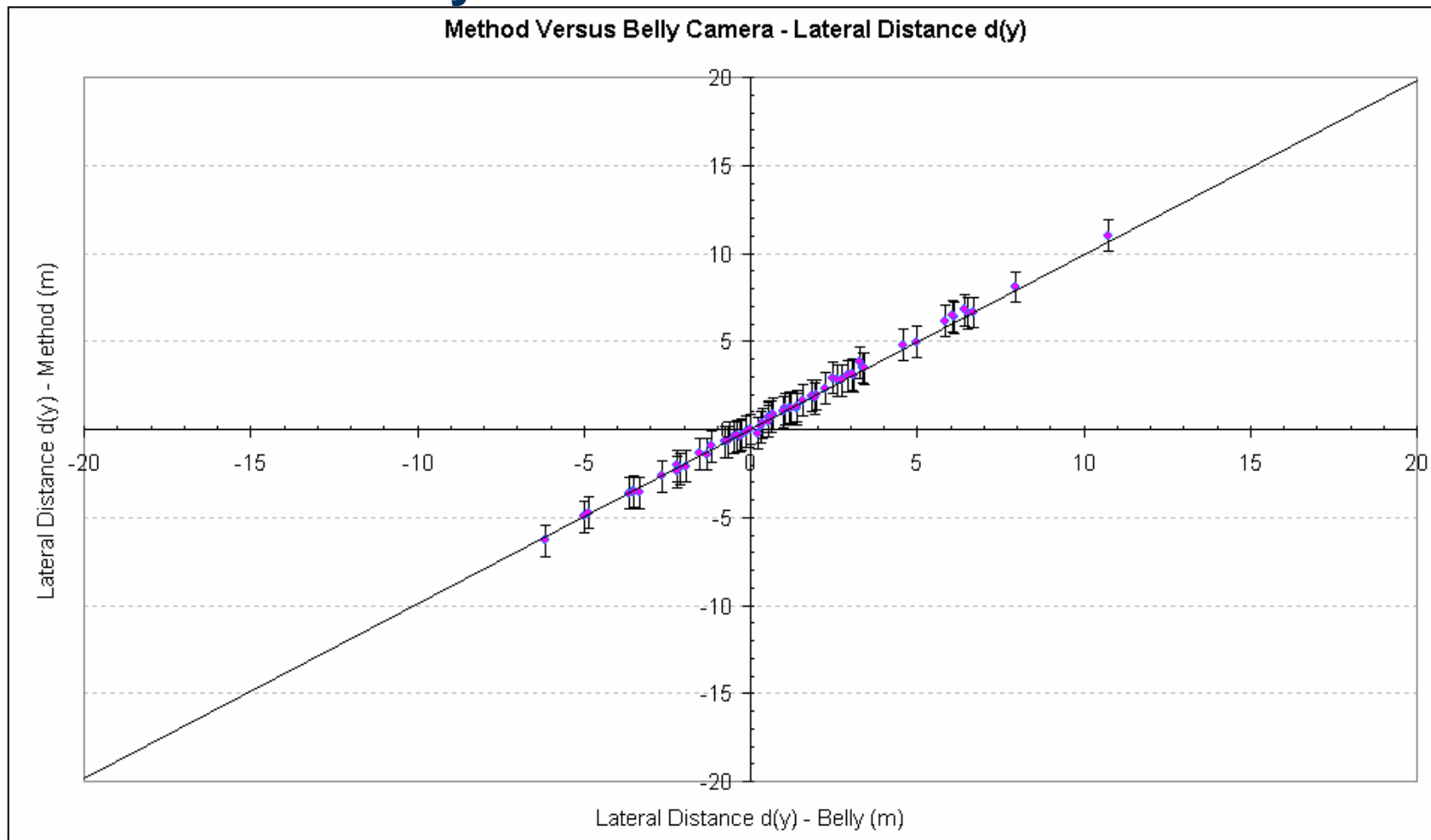


- Analysis and Results
  - Method II x Belly Camera



## ■ Analysis and Results

### ■ Method x Belly Camera - Lateral Distance

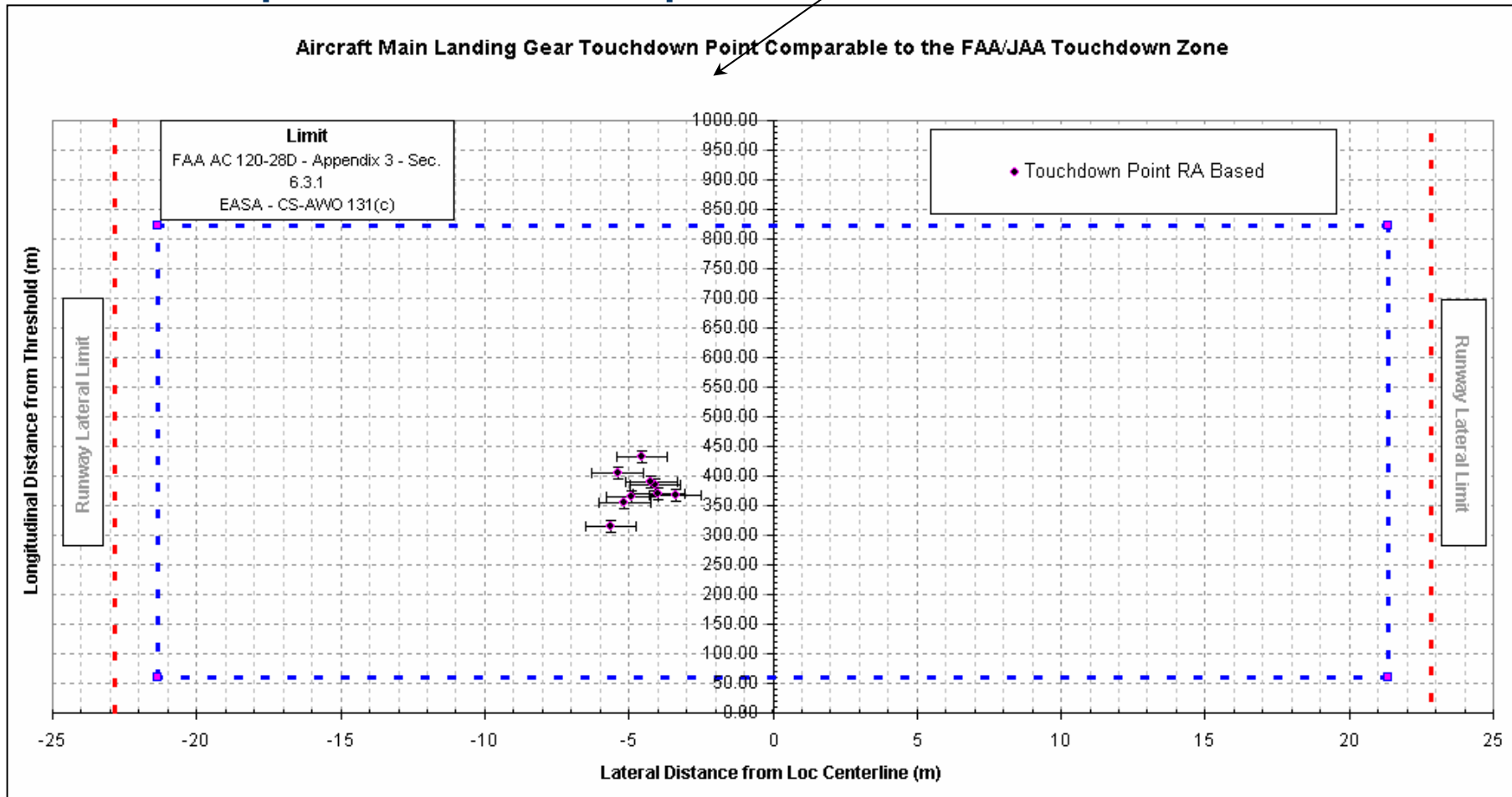


## ■ Analysis and Results

### ■ Example: Touchdown Dispersion

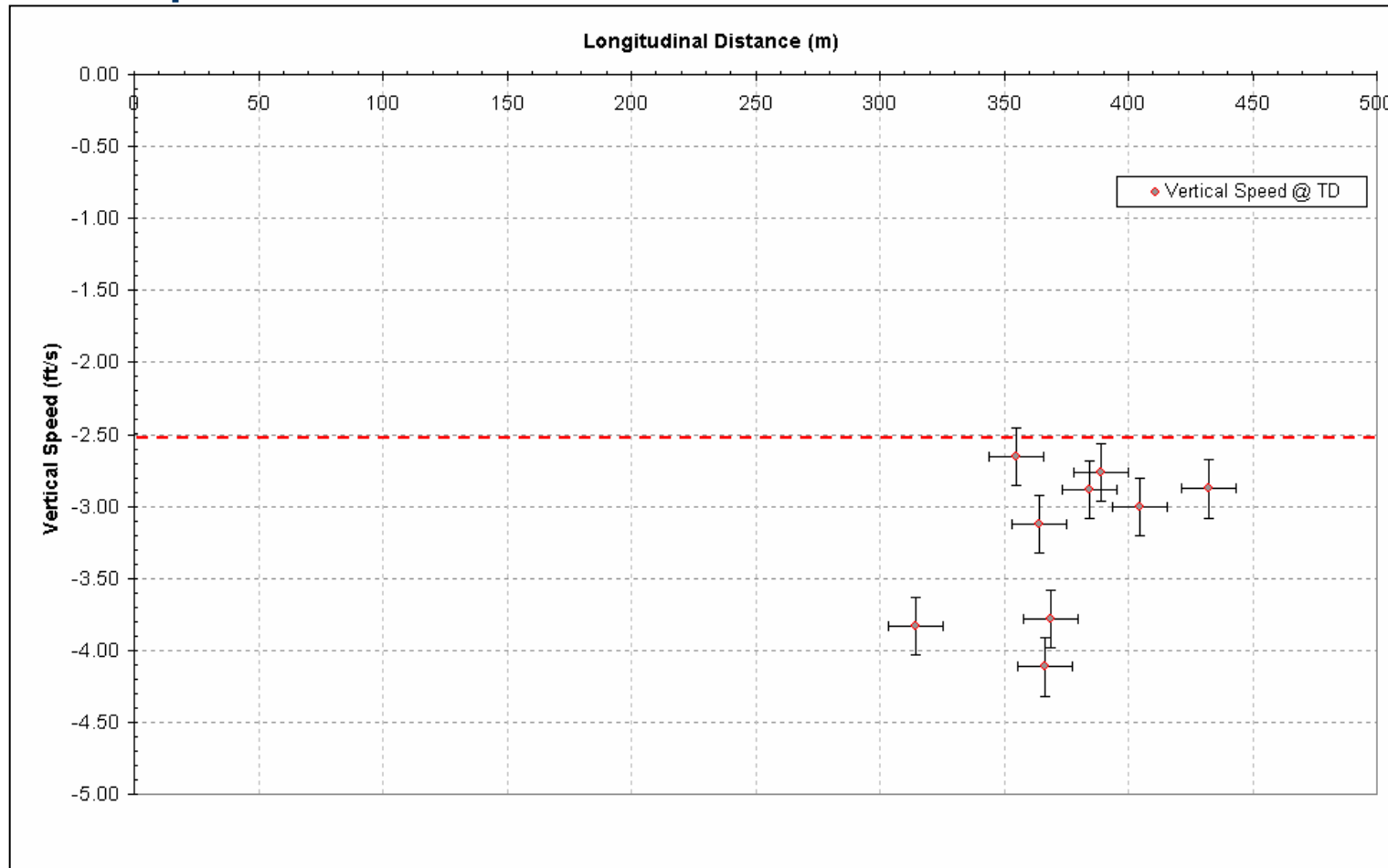
Real Data: Flight 170-001-0502  
(Beginning of development)

Aircraft Main Landing Gear Touchdown Point Comparable to the FAA/JAA Touchdown Zone



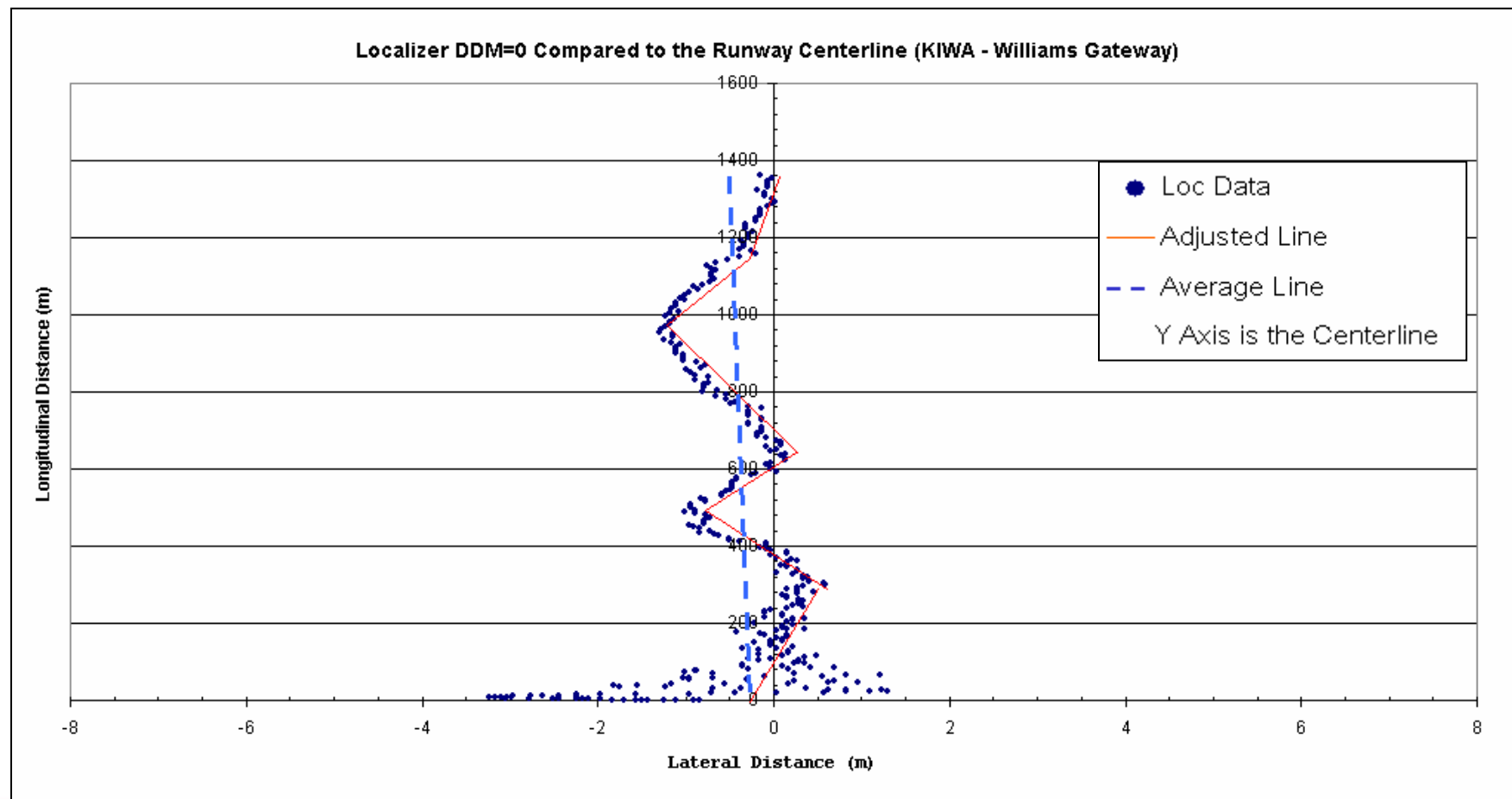
## ■ Method I

### ■ Example: Touchdown Rate



## ■ Method I

### ■ Output Parameters: Runway Localizer Beam Survey



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## ■ **Conclusions and Final Considerations**

- Method I has been defined as the main method and Method II as the backup method
  
- Validation process has demonstrated that Methods I and II are equivalents since it presents results within 95% confidence interval compared to the desired footprint (2 Sigma)
  
- Method I was chosen because:
  - **It is Equivalent to Method II**
  - **It is more conservative rather than method II**
  - **It is not depended on navy aids position and signal precision**
  - **Terrain irregularities before threshold affects the dispersion but not enough to induce points outside 95% confidence interval (10m for each 2ft)**
  - **Terrain irregularities affects just 100ft radalt height detection and FPA past history correction would reduce this effect**

## ■ Conclusions and Final Considerations

- Whenever footprint description becomes an outlier, radalt x FPA trace will be provided to confirm terrain irregularity issue.
- In last case, Backup (Method II) will be executed in order to provide accurate data, since equivalence has been proven.
- Both Backup and Method I will be ran during all certification flights in order to have as much data as possible
- Belly Camera (All Airports) and DGPS (Brazilian Airports) will be the tools for method validation.

## ■ Bibliography

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- **COLLEMAN, H.W. Experimental and Uncertainty Analysis for Engineers, second edition, 1999.**
- **EASA CS-AWO – Certification Specifications for All Weather Operations , October 2003**

## ■ Authors

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